From: Barbara Ritchie <BARBARA.RITCHIE@fmc.com>

Sent: Friday, March 14, 2014 2:54 PM

To: Rochlin, Kevin

Cc: Sheldrake, Beth; Greutert, Ed [USA]; Kelly Wright; susanh@ida.net; Bruce.Olenick@deq.idaho.gov;

Douglas.Tanner@deq.idaho.gov; Scott.Miller@deq.idaho.gov; Jeff Hamilton; Marguerite

Carpenter; David Heineck; Marc Bowman; Michael Steiner; 'Rob Hartman'

Subject: RE: Comments on the Data Gap Report

Attachments: 2014-03-14 FMC Responses to EPA Comments on the Data Gap Report for thepdf; 2014-03-14

FMC Data Gap Report for the FMC OU - Highlighted Rev.pdf

Categories: Lepic 3-22 to 4-4, COPIED TO LEPIC FOLDER ALREADY

Kevin,

Please find attached FMC's responses to the EPA comments on the Data Gap Report for the FMC OU received from EPA on February 20, 2014 as well as a revised copy of the Data Gap Report with the changes shown highlighted in yellow. Revised Figures 2-2 and 4-1 and minor pagination changes are not highlighted.

Any questions, please advise.

From: Rochlin, Kevin [mailto:rochlin.kevin@epa.gov]

Sent: Monday, March 03, 2014 11:17 AM

To: Barbara Ritchie

Subject: RE: Comments on the Data Gap Report

Your request for an extension is approved.

Kevin

From:

Kevin Rochlin | Superfund Remedial Project Manager U.S. Environmental Protection Agency | Region 10 Office of Environmental Cleanup 1200 6th Avenue, Suite 900, ELC-111 | Seattle, WA 98101 (206) 553-2106 (206) 553-0124 (fax) rochlin.kevin@epa.gov

From: Barbara Ritchie [mailto:BARBARA.RITCHIE@fmc.com]

Sent: Thursday, February 27, 2014 7:40 AM

To: Rochlin, Kevin

Subject: RE: Comments on the Data Gap Report

Kevin,

As per my voice message, the UAO would appear to require us to respond to the comments you provided on the Data Gap Report within 15 days, which would be 3/5/14. FMC requests your approval of an extension until 3/14/14 to submit a response to these comments and a revised Data Gap Report.

Please confirm your approval.

From: Rochlin, Kevin [mailto:rochlin.kevin@epa.gov] Sent: Thursday, February 20, 2014 12:49 PM

To: Barbara Ritchie

Cc: Douglas.Tanner@deq.idaho.gov; Greutert, Ed [USA]; Kelly Wright; Scott Miller - Idaho DEQ (Scott.Miller@deq.idaho.gov); Stifelman,

Marc; susanh@ida.net; Zavala, Bernie **Subject:** Comments on the Data Gap Report

See attached file.

Kevin Rochlin

From:

Kevin Rochlin | Superfund Remedial Project Manager U.S. Environmental Protection Agency | Region 10 Office of Environmental Cleanup 1200 6th Avenue, Suite 900, ELC-111 | Seattle, WA 98101 (206) 553-2106 (206) 553-0124 (fax) rochlin.kevin@epa.gov

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FMC Idaho LLC, Pocatello, Idaho

REMEDIAL DESIGN
DATA GAP REPORT
for the FMC OU

March 2014



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ACRONYMS/ABBREVIATIONS

ASTM American Society of Testing and Materials

bgs below ground surface

CERCLA Comprehensive Environmental Response, Compensation, and Liability Act

cm/sec centimeters per second

DGWP Data Gap Work Plan

EPA U.S. Environmental Protection Agency

ET evapotranspirative

ft feet

in. inch

IRODA Interim Record of Decision Amendment

LL liquid limit

meq molar equivalent
MDD maximum dry density
mg/kg milligrams per kilogram

mmhos micromohs

OMC optimal moisture content

OU operable unit

lbs/ft³ pounds per cubic foot

PI plasticity index PL plastic limit

RA remediation area

RAO remedial action objective

RDRA Remedial Design/Remedial Action RDWP Remedial Design Work Plan

SB soil boring

SFS Supplemental Feasibility Study
SRI Supplemental Remedial Investigation

TCLP Toxicity Characteristic Leaching Procedure

TP test pit

UAO Unilateral Administrative Order

WUA Western Undeveloped Area

1.0 INTRODUCTION

As specified in the *Interim Amendment to the Record of Decision for the EMF Superfund Site FMC Operable Unit* (IRODA; EPA 2012), the selected soil remedy for the FMC OU includes the construction of soil covers over specified remediation areas (RAs). Two soil cover designs are specified: gamma cap and evapotranspiration (ET) cap. The preliminary designs for these soil covers are summarized below:

- The ET soil cover design consists of a minimum cover thickness of 24 inches of soil that will provide sufficient water storage and an additional 6 inches of soil to address potential long-term erosion of the cover. The design basis is presented in the *Comparison of Conventional and Alternative Capping Systems for Use at the FMC Plant OU (Capping Memorandum)* contained in Appendix D of the *Supplemental Feasibility Study Report for the FMC Plant Operable Unit (SFS Report*, MWH, 2010).
- The gamma soil cover consists of a nominal 12 inches soil and is expected to provide sufficient gamma shielding from underlying fill materials. As described in the Remedial Design Work Plan (RDWP; MWH, 2013a), a gamma cap performance evaluation will be detailed in the separately-submitted Gamma Cap Performance Evaluation Work Plan.

The selected remedy requires approximately 155 acres of ET soil covers and 340 acres of gamma soil covers. The soil to be used for construction of both types of covers will be removed from the Western Undeveloped Area (WUA), an area of the westernmost portion of the FMC Plant OU that was never used in the phosphorus manufacturing process. Additional site-specific soil data from the WUA is required to proceed with cover design. This report details the additional soil sampling and material (geotechnical) testing that was performed to better define the volume of available borrow soil and its material properties to finalize the design of the soil covers.

As specified in the IROD, the selected groundwater remedy for the FMC OU includes groundwater extraction and treatment, with treatment either at the City of Pocatello POTW or by a water treatment facility built within the FMC OU. The latter alternative would discharge treated water to an infiltration basin, from which it would either percolate down to groundwater or evaporate to the atmosphere. FMC is evaluating both of these treatment options. This report describes the collection of soil percolation data that was performed to support the evaluation and potential design of the onsite percolation/ evaporation basin(s).

Another remedial action requirement of the IROD is that elemental phosphorus residues that may remain in underground 16-inch, reinforced concrete storm/sewer piping in RA-A must be removed and disposed of offsite. This report presents the procedures used to perform a video survey of that underground storm drain piping to better understand the volume of residual solids it contains and support design of this element of the remedial action.

1.1 REGULATORY BACKGROUND

On June 10, 2013, EPA Region 10 issued a Unilateral Administrative Order to FMC for Remedial Design and Remedial Action (UAO for RD/RA, or UAO; EPA 2013), EPA Docket No. Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA)-10-2013-0116. The UAO for RD/RA requires FMC to implement the interim remedial actions that EPA selected in its September 27, 2012 Interim Record of Decision Amendment for the FMC OU ("IRODA"). FMC is implementing the selected remedy in accordance with the UAO.

As summarized in Section 3 of the RDWP a data gap investigation was performed between October 29th to November 13th, 2013 to collect site specific data to support the RD as defined in of Section IX, Paragraph 30 a. and 30 b. of the UAO. This Data Gap Report summarizes the investigations performed and testing completed in accordance with the Data Gap Work Plan (DGWP; MWH, 2013b) that was approved by EPA on October 22, 2013.

1.2 FMC SITE DESCRIPTION

A description of the FMC OU is presented in Section 2 of the RDWP. A site map showing the FMC OU RAs and WUA is provided on Figure 1-1.

1.3 PURPOSE AND SCOPE OF REPORT

This report has been developed to provide the following:

- 1. Summarize the site investigations and material testing performed as per the DGWP;
- Present the results of soil testing performed on samples collected from the WUA, including properties (geotechnical, hydrological, agronomical, vegetative) to support design of the ET soil covers and evaluate potential design of the infiltration basin option for managing treated groundwater;
- 3. Provide an estimate of the availability of borrow soil within the WUA for cap construction;
- 4. Present the results of the RA-A stormwater sewer survey; and
- 5. Provide an estimate of the root density expected based on the vegetation trial plot survey.

1.4 DOCUMENT ORGANIZATION

The remainder of this Data Gap Report consists of the following:

- Section 2.0 Data Gap Field Investigations Presents a summary of the field investigations performed per the DGWP.
- Section 3.0 Laboratory Testing Presents a summary of the laboratory testing performed on samples collected during the field investigation.

- Section 4.0 Data Gap Investigation Results Presents the results of the field investigation, including a summary of soil property testing, root density testing, and the stormwater sewer video survey.
- Section 5.0 contains references.
- Appendix A: Field Investigation Photographs
- Appendix B: Test Pit Logs
- Appendix C: Soil Boring Logs
- Appendix D: Geotechnical and Hydrological Testing Reports
- Appendix E Agronomic Testing Reports
- Appendix F: Root Density Testing Reports
- Appendix G: RA-A Stormwater Sewer Decontamination Waste Determination Laboratory Reports and DVD of Video Survey
- Appendix H: ProUCL 5.0 Statistical Analysis

2.0 DATA GAP FIELD INVESTIGATIONS

A variety of field investigations were performed during October 29th to November 13th per the DGWP and included the following:

- Excavation of 10 test pits within the WUA;
- Drilling of 5 soil borings within the WUA;
- Video survey of stormwater sewer piping in RA-A; and
- Collection of soil samples from the FMC vegetation trial plot.

A description of the above investigations is provided below. Photographs taken during the field investigations are presented in Appendix A.

2.1 WESTERN UNDEVELOPED AREA INVESTIGATIONS

A focused investigation was performed in the WUA consisting of test pits and soil borings. Test pit and soil boring locations are presented in Figure 2-1 and a summary of the investigations are presented in Table 2-1. Test pit and soil boring logs from the WUA are presented in Appendix B and C, respectively.

Table 2-1 Summary of WUA Soil Investigation

Test Pit/Soil Boring I.D.	Total Depth (feet bgs)	Depth of Gravel (feet bgs)	Maximum Depth of Grab Sample	Sample Depths/Intervals
TP001	15.7	15.7	10	Grab samples collected at 1 foot intervals down to 10 feet.
TP002	17.3	NC ^{a/}	10	Grab samples collected at 1 foot intervals down to 10 feet.
TP003	4	4	3	Grab samples collected at 1 foot intervals down to 10 feet.
SB003	31.5	2.0	15	Undisturbed sample collected at 0 to 2 feet (bgs), and disturbed sample collected 2 to 15 feet.
TP004	18	NC ^{a/}	10	Grab samples collected at 1 foot intervals down to 10 feet.
SB004	31.5	23.5	NA	Undisturbed samples collected at 2 to 4 and 6 to 8 feet (bgs).

Test Pit/Soil Boring I.D.	Total Depth (feet bgs)	Depth of Gravel (feet bgs)	Maximum Depth of Grab Sample	Sample Depths/Intervals
TP005	20.5	NC ^{a/}	11	Grab samples collected at 1 foot intervals down to 10 feet.
TP006	17.1	NC ^{a/}	10	Grab samples collected at 1 foot intervals down to 10 feet.
SB006	31.5	21.1	NA	Undisturbed samples collected at 2 to 4, 6 to 8 feet (bgs).
TP007	19.8	NC ^{a/}	10	Grab samples collected at 1 foot intervals down to 10 feet.
SB007	31.5	24.5	NA	Undisturbed samples collected at 2 to 4, 6 to 8, and 12 to 14 feet (bgs).
TP008	19.8	NC ^{a/}	10	Grab samples collected at 1 foot intervals down to 10 feet.
SB008	31.5	30.0	NA	Undisturbed samples collected at 2 to 4 and 6 to 8 feet (bgs).
TP009	12.3	7.5	7	Grab samples collected at 1 foot intervals down to 10 feet.
TP010	9.0	6.0	6	Grab samples collected at 1 foot intervals down to 10 feet.

Notes:

2.1.1 Test Pits

A total of ten (10) test pits (TP001 through TP010) were excavated throughout the WUA. Grab soil samples were collected from each test pit at approximately 1-foot intervals down to 10 feet or until gravels were contacted and composited to provide 2 5-gallon buckets of representative soils from each location per the Work Plan. The test pits were excavated to various depths ranging from 7 to 20 feet below ground surface. Soils encountered in the test pits were predominantly loess silt (silt) overlying gravels. The depth of silts ranged from 4 to 20.5 feet deep with the majority of test pits encountering silt down to at least 15 feet. Depth measurements were completed at the base of the test pit and in any test pits where gravels were contacted. As indicated by the test pitting and confirmed by the subsequent soil borings, shallow

^{a/} NC = gravels not contacted in test pit before maximum depth of the excavator was reached.

gravel was contacted in TP003, TP009, and TP010 at depths ranging between 4 and 7 feet bgs. This gravel deposition appears to bisect the WUA in an east-west direction, generally shallower on the east end and deeper on the west end. Additional exploratory borings were also excavated, without samples being collected on the north and south sides of TP003, TP009, and TP010 to define the lateral extent of the gravel lense. Visual observations during the exploratory borings indicate that there is a sharp drop in depth of the gravels at an approximate distance of 300 feet on either side of the test pits where gravel was contacted. The field investigation (including test pits and soil borings) adequately characterized the extent of the shallow gravels for assessing the amount of soil available for use as capping soil in the WUA.

2.1.2 Soil Borings

Five soil borings (SB003, SB004, SB006, SB007, and SB008) were collocated within 20 feet of five test pit locations (TP003, TP004, TP006, TP007, and TP008) and drilled to depths ranging up to 31.5 feet. The purpose of the soil borings were to collect undisturbed samples of the silt, to characterize the general depth of gravels underlying the silts, and collect disturbed samples of the gravel. Undisturbed samples of the silts were collected at SB003, SB004, SB006, SB007, and SB008 using a Shelby tube at depths of 0 to 2-feet, 2 to 4-feet and 6 to 8-feet with one sample collected at 12-14 feet. The undisturbed silt sample was collected at 0 to 2-feet at SB003, but no deeper samples were collected, due to the presence of gravels at 2 feet and below. The sample at 12-14 feet was collected at SB007 to provide additional information related to the in-situ hydraulic conductivity of the silts at deeper depths. One grab sample of the gravels recovered from the auger during drilling from 2 to 15 feet bgs in SB003 was also collected for laboratory permeability analysis. Based on visual observation, the underlying gravels size was predominantly 3-inch minus and were metamorphic in nature.

The DGWP specified that gravel samples would be collected at a depth approximately 10 feet below the gravel horizon in each soil boring. When the Data Gap Work Plan (MWH, 2013) was prepared, the depths of gravels were believed to be shallower, on the order of ± 10 feet. However, during the test pitting, the depths of gravel were shown to be generally much deeper than 10 feet throughout the site, with the exception of the east-west trending shallow gravel area. The main purpose of the gravel sampling was to determine the hydraulic conductivity of the gravels for the purpose of sizing potential infiltration basins for treated groundwater. Given that the depth of excavation required to obtain the required amount of capping soil in general will be much shallower than the underlying gravels, it was determined that the controlling factor in the infiltration basins will be the in-situ hydraulic conductivity of the silts. Therefore, an undisturbed sample of the silts was collected at a deeper depth, 12-14 feet bgs, in SB0007 to provide data for this purpose. Further, the gravels that were contacted appeared to be very uniform in terms of shape and size suggesting that the hydraulic conductivity of these gravels will be fairly uniform. Therefore, no additional sampling is required at deeper depths for the gravels.

2.2 STORMWATER SEWER SURVEY

2.2.1 Background and Objectives

Historical information gathered during the Supplemental Remedial Investigation (SRI) indicated that the subsurface stormwater piping located in RA-A had carried stormwater runoff and process materials from the furnace building and phos loading dock (RA-B) to the railroad swale (RA-K). These process materials consisted of wash waters that were suspected of containing ore, slag, precipitator slurry, and phossy water (containing elemental phosphorus). However, it was not known if these materials were still present in the underground stormwater piping and to what extent. The selected remedy (Soil Alternative 3) prescribed that the underground stormwater sewer piping within RA-A (to be capped with a gamma cap) be cleaned out to remove any process materials that could present a threat to groundwater or future site workers (i.e., elemental phosphorus, metals, and radionuclides). Underground storm sewer piping that is successfully cleaned in-place will no longer present a threat to human health and the environment as all COCs potentially associated with the storm sewer piping (i.e., P4, radionuclides, metals, and leachable metals posing a threat to groundwater) will have been removed and appropriately disposed. Therefore, cleaned underground storm sewer piping by itself meets all of the RAOs specified in the IRODA.

A video survey of the subsurface stormwater piping located in RA-A was conducted to determine the approximate volume of accumulated solids within the piping (with the potential presence of P4) and to estimate the amount of material (sediments) that will require removal, characterization, and disposal. The subsurface stormwater sewer piping included in the video survey is presented in Figure 2-2. Although the cleaning of the stormwater sewer piping as specified in the selected remedy was limited to the piping within RA-A, an attempt will be made to clean all of the stormwater sewer piping as shown in Figure 2-2 during the remedial action. If cleaning of any piping segment is not possible due to physical constraints, the ET cap over RA-B will be extended to cover the uncleaned segments. As stated in the IRODA, placement of a properly designed ET cap over underground piping would meet all of the above listed RAOs, even with the presumption that radionuclides, metals, and/or P4 remain within the un-cleaned sections of the underground storm sewer piping. Also, any stormwater piping which extends under an ET cap will be plugged with concrete to prevent water migration through the piping under the ET cap.

2.2.2 Video Survey Description

The stormwater sewer video survey was performed on November 6, 2013. The video surveillance utilized a remote control robotic camera that was lowered down into the piping through existing drain inlets, manholes and discharges. This technology is typically used on underground sewer piping that has been cleaned prior to the survey. Results of the video survey were very useful, but limited due to the inability of the robotic camera to proceed through 16-

inch piping that was partially full of sediment and did not fit in the 8-inch lines. A DVD of the survey video is included in Appendix G. A summary of the video surveys is presented below with the surveyed piping segments shown on Figure 2-2:

- The piping segment from west discharge pipe toward Area Inlet #4 This piping segment consists of a 16-inch concrete pipe from the west discharge into the railroad swale (RA-K) toward the Area Inlet #4 (about 129 feet total length). This segment was about 50% full of sediments at the discharge and there was not sufficient headspace to send the robotic camera into this piping. The sediment as observed from the end of the west discharge pipe appeared to consist of ore, slag, and native soils. There was no evidence of P4 in the sediment.
- The piping segment from Area Inlet #4 toward the west discharge pipe This piping segment is the same as described above. An attempt was made to send the robotic camera in the reverse direction from Area Inlet #4 toward the west discharge pipe. The robotic camera was only able to travel about 2 feet before becoming stuck in the sediment. The sediment as observed from the robotic camera and from decon of the robotic camera appeared to consist of ore, slag, and native soils. There was no evidence of P4 in the sediment. This pipe as observed from Area Inlet #4 was greater than 50% full of sediments.
- The piping segment from east discharge pipe toward Area Inlet #1 This piping segment consists of a 16-inch concrete pipe from the east discharge into the railroad swale (RA-K) toward the Area Inlet #1 (about 85 feet total length). This segment was surveyed with the robotic camera. The first half of the pipe was relatively clean from the east discharge until about 40 feet into the pipe. The pipe was about 10 to 20% full of sediment the remainder of the distance to Area Inlet #1. The sediment as observed from the robotic camera and from decon of the camera appeared to consist of ore, slag, and native soils. There was no evidence of P4 in the sediment.
- The piping segment from Area Inlet #4 to Area Inlet #3 This piping segment consists of a 16-inch concrete pipe from the Area Inlet #4 to Area Inlet #3 (about 107 feet total length). An attempt was made to send the robotic camera from Area Inlet #4 toward Area Inlet #3. The robotic camera was not able to travel down this segment due to the sediment. The sediment as observed from the robotic camera and from the decontamination of the robotic camera appeared to consist of ore, slag, and native soils. There was no evidence of P4 in the sediment. This pipe as observed from Area Inlet #4 is assumed to be 100% full of sediments.
- The piping segment from Area Inlet #4 to Area Inlet #2 and Area Inlet #5 These piping segments consists of 8-inch steel piping from the Area Inlet #4 to Area Inlet #2 (about 170 feet total length). A separate 8-inch steel pipe branches off from this segment toward Area Inlet #5 (about 180 feet total length). As the robotic camera could not pass through an 8-inch pipe, an attempt was made to send a cable camera from Area Inlet #4 toward Area Inlet #2 and Area Inlet #5. The cable camera was not able to travel down these piping segments due to the sediments in the pipes and access restrictions. The sediment as observed from the cable camera and from decon of the cable camera appeared to consist of ore, slag, rust, and native soils. There was no evidence of P4 in the

- sediment. These pipes as observed from Area Inlet #4 are assumed to be 70% full of sediments.
- The piping segment from Manhole #1 to Area Inlet #3 This piping segment consists of a 16-inch concrete pipe from Manhole #1 to Area Inlet #3 (about 169 feet total length). The robotic camera was sent from Manhole #1 toward Area Inlet #3 and traveled about 55 feet before being blocked by sediment. The sediment as observed from the robotic camera and from decon of the robotic camera appeared to consist of ore, slag, and native soils. There was no evidence of P4 in the sediment. This pipe as observed from Manhole #1 is assumed to be 50% full of sediments.
- The piping segment from Area Inlet #1 to Area Inlet #3 While historical plant drawings indicate that the piping segment from Area Inlet #1 to Area Inlet #3 exists, visual investigation of the vault at Area Inlet #1 did not reveal the presence of a pipe entering from the south only a pipe running towards the north to the East Discharge. Similarly, visual investigation of the vault at Area Inlet #3 only revealed pipes connected on the south side (from Manhole #1) and west side (toward Area Inlet #4); no pipe leaving to the north towards Area Inlet #1 was present. Whether the historical drawing was incorrect or had not been updated to reflect later removal of the pipe segment cannot be determined; regardless, there is no observable evidence that a segment of piping is present between Area Inlet #3 and Area Inlet #1. Therefore, this segment was not present to survey.

2.2.3 Equipment Decon and Waste Determination

After each segment was surveyed (or attempted to be surveyed), the robotic camera or cable camera were decontaminated as removed from the piping. The cameras and cables were decontaminated using water and brushes to mechanically remove the contaminants. The decon water was collected in a plastic drum. The removed materials appeared to be primarily ore, slag, and native solids. There was no evidence of P4 (i.e., no observed smoking). The decon water and sediments were separated and sent to a laboratory for waste determination analysis. The results of the analyses are presented in Appendix G. Based upon observations, process knowledge, and the laboratory analyses, the decon water and sediments removed from the video equipment were determined to be non-hazardous and were managed pursuant to the Work Plan.

Findings and conclusions of the video survey are presented in Section 4.4.

2.3 VEGETATION TRIAL PLOT SAMPLING

In order to provide site-specific information associated with root depth and density, sampling was performed on FMC's former vegetation trial plots to provide an estimate of these parameters for use in performance modeling of the ET cover. Prior to laying out the sampling grid, test holes were excavated with a shovel to identify an area containing at least 18-inches of soil. Once identified, a 25 ft by 25 ft transect was measured. The transect was further divided into 5 ft by ft sampling grids. Three randomly placed hand-auger borings were advanced within each sampling grid and samples were collected at 6-inch increments (e.g. 0-6", 6-12", etc.). In general, top

soil sampling was possible to a depth of 18-inches in the majority of soils with some locations only having top soil depth to 12-inches before contacting the underlying slag. The vegetation sampling grid is shown in Figure 2-3.

3.0 Laboratory Testing and Results

Following sample collection, the soil samples from the WUA, vegetation trial plot samples, and stormwater sewer piping were sent off for laboratory testing and analysis as described below.

3.1 WESTERN UNDEVELOPED AREA SOIL TESTING

3.1.1 Geotechnical Testing

Following collection of the disturbed (composite) and undisturbed samples, the samples were sent to IGES out of Salt Lake City for geotechnical and hydrological testing. The following tests were performed to further define the geotechnical properties of the soil:

Disturbed (composite) samples from test pits:

- Atterberg Limits (American Society of Test and Materials [ASTM] D4318) testing was
 conducted to evaluate the shrink-swell potential of the soil and its propensity to develop
 desiccation cracks during cyclical wetting and drying.
- Standard Proctor (ASTM D698) testing was conducted to further refine the maximum dry density (MDD) and optimum moisture content (OMC) of the soil to be used for specifying the percent compaction and in-place density of the soil.
- Particle size distribution testing (ASTM D422) was conducted to provide an indicator of material properties across the entire borrow area.
- Crumb and double hydrometer dispersion testing (ASTM D6572-12 and ASTM D4221-11) were conducted to evaluate the erosive potential of the soil due to dispersion.

Undisturbed samples from borings:

- In-situ density (ASTM D7263-09)
- In-situ moisture content (ASTM D2216-10)

The geotechnical tests and associated results performed on the grab samples collected from each test pit are summarized in Table 3.1. The laboratory report for the geotechnical tests are presented in Appendix D.

3.1.2 Hydrological Testing

The following tests were performed to determine the saturated and unsaturated hydrological properties of the borrow soil based on test pit samples and two boring samples (SB007 at 6' to 8' and 12' to 14' bgs):

- Saturated Hydraulic Conductivity (ASTM D5084)
- Water Characteristic Curve Testing (ASTM D6836)

The hydrological tests performed on the grab samples collected from each test pit and associated results are summarized in Table 3.2. The laboratory reports for the hydraulic tests are presented in Appendix D.

Table 3.1 Summary of WUA Soil Geotechnical Testing and Associated Results

Soil Test	TP001	TP002	TP003	TP004	TP005	TP006	TP007	TP008	TP009	TP010	SB003	SB004	SB006	SB007	SB008
Standard Proctor Compaction Test (MDD lbs/ft³) (ASTMa ¹ D698)	106.9	97.7	107	106.4	107.2	104.4	104.2	99.6	103.7	104.8	NA ^{b/}	NA	NA	NA	NA
Optimum Moisture Content (OMC %) (ASTM D698)	17.5	22.7	16.6	16.2	15.9	16.8	17.7	19.4	16.9	16.8	NA	NA	NA	NA	NA
Particle Size Distribution (ASTM D422)											NA	NA	NA	NA	NA
% Gravel	0.0	0.0	0.3	0.0	0.0	0.0	0.0 - 0.1	0.0	0.6	0.1					
% Sand	3.4 - 4.8	1.6 – 9.4	4.1 – 4.8	2.9 – 4.5	3.3 – 3.7	4.0 - 4.4	12.4 – 15.4	4.1 – 11.4	3.7 – 5.5	6.5 – 7.4					
% Fines	95.2 – 96.6	90.6 – 98.4	95.0 – 95.6	95.5 – 97.1	96.3 – 96.7	95.6 - 96	84.6 – 87.6	88.6 – 95.9	94.0 – 95.8	92.5 – 93.4					
Atterberg Limits (ASTM D4318)											NA	NA	NA	NA	NA
(ASTM D4318) LL ^{c/} (%)	28	36	27	N.P. f/	24	25	23	28	26	N.P.					
PL ^{d/} (%)	21	22	21		22	21	22	22	21						
PI ^{e/} (%)	7	14	6		2	4	1	6	5						
Crumb Test (D6572-12)	2 ^{g/}	2	3	1	1	3	2	2	1	1	NA	NA	NA	NA	NA
Double Hydrometer Dispersion Test (D4221-11) (% Dispersion)	22.5	24.8	44.3	33.9	32.1	38.0	37.4	18.6	29.7	24.4	NA	NA	NA	NA	NA
In situ Density	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	90.8 (0' to 2')	77.5 (2' to 4')	80.2 (2' to 4')	70.4 (2' to 4')	79.3 (2' to 4')
(lbs/ft ³)												78.1 (6' to 8')	81.7 (6' to 8')		77.3 (6' to 8')
(ASTM D7263-09)														85.3 (12' to 14')	
In-situ Moisture	NA	NA	NA	NA	NA	NA	NA	NA	NA	NA	4.9 (0' to 2')	4.8 (2' to 4')	15.1 (2' to 4')	15.5 (2' to 4')	8.4 (2' to 4')
Content (%) (ASTM D2216-10)												6.0 (6' to 8')	9.4 (6' to 8')	5.9 (6' to 8') 3.3 (12' to 14')	8.6 (6' to 8')
Notes:														3.3 (12 10 14)	

a' ASTM American Society of Testing and Materials
b' Not Analyzed
c' LL: Liquid Limit
d' PL Plastic Limit

e/ PI: Plasticity Index

f/NP: Non-plastic

Table 3.2 Summary of WUA Soil Hydrological Testing and Associated Results

Test Pit/Boring I.D.	$\mathbf{K}_{\mathrm{sat}}^{\mathrm{b/}}$		Van Genuchten	Parameters ^{a/}	
I.D.	(cm/sec)	$\alpha^{c/}$	N ^{d/}	$\theta_{r}^{e/}$	$\theta_{\rm s}^{{ m f}\prime}$
		(cm ⁻¹)	(dimensionless)	(% vol)	(% vol)
TP001	3.3E-05	1.0624	1.2659	0.0207	0.5257
TP004	1.4E-04	1.7409	0.2293	0.0431	0.4417
TP006	2.3E-05	0.5592	1.3116	0.0191	0.4776
TP007	5.8 E-05	0.8571	1.3562	0.0409	0.4865
TP008	7.87E-05	0.6665	1.4267	0.0543	0.5219
SB03 (2-15 feet)	2.6E-06	NA ^{t/}	NA ^{t/}	NA ^{t/}	NA ^{f/}
SB7 (6 to 8 feet bgs)	6.2E-05	NA ^{f/}	NA ^{f/}	NA ^{f/}	NA ^{f/}
SB7 (12 to 14 feet bgs)	3.1E-04	NA ^{t/}	NA ^{t/}	NA ^{f/}	NA ^{f/}

a/ Van Genuchten Parameters for SWCC testing (ASTM 6836)
b/ K_{sat} = saturated hydraulic conductivity (ASTM D5084)
c/ α = inverse of the air-entry value (or bubbling pressure)
d/ n = pore size distribution index [dimensionless]

 $[\]theta_{\rm r} = 0$ residual water content $\theta_{\rm r} = 0$ saturated water content

g/NA = not analyzed

The DGWP specified that Soil Water Characteristic Curve Testing would be performed on disturbed samples remolded to both 85 and 90% of MDD. However, Water Characteristic Curve Testing was performed only on disturbed samples remolded to 85% MDD. The deviation was mainly due to the fact that the construction specifications for the cover soil (silt from the WUA) would target an in-place density of 85% MDD ±3%. This specification has been chosen to limit the in-place density to below 90% MDD. Therefore, Water Characteristic Curve Testing at 90% MDD was not warranted.

3.1.3 Agronomic Testing

Three (3) composite samples (CP01, CP02 and CP03), derived from the ten (10) test pits were sent off for agronomic testing. The agronomic testing was performed by ACZ Laboratories. The agronomic test performed and associated results are presented in Table 3.3. As indicated by Table 3.3, the results were consistent for the three samples. The laboratory reports for the agronomic testing are presented in Appendix E.

Table 3.3 Summary of WUA Soil Agronomic Testing and Associated Results

Analyses		Sample I.D.	
	WUA-CP01	WUA-CP02	WUA-CP03
Cation Exchange Capacity (meq/100g)	8.50	11.0	10.0
Phosphorus, total (mg/Kg)	790	780	790
Potassium, total (mg/Kg)	2410	2780	2620
Carbon, total organic (%)	0.2	0.2	0.2
Conductivity @25°C (mmhos/cm)	0.442	0.594	0.456
Organic Matter (%)	0.8	0.9	0.9
pH, Saturated Paste	8.6	8.4	8.5
Solids (%)	94.1	91.9	93.0
Nitrogen, ammonia (mg/Kg)	10.6	11.1	10.7

3.2 ROOT DENSITY TESTING

Root density testing was performed using the procedures described in the Work Plan. The results of the root density testing are summarized in Table 3.4. The laboratory report for the root density measurements are presented in Appendix F.

Table 3.4 Root Density Measurements

Sample	Grams of Roots per 100 grams of Soil
Grid #6—Location #1	grams or son
0-6 inches	0.019
6-12 inches	0.078
12-18 inches	0.003
Grid #6—Location #2	
0-6 inches	0.084
6-12 inches	0.019
12-18 inches	0.014
Grid #6—Location #3	
0-6 inches	0.032
6-12 inches	0.013
12-18 inches	0.005
Grid #7—Location #1	
0-6 inches	0.039
6-12 inches	0.020
12-18 inches	0.013
Grid #7—Location #2	
0-6 inches	0.036
6-12 inches	0.029
12-18 inches	0.021
Grid #7—Location #3	
0-6 inches	0.089
6-12 inches	0.024
12-18 inches	0.015
Grid #8—Location #1	
0-6 inches	0.102
6-12 inches	No sample
12-18 inches	0.020
18-24 inches	0.006
Grid #8—Location #2	
0-6 inches	0.076
6-12 inches	0.075
12-18 inches	0.013
18-24 inches	0.004
Grid #8—Location #3	
0-6 inches	0.048
6-12 inches	0.028
12-18 inches	0.013
Grid #13—Location #1	
0-6 inches	0.104
6-12 inches	0.036
12-18 inches	No sample
Grid #13—Location #2	
0-6 inches	0.064
6-12 inches	0.032
12-18 inches	No sample
Grid #13—Location #3	
0-6 inches	0.101
6-12 inches	0.034
12-18 inches	0.014
Grid #14—Location #1	
0-6 inches	0.087
6-12 inches	0.054
12-18 inches	0.016

Sample	Grams of Roots per 100
	grams of Soil
Grid #14—Location #2	
0-6 inches	0.109
6-12 inches	0.051
12-18 inches	0.026
Grid #14—Location #3	
0-6 inches	0.053
6-12 inches	0.040
12-18 inches	0.019
Grid #15—Location #1	2.2.5
0-6 inches	0.054
6-12 inches	0.018
12-18 inches	0.011
Grid #15—Location #2	0.055
0-6 inches	0.077
6-12 inches	0.038
12-18 inches	0.008
Grid #15—Location #3	0.000
0-6 inches	0.060
6-12 inches	0.023
12-18 inches	0.013
Grid #16—Location #1	0.060
0-6 inches	0.069
6-12 inches	0.051
12-18 inches	0.016
Grid #16—Location #2	0.110
0-6 inches	0.118
6-12 inches	0.044
12-18 inches	0.023
Grid #16—Location #3	0.083
0-6 inches	0.083
6-12 inches 12-18 inches	0.030
Grid #17—Location #1	0.018
0-6 inches	0.093
6-12 inches	0.024
12-18 inches	0.013
18-24 inches	0.005
Grid #17—Location #2	0.003
0-6 inches	0.052
6-12 inches	0.020
12-18 inches	0.015
18-24 inches	0.002
Grid #17—Location #3	0.002
0-6 inches	0.037
6-12 inches	0.037
12-18 inches	0.015
18-24 inches	0.006
Grid #18—Location #1	0.000
0-6 inches	0.014
6-12 inches	0.018
12-18 inches	0.003
Grid #18—Location #2	0.000
0-6 inches	0.068
6-12 inches	0.023
12-18 inches	0.013
Grid #18—Location #3	
Ora ii o Location ii o	ļ.

Sample	Grams of Roots per 100 grams of Soil
0-6 inches	0.041
6-12 inches	0.022
12-18 inches	0.011

As indicted in Table 3.4, 3 discrete interval samples were not analyzed. The two Grid # 13 samples collected at an interval of 12- 18-inches were not sent to the lab due to the presence of shallow slag, which precluded obtaining a hand-auger sample. The sample associated with Grid #8 for the 6 to 12 inch interval was not analyzed because the quart size bag sample bag was reported as torn when received at the laboratory and was evidently damaged during shipment. All other samples were inspected upon arrival and determined to be intact.

4.0 Data Gap Findings and Conclusions

This section presents recommendations for the design parameters to be used in the Remedial Design (RD). ProUCL 5.0 Statistical Software was used to calculate the means for the design parameters shown in the table below. The results of the ProUCL analysis are presented in Appendix H. As shown in Appendix H, the data for the geotechnical and hydrological parameters were generally normally distributed and hence the use of mean values for these parameters in the remedial design is appropriate.

4.1 GEOTECHNICAL RECOMMENDATIONS

The main purpose of the geotechnical testing was to define appropriate design parameters of the WUA borrow soil for use in ET soil cover modeling, to estimate volume of soil required from the WUA, and evaluate the WUA soils susceptibility to erosion and desiccation cracking. The proposed geotechnical design parameters for the WUA borrow soil are summarized Table 4.1.

Table 4.1 Recommended Geotechnical Design Parameters for WUA Borrow Soil

Parameter	Value
MDD (lbs/ft³) per ASTM D698	104.2 (mean)
OMC (%) per ASTM D698	17.1 (mean)
In situ Density (lbs/ft3) per ASTM D7263-09	81.1 (mean)
In-situ Moisture Content (%) per ASTM D2216- 10	8.7 (mean)

A review of particle size distribution curves and Atterberg Limits, which are known to be key soil index properties, suggest that the silts within the WUA are very uniform. Although disturbed grab samples were not collected at depths deeper than 10 feet, visual observations of the silts below 10 feet in test pits and soil borings indicate that the soils are uniform in terms of soil color, texture, plasticity, and gran size. Therefore, the physical properties of the silts at deeper depths are adequately represented by the grab samples collected to a depth of 10 feet.

Atterberg limits and dispersive testing was performed on the majority of disturbed samples to assess the potential for desiccation cracking and erosion of the silts. Based on the Atterberg limits testing, the plasticity index (PI), ranged between 1 and 14. These results indicate that the soils have very low-plasticity and therefore are not susceptible to desiccation cracking associated with volumetric changes (shrinkage) induced by moisture fluctuations. The results of the dispersion testing both (Crumb and double hydrometer testing) indicate that the soils are generally non-dispersive to moderately dispersive based on Crumb test results characterizing the

majority of samples being between a Grade 1(non-dispersive) and 2 (intermediate) and double hydrometer testing ranging between 18.6 and 44.3 percent dispersion. Therefore, based on these results, there is nothing to preclude the WUA soils being used as capping soil.

4.2 HYDROLOGICAL RECOMMENDATIONS

The main purpose of the hydrological testing was to define appropriate design parameters of the WUA borrow soil for use in the modeling of the ET soil cover. The proposed hydrological design parameters for the WUA borrow soil are summarized Table 4.2.

Table 4.2 Recommended Hydrological Design Parameters for WUA Borrow Soil

Parameter	Value			
Hydraulic Conductivity (cm/sec) per ASTM 5084	6.57E-5 (mean)			
Van Genuchten Parameters (per ASTM 6836)				
α (cm)	0.97722 (mean)			
n (dimensionless)	1.11794 (mean)			
θ_{r} (%vol)	0.03562 (mean)			
θ _s (%vol)	0.49068 (mean)			

4.3 ROOT DENSITY RECOMMENDATIONS

The main purpose of the root density testing was to provide a quantification of the vegetation quality that can be established for use in the ET soil cover modeling. Based on the ProUCL analysis presented in Appendix H, a mean was selected resulting in a design root density value of 0.051 grams of roots per 100 grams of soil.

4.4 STORMWATER SEWER VIDEO SURVEY FINDINGS

A summary of the stormwater sewer piping video survey is provided in Table 4.3 presenting the total volume of solids expected to be removed, characterized, and disposed as result of the RA-A stormwater sewer pipe cleaning. While the video survey did not identify any P4 present in the stormwater sewer piping, all precautions will be taken during cleaning of the piping in the event P4 is encountered. Also, while the waste determination performed on the decon water and sediments collected during the video survey indicated that the water and sediments were non-hazardous, wastes generated during the cleaning of the stormwater sewer piping will be fully characterized.

4.5 BORROW SOURCE AVAILABILITY

In addition to collecting disturbed and undisturbed soil samples, the WUA soil investigation was also used to characterize the approximate quantity of borrow soil available for use during the remedial action. The depth information obtained from the soil boring and test pit were used to develop an isocontour map of the depth of silt throughout the WUA and is presented in Figure 4-1. Based on Figure 4-1, there is approximately 2.4 million CY of soil (silt) available for use in the ET and Gamma soil covers. The preliminary required soil volume based on a 12-inch gamma cap and 30-inch ET cover is approximately 1.3 million CY. Therefore, there is ample soil available in the WUA to support the RA.

Table 4.3 Summary of Stormwater Sewer Piping Video Survey

Piping Segment	Total Segment Length (ft)	Pipe Construction	Pipe OD/ID (in)	Total Segment Volume (ft³)	Percent Full of Sediment %	Maximum Sediment Volume to be Removed per Segment 1 (ft ³)	Evidence of P4?
West Discharge to Area Inlet #1	129	concrete	16/11.5	93	70	65	No
East Discharge to Area Inlet #1	85	concrete	16/11.5	61	10	6	No
Area Inlet #4 to Area Inlet #3	107	concrete	16/11.5	77	100	77	No
Area Inlet #4 to Area Inlet #2	170	steel	8/7.98	60	70	42	No
Area Inlet #5 to pipe junction	180	steel	8/7.98	62	70	43	No
Manhole #1 to Area Inlet #3	169	concrete	16/11.5	122	50	61	No
Total Maximum Sediment to be Removed						294	

¹ This "maximum" sediment volume is a conservative estimate for waste management planning purposes.

5.0 REFERENCES

EPA, 2012. Interim Amendment to the Record of Decision for the EMF Superfund Site - FMC Operable Unit - Pocatello, Idaho (IRODA), September 27, 2012.

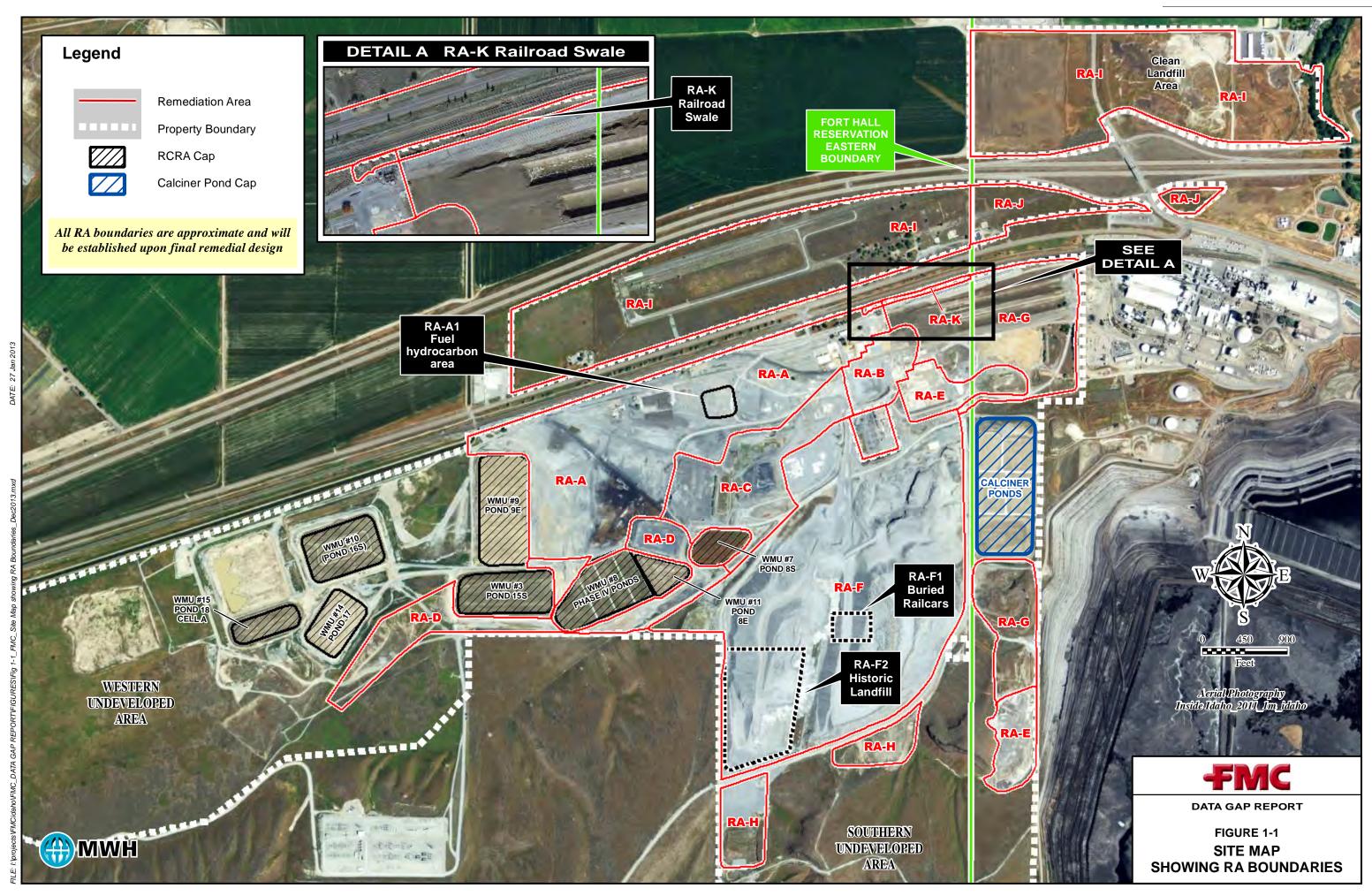
EPA, 2013. Unilateral Administrative Order for Remedial Design and Remedial Action, EPA Docket No. CERCLA-10-2013-0116 (UAO for RDRA), June 10, 2013.

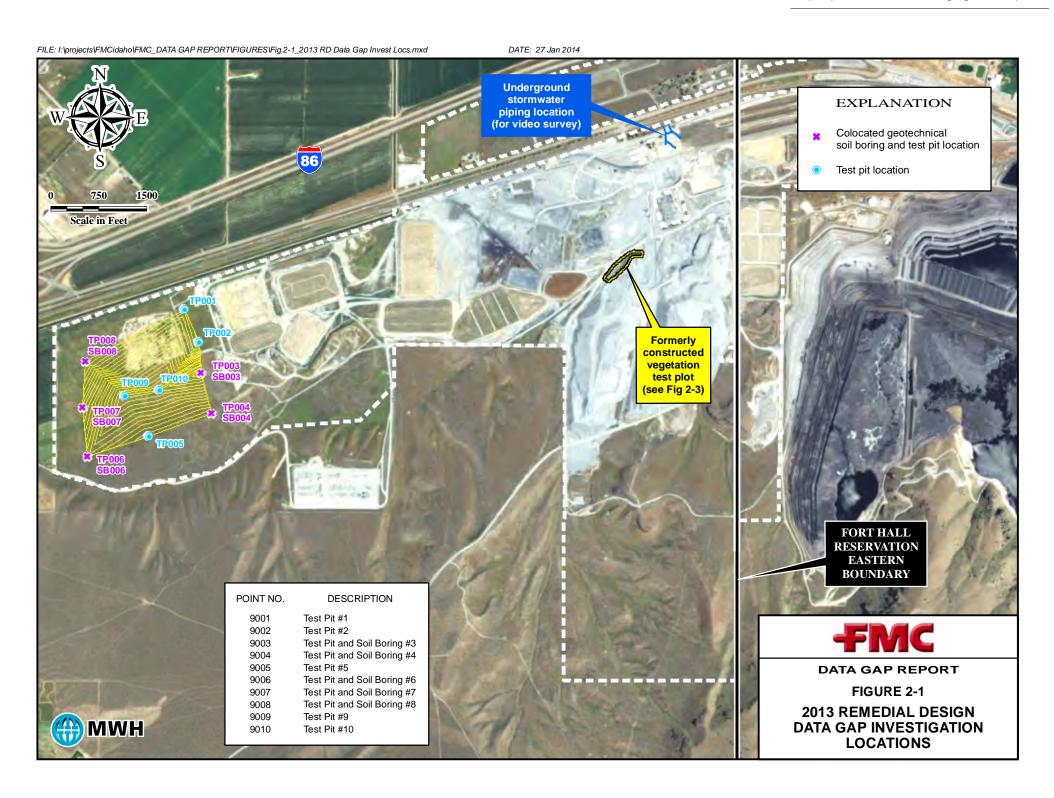
MWH, 2010. Supplemental Feasibility Study Report for the FMC Plant OU, MWH Americas, Inc., July 2010.

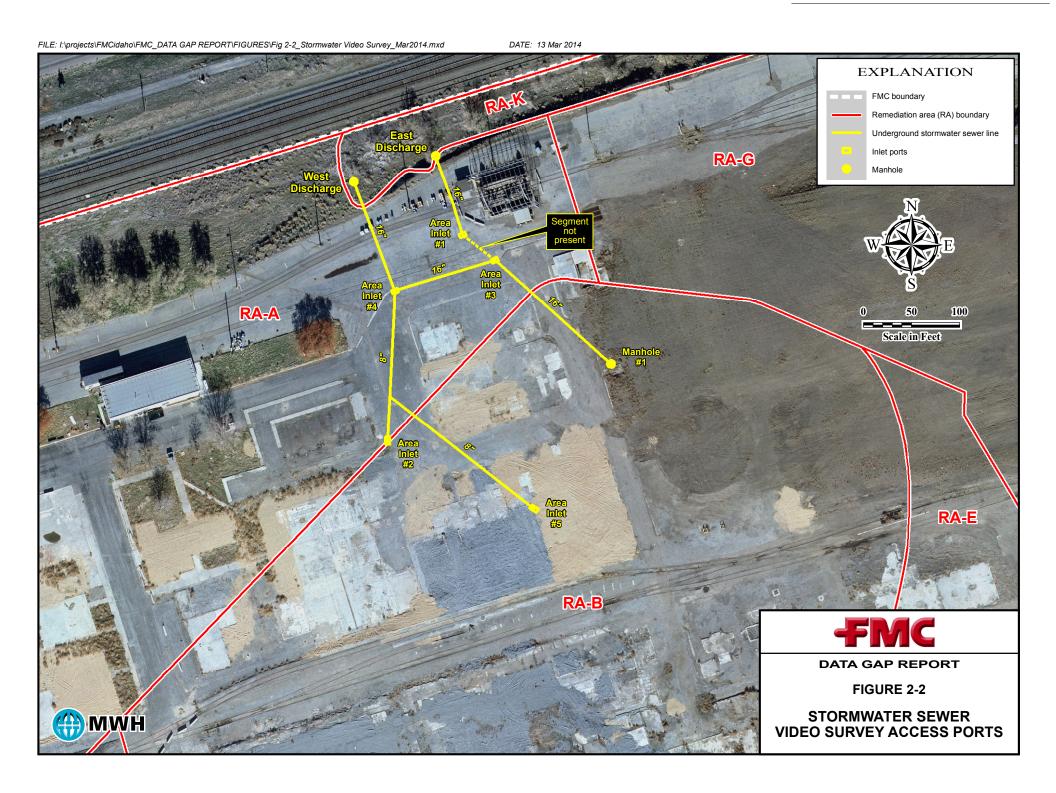
MWH, 2013a. Remedial Design Work Plan, MWH Americas, Inc., August 2013.

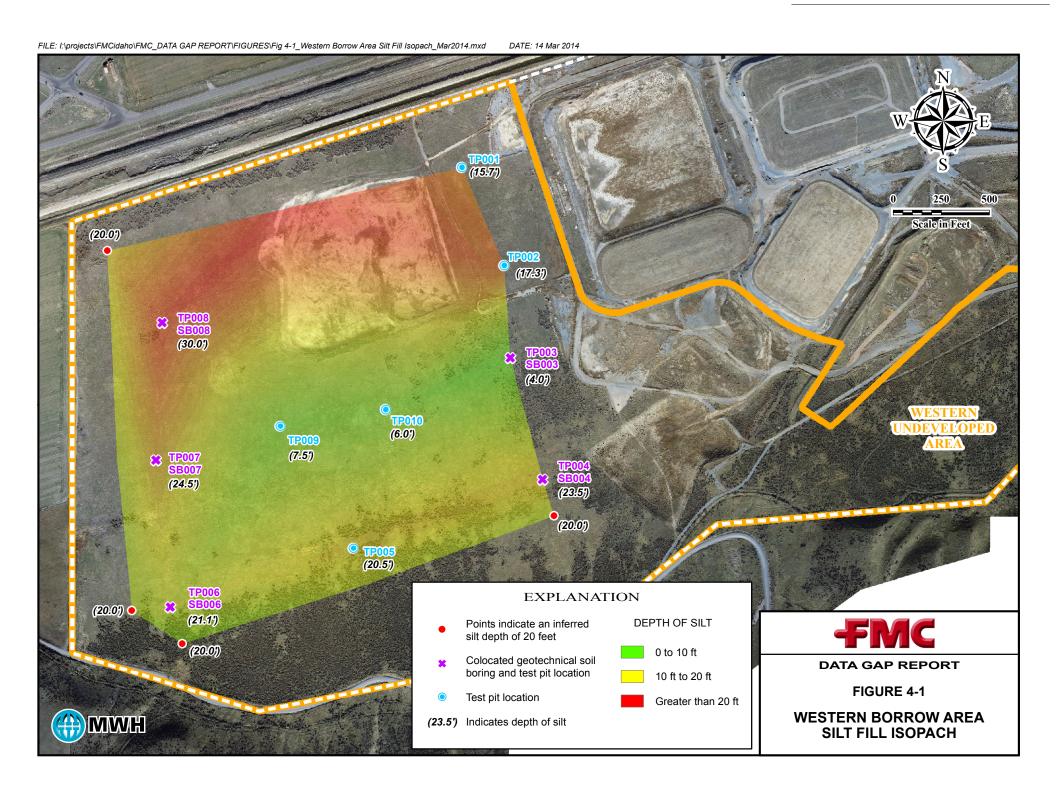
MWH, 2013b. Remedial Design Data Gap Work Plan, MWH Americas, Inc., October 2013.

Figures









APPENDIX A

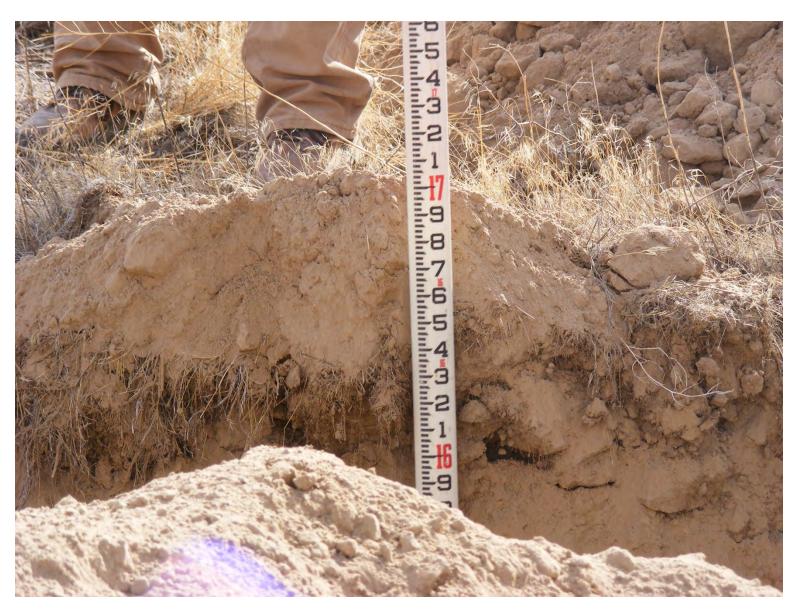
Field Investigation Photographs



Photograph 1 (taken 10/29/2013) – Looking at base of excavation in TP001.



Photograph 2 (taken 10/29/2013) – Looking at shallow gravels contacted in TP003.



Photograph 3 (taken 10/29/2013) – Looking at depth measurement taken at the base of TP004.



Photograph 4 (taken 10/30/2103) – Looking at base of excavation in TP005.



Photograph 5 (taken 10/30/2013) – 6-inch minus gravels excavated from TP009 encountered at 7.5 feet bgs.



Photograph 6 (taken 11/12/2013) - Core taken from SB004 showing silt borrow material collected from 20 to 21.5 feet bgs.



Photograph 7 (taken 11/12/2013) - Core taken from SB004 showing gravels collected from 25 to 26.5 feet bgs.



Photograph 8 (taken 11/13/2013) – Looking southwest at hollow-stem auger drill rig at SB008.



Photograph 9 (taken 11/06/2013) – Looking south at video survey equipment in 16-inch reinforced concrete pipe in entrance to East Discharge.



Photograph 10 (taken 11/06/2013) – Video survey equipment lowered into manhole.



Photograph 11 (taken 11/06/2013) – Video survey control room.



Photograph 12 (taken 11/06/2013) – Decontamination of video survey equipment.

APPENDIX B

Test Pit Logs

Project / No. Sample Loca Coordinates Slov	TRENCH TEST PIT LOG FORM Project Number 10 S 0 3 3 1 1 Trench Number TP 00 7 Date 16/ Project Number TP 00 7 Date 16/ Outside Stake 547/60. 5 Native Fill Stake 4482.9 Chad Tealinson	age of
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WEATHER

DAILY QUALITY CONTROL REPORT

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PERSONNEL AND SUBCONTRACTORS ON SITE:
KW: Mark Smith, Rick, Tribe: kelly Wright MWH: Chad Tonlinson Booze
MWH: Chad Tonlinson Booze
VISITORS ON SITE:
EQUIPMENT ON SITE: Trackhoc frontend loader, shotels, buckets
WORK PERFORMED (INCLUDING SAMPLING):
Excavated TP001, TP002, TP003, TP004, TP005 and TP006. Collected gamples from every 1ft interval down to approximately 10ft. Filled 2 5-gallon buckets at each test pit. Continued excavation below 10ft while uderlying gravels reached ar depth of excavator met. Gravels contacted in 2 test pits: 1) TP001 Q 15.7 ft
interval down to approximately 10 ft. Filled
2 5-gallon buckets at each test pit. Continuel
reached or dooth of excavator met. Gravels
contacted in 2 test pits: 1) TPOOL @ 15.7 ft
and 2) TP003 @ 4 ft, TP002, TP004, TP005
and 2) TP003 @ 4 ft, TP002, TP004 TP005 and TP006 excavated to total depth of excavate generally around 17.5 to 20 ft bgs. #P
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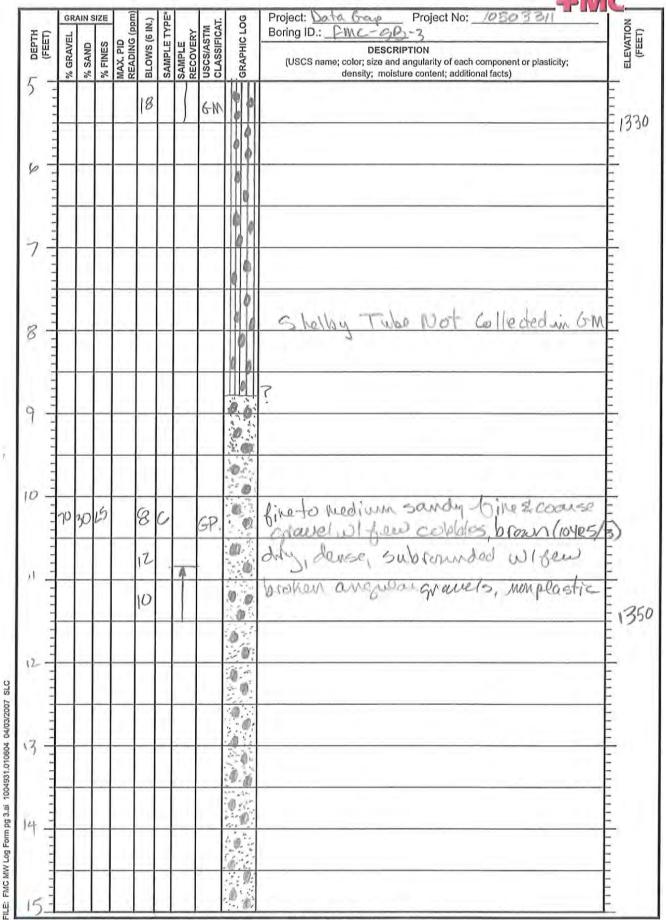
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APPENDIX C

Soil Boring Logs

						7	otal C	deasur Depth (ter (in.	ft.):		Drilling Contractor: Cong Tec/ Jeff Drilling Method: +13 fr	
						-	band	onmer	t Inf	orm	nation: 13ack filled with soil Cuttings	
(FEET)	% GRAVEL S	% SAND	% FINES	MAX. PID READING (ppm)	BLOWS (6 IN.)	SAMPLE TYPE*	SAMPLE	USCS/ASTM CLASSIFICATION		GRAPHIC LOG	DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts)	
1141111111	ø	15	100			July Tube 15 PAME		ML			self (ML) light away (104R 7/2) slightly to low plasticity, dry, few posts and organics, medium stiff	17
Present						S.M.S.						
1	70	5	30					3M			Pushed shelloy Tube 0-2 in second boring throch @ 2' bgs unable to drive shelloy Tube from 2-4'	
11444							-		0	80	Silly fine & coarse grave (GN)	
I Link							l I		-	9	Medium donce dry, subtramped	
DEC LO									0	0	when sub angulad gravels	
								GM	0 0	-	Shelly Tube Not Collected in 6m	
1.1.1.1	70	15	P		15	C			0	9		
1.1.1.1					25		4		0	0		







PAGE 2 OF 4

7.6		RAIN	SIZE	(mdd)	6 IN.)	TYPE*	<u>خ</u>	TM CAT.	907:	Project: Data Gap Project No: 10503311 Boring ID.: CMC-36-3	NOIT:
DEPTH	GRAVEI	% SAND	% FINES	MAX. PID READING (ppm)	BLOWS (6 IN.)	SAMPLE	SAMPLE	USCS/ASTM CLASSIFICAT.	GRAPHIC LOG	DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts)	(FEET)
15					12						= 1 inc
	1	30	10		14		*	GP		As Above w/ some self (10%)	
16	1				16			Ī	00		E 1411
	11111						-1-		0		E
17	9								0		Ē
1	3								0.0		
18	1								0		
									0		E E
19	1475								0		
	PICT I					-			0		
20	=50	40	10		5	C		68	9	fireto coarse sandy five si coarse gravel, maisly five i vousel, yourse brown crove s/4) dry, new place	
	11111				5			0.		Yorlowsh brown (104R s/4) dry, new place	E Bic
21	1111				6		*		0.0	dange, subrounded.	
	1111						+				E1419
22	1								0		
									0		
23				Ħ					0		
									服		
24.									0		
25									0		

(#) WWH

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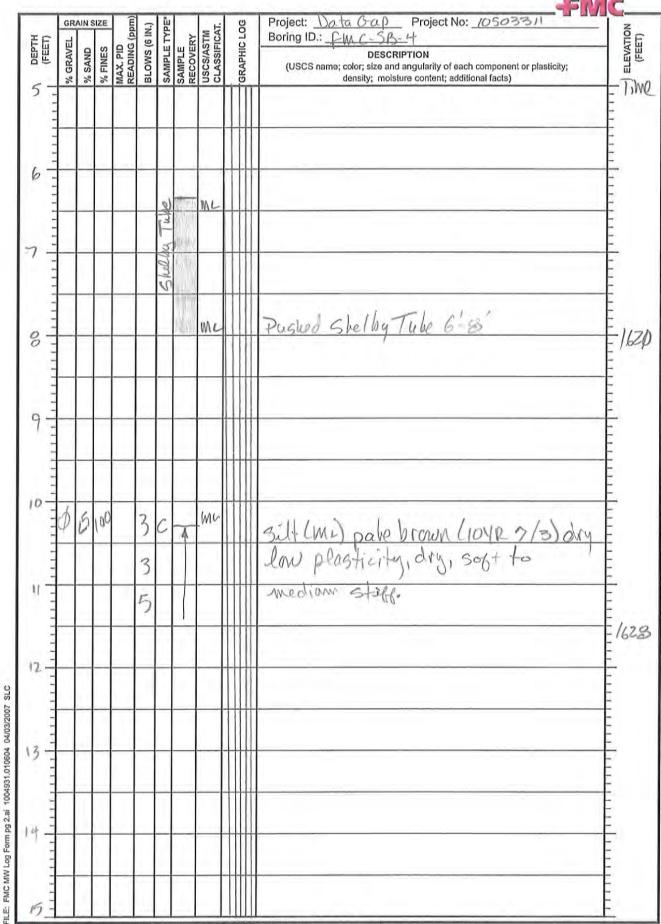
MAX. PID READING (ppm) Project: Data Gap Project No: 1050331 SAMPLE TYPE* SAMPLE RECOVERY USCS/ASTM CLASSIFICAT. **GRAPHIC LOG** BLOWS (6 IN.) ELEVATION FMC Boring ID .: _ (FEET) DEPTH (FEET) % GRAVEL % SAND % FINES DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts) Time 0 26 1427 medium stiff to stoff. Crumbles under weak binger pressure. 30 5 C 0 WIL 6 -1437 8 boring 32-FILE: FMC MW Log Form pg 3.ai 1004931.010604 04/03/2007 SLC

MWH

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							Logge Water	ed By: Eleva Measu	tion	(ft.):	13 Date Completed: 11 12 13 Northing: 44 8 19 6 6 Easting: 54 9 7 7 1 6	
								Depth eter (in		_	Drilling Contractor: Cove Tec/ John Prilling Method:	
						-			415	nform	nation: Backfilled with Soil Cultives	
DEPTH (FEET)	% GRAVEL B	% SAND	% FINES	MAX. PID READING (ppm)	BLOWS (6 IN.)	SAMPLE TYPE*	SAMPLE RECOVERY	USCS/ASTM		GRAPHIC LOG	DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts)	STELEVATION
1111111	p	5	100			SAR		Mc			self (ML) light aron (10412 7/2) - seightly to low prosticity, ary, few roots and organies, medium	
11111111											Stiff	
2						2 125		MC				
3						Shall						
4								ML			Pushed Shellog Tube 2'-4'	-15
5												





MWH

PAGE 2 OF 4

MAX. PID READING (ppm) Project: Data Gop Boring ID.: PMC SB-4 Project No: 10503311 SAMPLE RECOVERY USCS/ASTM CLASSIFICAT. SAMPLE TYPE GRAPHIC LOG ELEVATION (FEET) BLOWS (6 IN.) DEPTH (FEET) % GRAVEL % SAND % FINES DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts) ML Self (mi), pale brown (104R7/3) dry 8 to stiff. 10 -1645 18 C 15 100 ML Silt (Mi) pale brown (104R713) dry, low to slightly plastic, medium Stiff to stiff. 1654 FILE: FMC MW Log Form pg 3.ai 1004931.010604 04/03/2007 SLC harder drilling about 23.5' Estimated topol Gravel. 0 0 0 =

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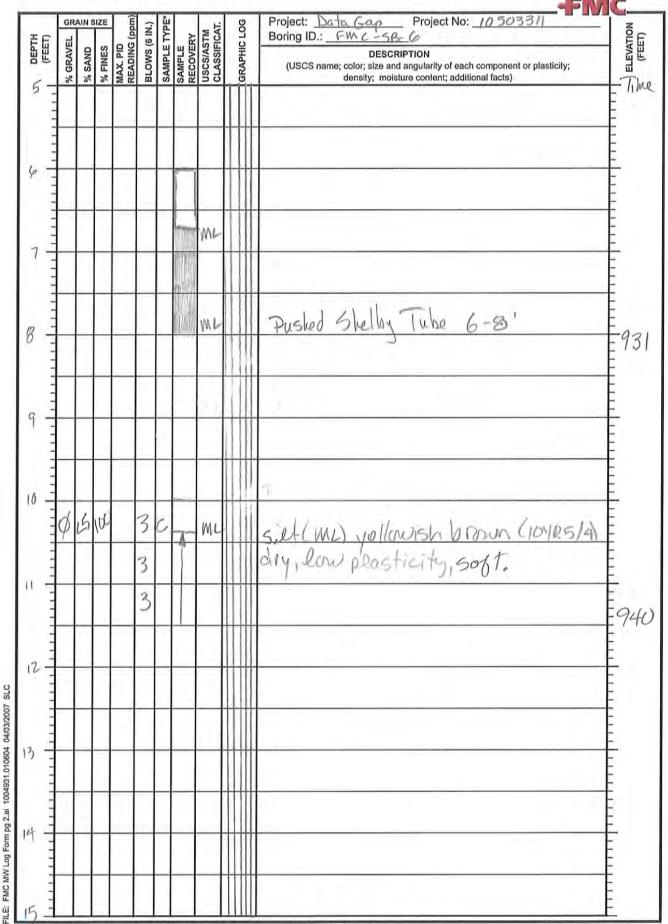
MAX. PID READING (ppm) Project: Data Gap Project No: 10503311 SAMPLE TYPE GRAPHIC LOG ELEVATION (FEET) BLOWS (6 IN.) USCS/ASTM CLASSIFICAT. Boring ID .: FMC SAMPLE DEPTH (FEET) % GRAVEL % FINES % SAND DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts) 0 C gravel (6P) w/ few cobbles, Pale brown 0 -60 30 10 b CIOYR 7/3), dry, non plastic to -1720 slightly plastic where silty, 4 80 28 0 ŏ 0 0 0 10 0 30. 0 0 30 10 6 00 GP grave 1 (GP), Pale brown (101B) aru, non plastic, medium de 19 TO 30' w/ HSA 31.5' w/splitso. Bock filled with soil cuttings 0 Brown boring -FMC MW Log Form pg 3.ai 1004931.010604 04/03/2007 SLC



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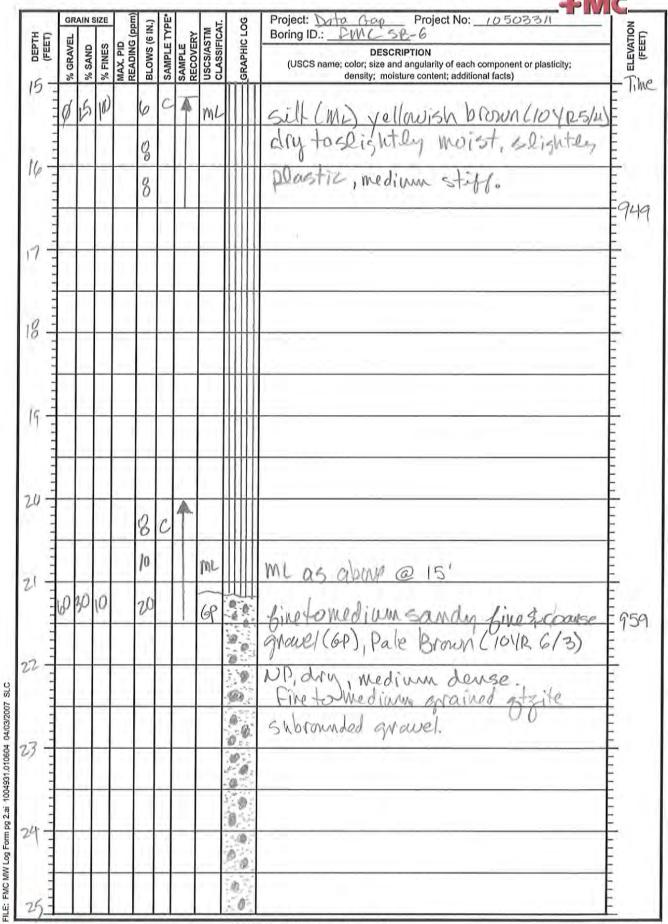
							Water Date N	Elevat deasur epth (red	i (it.):	Ground Surface Elevation (ft.): 4454.9 Datum: NGVD (1988) 30' Drilling Contractor: CNO TEC Soft	
						1	Diame	ter (in.)_	_	Brilling Method:	
							Aband	onmer	it I	nform	mallon: BOCK filled with soil cuttings.	
DEPTH (FEET)	% GRAVEL S	% SAND	% FINES	MAX, PID READING (ppm)	BLOWS (6 IN.)	SAMPLE TYPE*	SAMPLE RECOVERY	USCS/ASTM CLASSIFICATION		GRAPHIC LOG	DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts)	CONTRACTION (FEET)
	Ø	15	100			35.50		ML			SIH (MA) Dightoran (10 YR 7/2) to	1111
1.1.4.4.1											Silf (ML) light gray (10 YR 7/2) to Pale brown (10 YR 7/3) plighty to low plasticity, medium stiff, few roots and organics.	
1 7										H	roots and organics.	
TO TOTAL	1.5				-					H		
2												
1111								ML				1111
					Ī	1 NWC	1					1111
3-					11.11	SKELDS						De care
14								N			Dushed Shelby Tube 2'-4'	
1111												-90 -
						1						
5-					1					Ш		Ξ,





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Project: Dota Gap Boring ID.: CWC SA 6 Project No: 105033/1 SAMPLE TYPE SAMPLE RECOVERY USCS/ASTM CLASSIFICAT. GRAPHIC LOG BLOWS (6 IN.) ELEVATION (FEET) DEPTH (FEET) % GRAVEL DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts) 0 THATE 13 c GP . 0 0 0 0 As Above @ 21'bgs 30 60 -1022 Sepi--00 a0 ... 6 00 60 20 40 0 0 00 0. 0. à 30 4 SP 10 0 00 18 000 20 60 30 10 50il cultings prom boring. 1035 FMC MW Log Form pg 3.ai 1004931,010604 04/03/2007 SLC

MWH

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	ORIN	GLO	CAT	ION	(4)	-	Date I Logge Water	ct: \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	tion	(ft.):	Project No: 1030331 Boring ID: WC-313-7 Date Completed: 11/13/13 Northing: 44 3 295 Easting: 5 4 160.5 Ground Surface Elevation (ft.): 44 5 2-9 Datum: NGVD (1988)	MC
								Depth (_	Drilling Contractor: Conclude Tell	
						-			-	form	ation: Backfilled with Soil Cuttings	
O DEPTH (FEET)	% GRAVEL S	% SAND % FINES		MAX. PID READING (ppm)	BLOWS (6 IN.)	SAMPLE TYPE*	SAMPLE	USCS/ASTM CLASSIFICATION		GRAPHIC LOG	DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts)	ELEVATION
	φ	15	(d)			GARB		ML			Silt (ML) pale brown (10/R 6/3) Slightly to low plasticity, medium Stiff, drg.	110.
T. C.								ML				
2						- Was	100	ML				
3						Shellber						
4								WL			Pushed shellby Tube Z-4'	- [[1]
5-1												



SAMPLE TYPE*
SAMPLE
RECOVERY
USCS/ASTM
CLASSIFICAT. Project: Data Gap Pr Boring ID.: PMC-SB 7 Project No: GRAPHIC LOG ELEVATION (FEET) BLOWS (6 IN.) DEPTH (FEET) DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts) TIME ML She WL Shellby Tube 6-8' Pushod 8 -1140 -1140 10 Silt (ML) very pale brown (104R7A) dry, low to slightly plastic Soft to medium Stiff. ML 10 -1142 12 Pushed Shelby Tube 12-14' 1202

(III)

FILE: FMC MW Log Form pg 3.ai 1004931,010604 04/03/2007 SLC

PAGE 2 OF 4

DEPTH	~ [GRAI	N SI	ZE	MAX. PID READING (ppm)	BLOWS (6 IN.)	E TYPE*	E V	ASTM IFICAT.		GRAPHIC LOG	Project: Data Gap Project No: 10503311 Boring ID.: PWC-SB-7	ELEVATION
15		% GRAVEL	% SAND	% FINE	MAX. P	BLOW	SAMPL	SAMPL	USCS/ASTM CLASSIFICAT.		GRAPH	DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts)	E.E.
10	= 0	1 6	0	40		5	C	A	ML 5M			Silty fine to coarse sand (SM)	E '
16	1111				1	7				il;	III Eri	Silty fine to coarse sand (SM) Pele Brown (101R6/4), day Non plastic to slightly plastic where silty	Ē
1 p	TITLE					6					111	Non plastic to slightly prostic	12
	1111			ĺ				-					-10
17	=	Ì	Ī							1	1		Ē
	1	+		1							#		
18.	-	+	+	+	-					1	#		ılı.
		+	+	-							11		
19 -	1	+		-							Ī		au la
		1	-										
10 -	1111									1	11.		
	0	L	Sic	P		7	c	1	Mr	1		Sullui pale brown (101/26/4)	
71	1.1.1.					6				1	H	dry, low to slightly plastic medium	1
21 -	-		Ī		1	12				11	土	Stiffto stiff.	-12
		T	Ī	Ī									
22-	-	t	-	t			+			1	1		
		-	H		+	1	+		-	1	1		
13-	-	-		+	+	+	+			+			
					-		1			1	Ē		
24-										Y	1		
										11	7		
									SP	大阪	-	Harder drilling. Estimated	

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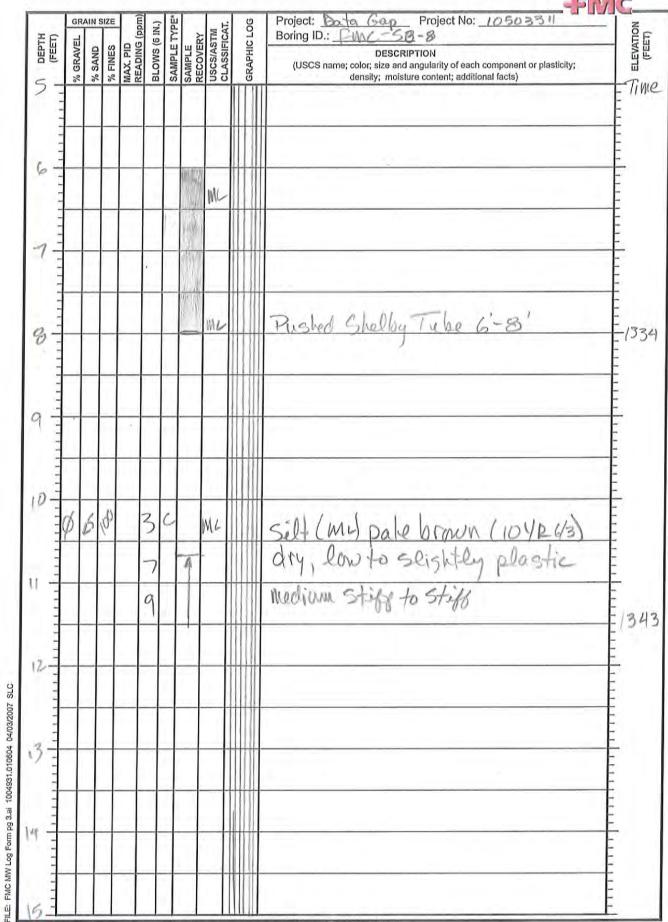
E E	. —	RAIN	T	(mad)	6 IN.)	TYPE*	3	TM ICAT.	507	Project: Data Gap Project No: 10503311 Boring ID.: +MC 68-7	NO.
DEPTH (FEET)	% CDAVE		% FINES	MAX. PID READING	BLOWS (6 IN.)	SAMPLE TYPE	SAMPLE	USCS/ASTM CLASSIFICAT.	GRAPHIC LOG	DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts)	ELEVATION
25	= 60	40	15		38			GP	00	fine to course gandy fine Ecourse	E7
26-	1110				U		4			grave (GP) eight gray (104 R 6/2)	E
CV					21					fine to coarse gandy fine Écoarse gravel(6P) eight gray (104P6/2) nun plastic, dry, medium dense to dense, subrounded.	= 12
27-											=
21				Ш					B (2)		
70-									Ø		
28-	1111								(B)		1111
									B 9		1111
29									60 B		
201									90:		1111
30	B	30	U		14	c		38		line to coarse sandy line & coarse	1111
					18	-	A	_	Ø	graver (COP) Wsome Bill Jew cobbles	
1					21				8.9	generally light opray(10/26/2) to yellowish brown (10/25/4) dry, medium dense, subsounded	- - - -
										dry, medium dense, subtranded	
										d	Litte
										TD W/HSIA 30' TD W/Samples 31.5' Back Billed W/Soil from boring.	HILL
11111											
1000											
1111			1	+		1					



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							Logge Water	Orilled: d By: Elevat Measur	ion (ft.	WA					
								epth (i ter (in.	30' Drilling Contractor: CONTEC / Jeff Drilling Method: 45th	-					
							Abandonment Information: Back filled with soil Cuttings.								
O DEPTH (FEET)	% GRAVEL B	% SAND	% FINES	MAX. PID READING (ppm)	BLOWS (6 IN.)	SAMPLE TYPE*	SAMPLE	USCS/ASTM CLASSIFICATION	GRAPHIC LOG	DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts)	-) ELEVATION				
	ø	5	100			GRAB		MC		Silt (Mr) pale brown (104R6/3) to yellowish brown (104R514), slightly woist, slightly to low plasticity,	- 13				
1 -										medium Staffitew roots & organics					
7															
11111					Ц			ML			-13				
3											-				
11111							Paralle Land				-				
w]								ML		Pushed Shelloy Tube 2-4'	132				
5															





MWH

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C DEPTH (FEET)	% GRAVEL 9	SAND	% FINES	MAX. PID READING (ppm)	BLOWS (6 IN.)	SAMPLE TYPE*	SAMPLE	USCS/ASTM CLASSIFICAT.	GRAPHIC LOG		Project: Data Gap Project No: 10503311 Boring ID.: PWC-SB-9 DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts)	ELEVATION
15-	Ø		100	100	4	100	A	ML				Fin
					6						Silt (Mi) pale brown (1018 6/3) low to seightly plastic, dry, soft to wedium stiff	
(6					8						306+ to wedium stiff	13
7												=
,,,												
18	Ī											E
, ,												
19												E
11111				Ĭ								Ē
20-												
101111	Ø	13	(VO		8	C	4	MU			Silt CML) sale brown (10110 6/3) low to seightly plasticity, dry, wedium	
2					7							
					9						stiff.	E E 140
น												and,
23						1						
			_			-						
24 =			_	_								-
3			1	_	-	1				_		
25=												Ē

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% FINES MAX. PID READING (ppm) Project: Data Gap Project No: 10503311 SAMPLE RECOVERY USCS/ASTM CLASSIFICAT. GRAPHIC LOG SAMPLE TYPE ELEVATION (FEET) BLOWS (6 IN.) Boring ID .: FWC-5B-8 DEPTH (FEET) % GRAVEL % SAND DESCRIPTION (USCS name; color; size and angularity of each component or plasticity; density; moisture content; additional facts) Time Mr 9 medium Stiff to Stiff 15 -1417 27 28 30 100 13 Silt (Mc) moderate yellowish brown clove 5/4) dry, low to slightly plastic median 2 ML 13 Gravel caugh 000 GP -1440 hard the last 3" of run Backfilled with soil cuttings from boring



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APPENDIX D

Geotechnical and Hydrological Testing Reports

Water Content and Unit Weight of Soil

(In General Accordance with ASTM D7263 Method B and D2216)



Project: MWH No: 00303-014

Location: FMC RDRA Data Gap Investigation

Date: 11/27/2013

By: JDF

ole	Boring No.	SB8	SB8	SB3	SB4	SB4	SB6	SB6	SB7
Sample Info.	Sample:								
S	Depth:	2-4'	6-8'	0-2'	2-4'	6-8'	2-4'	6-8'	2-4'
	Sample height, H (in)	4.427	4.492	4.663	4.000	6.051	4.409	5.159	4.921
Weight Info.	Sample diameter, D (in)	2.885	2.882	2.883	2.884	2.884	2.882	2.882	2.883
ht I	Sample volume, V (ft ³)	0.0167	0.0170	0.0176	0.0151	0.0229	0.0166	0.0195	0.0186
/eig	Mass rings + wet soil (g)	1721.56	1721.15	1848.02	1801.18	2045.31	1763.78	1151.00	1797.87
it W	Mass rings/tare (g)	1068.76	1075.67	1087.08	1244.25	1186.90	1067.18	361.78	1111.81
Unit	Moist soil, Ws (g)	652.80	645.48	760.94	556.93	858.41	696.60	789.22	686.06
	Moist unit wt., γ_m (pcf)	85.93	83.92	95.23	81.20	82.73	92.27	89.34	81.36
er ent	Wet soil + tare (g)	768.44	738.89	477.75	661.30	430.10	524.88	587.23	354.56
Water Content	Dry soil + tare (g)	718.97	690.41	461.22	636.71	413.13	472.91	547.48	324.20
> 0	Tare (g)	126.82	124.36	124.42	124.41	128.35	127.69	123.36	128.51
	Water Content, w (%)	8.4	8.6	4.9	4.8	6.0	15.1	9.4	15.5
	Dry Unit Wt., γ _d (pcf)	79.3	77.3	90.8	77.5	78.1	80.2	81.7	70.4

Entered by:	.
Reviewed:	

Water Content and Unit Weight of Soil

(In General Accordance with ASTM D7263 Method B and D2216)



Project: MWH No: 00303-014

Location: FMC RDRA Data Gap Investigation

Date: 12/16/2013

By: JDF

le .	Boring No.	SB7	SB7			
Sample Info.	Sample:					
S	Depth:	6-8'	12-14'			
	Sample height, H (in)	2.770	4.443			
nfo	Sample diameter, D (in)	2.884	2.798			
ht I	Sample volume, V (ft ³)	0.0105	0.0158			
/eig	Mass rings + wet soil (g)	628.36	800.26			
Unit Weight Info.	Mass rings/tare (g)	152.04	168.60			
Un	Moist soil, Ws (g)		631.66			
	Moist unit wt., γ_m (pcf)	100.28	88.08			
er ent	Wet soil + tare (g)	296.80	754.94			
Water Content	Dry soil + tare (g)	287.40	738.11			
7 O	Tare (g)	128.47	223.39			
,	Water Content, w (%)	5.9	3.3			
	Dry Unit Wt., γ _d (pcf)	94.7	85.3			

Entered by:_	
Reviewed:	

(ASTM D4318)



Project: MWH Boring No.: WUA-TP001-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/12/2013 Description: Brown silty clay

By: BRR

Preparation method: Air Dry Liquid limit test method: Multipoint

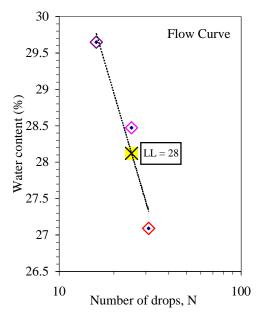
Plastic Limit

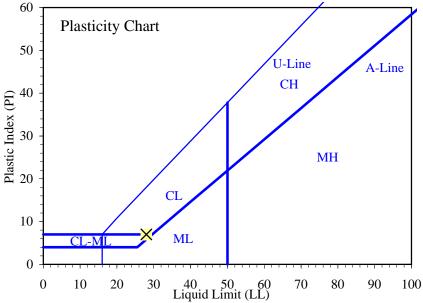
Determination No	1	2		
Wet Soil + Tare (g)	31.64	32.88		
Dry Soil + Tare (g)	30.00	31.03		
Water Loss (g)	1.64	1.85		
Tare (g)	22.14	22.07		
Dry Soil (g)	7.86	8.96		
Water Content, w (%)	20.87	20.65		

Liquid Limit

_				
Determination No	1	2	3	
Number of Drops, N	31	25	16	
Wet Soil + Tare (g)	31.38	30.95	32.16	
Dry Soil + Tare (g)	29.34	28.88	29.88	
Water Loss (g)	2.04	2.07	2.28	
Tare (g)	21.81	21.61	22.19	
Dry Soil (g)	7.53	7.27	7.69	
Water Content, w (%)	27.09	28.47	29.65	
One-Point LL (%)		28		

Liquid Limit, LL (%) 28
Plastic Limit, PL (%) 21
Plasticity Index, PI (%) 7





(ASTM D4318)



Project: MWH Boring No.: WUA-TP002-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/12/2013 Description: Brown lean clay

By: BRR

Preparation method: Air Dry Liquid limit test method: Multipoint

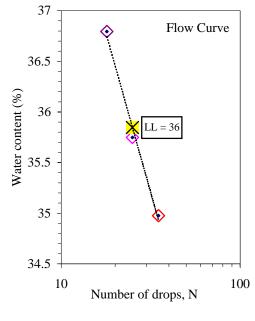
Plastic Limit

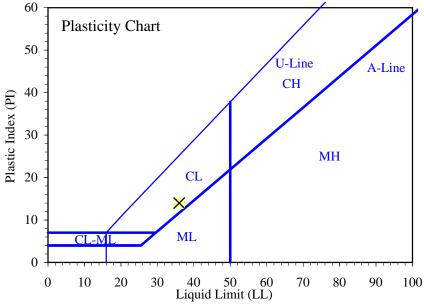
Determination No	1	2		
Wet Soil + Tare (g)	30.52	29.74		
Dry Soil + Tare (g)	29.02	28.38		
Water Loss (g)	1.50	1.36		
Tare (g)	22.04	22.12		
Dry Soil (g)	6.98	6.26		
Water Content, w (%)	21.49	21.73		

Liquid Limit

1	2	3			
35	25	18			
30.40	30.70	30.85			
28.20	28.43	28.37			
2.20	2.27	2.48			
21.91	22.08	21.63			
6.29	6.35	6.74			
34.98	35.75	36.80			
	36				·
	35 30.40 28.20 2.20 21.91 6.29	35 25 30.40 30.70 28.20 28.43 2.20 2.27 21.91 22.08 6.29 6.35 34.98 35.75	35 25 18 30.40 30.70 30.85 28.20 28.43 28.37 2.20 2.27 2.48 21.91 22.08 21.63 6.29 6.35 6.74 34.98 35.75 36.80	35 25 18 30.40 30.70 30.85 28.20 28.43 28.37 2.20 2.27 2.48 21.91 22.08 21.63 6.29 6.35 6.74 34.98 35.75 36.80	35 25 18 30.40 30.70 30.85 28.20 28.43 28.37 2.20 2.27 2.48 21.91 22.08 21.63 6.29 6.35 6.74 34.98 35.75 36.80

Liquid Limit, LL (%) 36
Plastic Limit, PL (%) 22
Plasticity Index, PI (%) 14





(ASTM D4318)



Project: MWH Boring No.: WUA-TP003-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/12/2013 Description: Brown silty clay

By: BRR

Preparation method: Air Dry Liquid limit test method: Multipoint

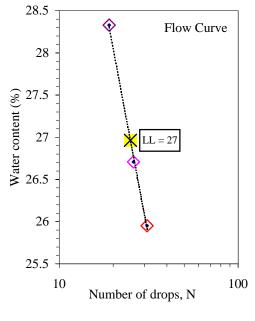
Plastic Limit

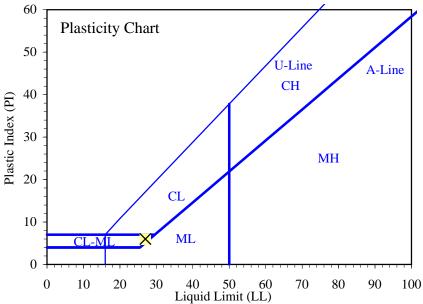
Determination No	1	2		
Wet Soil + Tare (g)	30.10	32.41		
Dry Soil + Tare (g)	28.69	30.62		
Water Loss (g)	1.41	1.79		
Tare (g)	22.05	22.08		
Dry Soil (g)	6.64	8.54		
Water Content, w (%)	21.23	20.96		

Liquid Limit

ziquia ziiiit					
Determination No	1	2	3		
Number of Drops, N	31	26	19		
Wet Soil + Tare (g)	30.69	30.15	30.75		
Dry Soil + Tare (g)	28.85	28.43	28.75		
Water Loss (g)	1.84	1.72	2.00		
Tare (g)	21.76	21.99	21.69		
Dry Soil (g)	7.09	6.44	7.06		
Water Content, w (%)	25.95	26.71	28.33		
One-Point LL (%)		27			

Liquid Limit, LL (%) 27
Plastic Limit, PL (%) 21
Plasticity Index, PI (%) 6





(ASTM D4318)



Project: MWH Boring No.: WUA-TP004-01

No: 00303-014

Location: FMC RDRA Data Gap Investigation
Date: 11/14/2013

Sample:
Depth: 1-10'
Description: Brown silt

By: BRR

Preparation method: Air Dry

Liquid Limit: Could not be determined (N.P.)

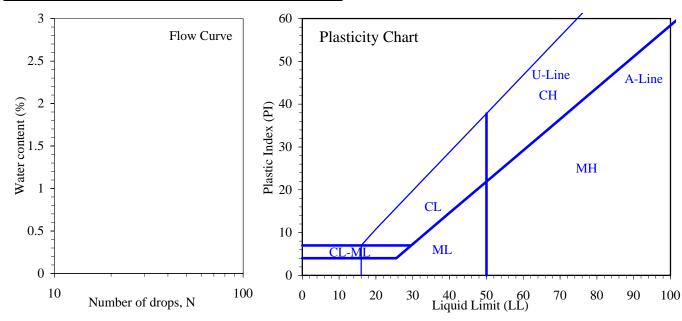
Plastic Limit

Difficult to thread.
)

Liquid Limit: Could not be determined (N.P.)

Determination No						
Number of Drops, N						
Wet Soil + Tare (g)	Unal	ole to obtai	n an adequ	ate blow c	ount.	
Dry Soil + Tare (g)						
Water Loss (g)						
Tare (g)						
Dry Soil (g)						
Water Content, w (%)						
One-Point LL (%)						

Liquid Limit, LL (%)
Plastic Limit, PL (%)
Plasticity Index, PI (%)



(ASTM D4318)



Project: MWH Boring No.: WUA-TP005-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/14/2013 Description: Brown silt

By: BRR

Preparation method: Air Dry Liquid limit test method: Multipoint

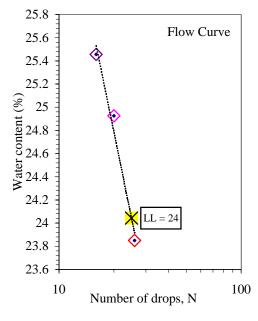
Plastic Limit

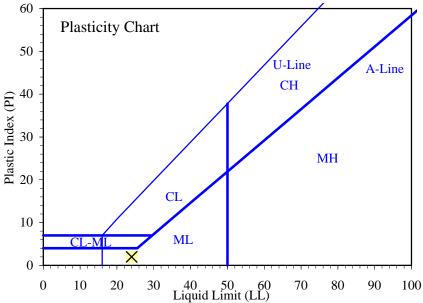
Determination No	1	2		
Wet Soil + Tare (g)	29.97	33.78		
Dry Soil + Tare (g)	28.49	31.70		
Water Loss (g)	1.48	2.08		
Tare (g)	21.64	22.04		
Dry Soil (g)	6.85	9.66		
Water Content, w (%)	21.61	21.53		

Liquid Limit

Determination No	1	2	3	
Number of Drops, N	26	20	16	
Wet Soil + Tare (g)	33.17	30.30	33.04	
Dry Soil + Tare (g)	30.89	28.62	30.81	
Water Loss (g)	2.28	1.68	2.23	
Tare (g)	21.33	21.88	22.05	
Dry Soil (g)	9.56	6.74	8.76	
Water Content, w (%)	23.85	24.93	25.46	
One-Point LL (%)	24	24		

Liquid Limit, LL (%) 24
Plastic Limit, PL (%) 22
Plasticity Index, PI (%) 2





(ASTM D4318)



Project: MWH Boring No.: WUA-TP006-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/14/2013 Description: Brown silty clay

By: BRR

Preparation method: Air Dry Liquid limit test method: Multipoint

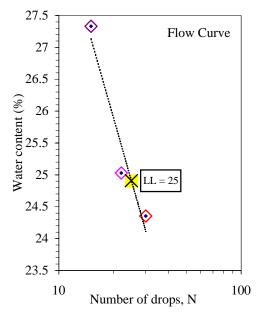
Plastic Limit

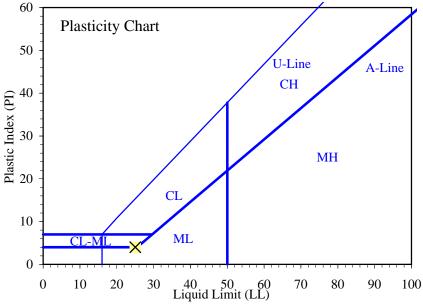
Determination No	1	2		
Wet Soil + Tare (g)	31.07	31.18		
Dry Soil + Tare (g)	29.41	29.55		
Water Loss (g)	1.66	1.63		
Tare (g)	21.70	21.80		
Dry Soil (g)	7.71	7.75		
Water Content, w (%)	21.53	21.03		

Liquid Limit

_					
Determination No	1	2	3		
Number of Drops, N	30	22	15		
Wet Soil + Tare (g)	32.11	32.92	31.87		
Dry Soil + Tare (g)	30.13	30.69	29.76		
Water Loss (g)	1.98	2.23	2.11		
Tare (g)	22.00	21.78	22.04		
Dry Soil (g)	8.13	8.91	7.72		
Water Content, w (%)	24.35	25.03	27.33		
One-Point LL (%)	25	25			·

Liquid Limit, LL (%) 25
Plastic Limit, PL (%) 21
Plasticity Index, PI (%) 4





(ASTM D4318)



Project: MWH Boring No.: WUA-TP007-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/12/2013 Description: Brown silt

By: BRR

Preparation method: Air Dry Liquid limit test method: Multipoint

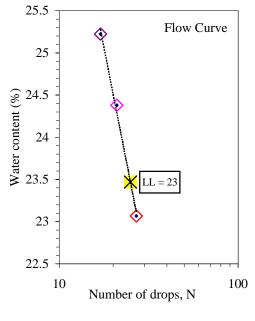
Plastic Limit

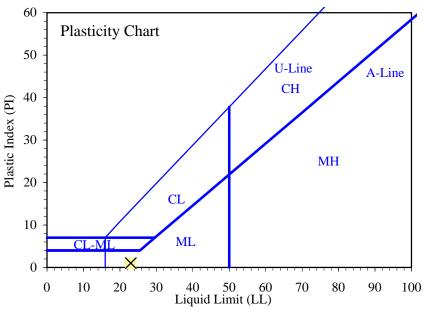
Determination No	1	2		
Wet Soil + Tare (g)	29.81	30.38		
Dry Soil + Tare (g)	28.31	28.86		
Water Loss (g)	1.50	1.52		
Tare (g)	21.57	21.95		
Dry Soil (g)	6.74	6.91		
Water Content, w (%)	22.26	22.00		

Liquid Limit

Determination No	1	2	3		
Number of Drops, N	27	21	17		
Wet Soil + Tare (g)	31.03	30.86	31.60		
Dry Soil + Tare (g)	29.30	29.09	29.62		
Water Loss (g)	1.73	1.77	1.98		
Tare (g)	21.80	21.83	21.77		
Dry Soil (g)	7.50	7.26	7.85		
Water Content, w (%)	23.07	24.38	25.22		
One-Point LL (%)	23	24			

Liquid Limit, LL (%) 23
Plastic Limit, PL (%) 22
Plasticity Index, PI (%) 1





(ASTM D4318)



Project: MWH Boring No.: WUA-TP008-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/12/2013 Description: Brown silt

By: BRR

Preparation method: Air Dry Liquid limit test method: Multipoint

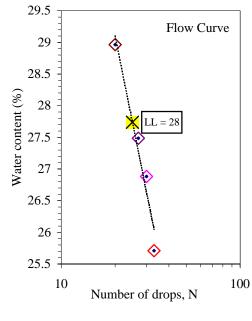
Plastic Limit

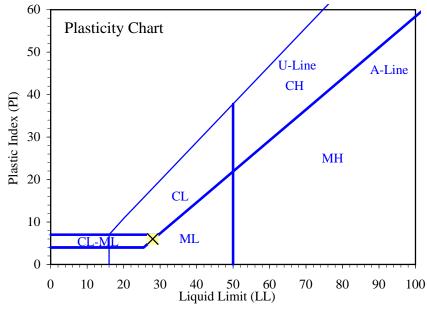
Determination No	1	2		
Wet Soil + Tare (g)	32.87	34.54		
Dry Soil + Tare (g)	30.87	32.20		
Water Loss (g)	2.00	2.34		
Tare (g)	21.88	21.71		
Dry Soil (g)	8.99	10.49		
Water Content, w (%)	22.25	22.31		

Liquid Limit

Determination No	1	2	3	4	
Number of Drops, N	33	30	27	20	
Wet Soil + Tare (g)	29.73	31.35	31.06	31.18	
Dry Soil + Tare (g)	28.10	29.35	29.07	29.08	
Water Loss (g)	1.63	2.00	1.99	2.10	
Tare (g)	21.76	21.91	21.83	21.83	
Dry Soil (g)	6.34	7.44	7.24	7.25	
Water Content, w (%)	25.71	26.88	27.49	28.97	
One-Point LL (%)	•	27	28	28	

Liquid Limit, LL (%) 28
Plastic Limit, PL (%) 22
Plasticity Index, PI (%) 6





(ASTM D4318)



Project: MWH Boring No.: WUA-TP009-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/12/2013 Description: Brown silty clay

By: BRR

Preparation method: Air Dry Liquid limit test method: Multipoint

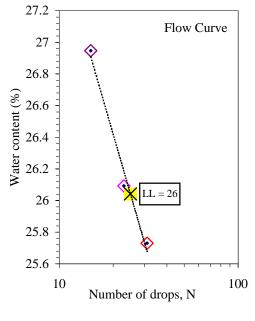
Plastic Limit

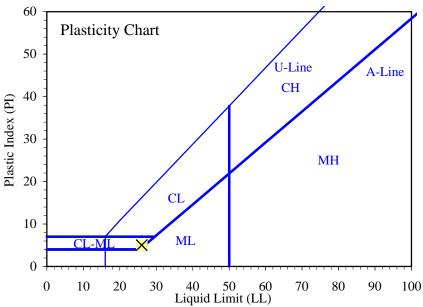
Determination No	1	2		
Wet Soil + Tare (g)	31.58	32.40		
Dry Soil + Tare (g)	29.88	30.55		
Water Loss (g)	1.70	1.85		
Tare (g)	21.85	21.71		
Dry Soil (g)	8.03	8.84		
Water Content, w (%)	21.17	20.93		

Liquid Limit

Determination No	1	2	3		
Number of Drops, N	31	23	15		
Wet Soil + Tare (g)	30.83	31.90	32.25		
Dry Soil + Tare (g)	28.98	29.81	30.07		
Water Loss (g)	1.85	2.09	2.18		
Tare (g)	21.79	21.80	21.98		
Dry Soil (g)	7.19	8.01	8.09		
Water Content, w (%)	25.73	26.09	26.95		
One-Point LL (%)		26			

Liquid Limit, LL (%) 26
Plastic Limit, PL (%) 21
Plasticity Index, PI (%) 5





(ASTM D4318)



Project: MWH Boring No.: WUA-TP010-001

No: 00303-014

Location: FMC RDRA Data Gap Investigation
Date: 11/14/2013

Sample:
Depth: 1-10'
Description: Brown silt

By: BRR

Preparation method: Air Dry

Liquid Limit: Could not be determined (N.P.)

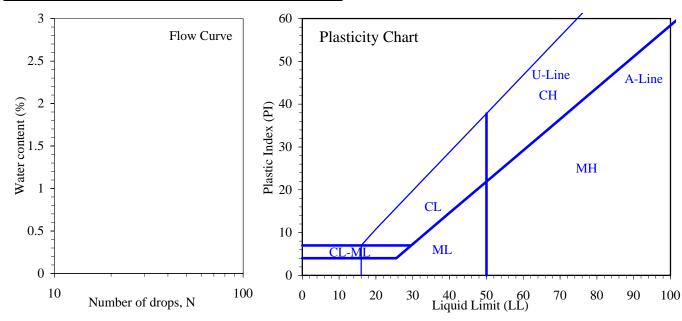
Plastic Limit

Determination No					
Wet Soil + Tare (g)					
Dry Soil + Tare (g)	Dif	Difficult to thread.			
Water Loss (g)					
Tare (g)					
Dry Soil (g)					
Water Content, w (%)					

Liquid Limit: Could not be determined (N.P.)

Determination No				
Number of Drops, N				
Wet Soil + Tare (g)	Unal			
Dry Soil + Tare (g)				
Water Loss (g)				
Tare (g)				
Dry Soil (g)				
Water Content, w (%)				
One-Point LL (%)				

Liquid Limit, LL (%)
Plastic Limit, PL (%)
Plasticity Index, PI (%)



Dispersive Characteristics of Clay Soil by Double Hydrometer



(ASTM D 4221)

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Project: MWH Boring No.: WUA-TP001-01

No: 00303-014 **Sample:**

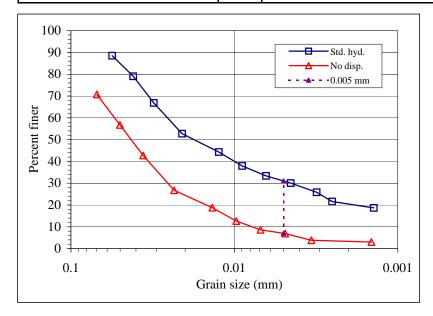
Location: FMC RDRA Data Gap Investigation **Depth:** 1-10'

Date: 11/18/2013 Description: Brown silty clay

By: BRR

Percent passing 5 um (ASTM D 4221) =	7.00
Percent passing 5 um (ASTM D 422) =	31.02
Percent Dispersion =	22.5

Standard Hyd. (AST	TM D 422)		Double Hyd. (ASTM D 4221)		
I	I J		I	J	
Particle size	Percent		Particle size	Percent	
(mm)	finer		(mm)	finer	
0.0559	88.5		0.0694	70.7	
0.0415	79.1		0.0501	56.7	
0.0311	66.9		0.0361	42.7	
0.0209	52.7		0.0234	26.7	
0.0124	44.3		0.0136	18.7	
0.0090	37.9		0.0097	12.6	
0.0064	33.4		0.0069	8.6	
0.0045	30.1		0.0049	6.9	
0.0031	25.9		0.0034	3.8	
0.0025	21.6		0.0014	3.0	
0.0014	18.7				



(ASTM D422)



Project: MWH Boring No.: WUA-TP001-01

No: 00303-014 Sample:

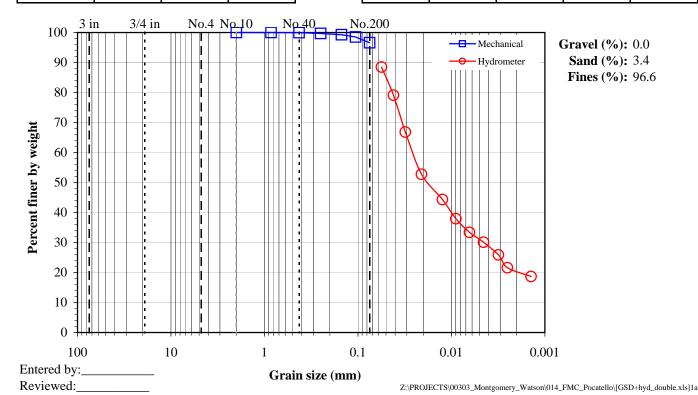
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silty clay

By: BRR

				Water content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
	Split sieve:	Yes		Moist soil + tare (g):	-	92.41	92.41	
	Split sieve:	#10		Dry soil + tare (g):	-	90.93	90.93	
		Moist	Dry	Tare (g):	-	37.69	37.69	
Total sam	ple wt. (g):	54.59	53.11	Water content (%):	0.00	2.78	2.78	
+#10 Coarse fi	raction (g):		0.00	Hydrometer data			Slope:	-0.1641
-#10 Split fi	raction (g):	54.59	53.11	Hyd. split:	No.10		Intercept:	16.3
Hydrometer f	raction (g):	54.59	53.11	Gs:	2.65	Assumed	a:	1.00
Spi	lit fraction:	1.000		Bulb No.	2	Н	yd. fraction:	100.00
				Dispersion period (min):	15	Disper	sion device:	Air-jet
	Accum.	Grain Size	Percent	Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
α. τ	17. D . ()	()	T-	(•)	(00)	D 1	()	с .

				Dispersion	criou (IIIII).	13	Disper	Sion acvice.	An-jet
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-	1	0.5	17.7	51	0.05593	88.50
6"	-	150	-		1	17.7	46	0.04154	79.09
4"	_	100	-		2	17.7	39.5	0.03112	66.85
3"	-	75	-		5	17.7	32	0.02088	52.73
1.5"	-	37.5	-		15	17.8	27.5	0.01244	44.30
3/4"	-	19	-		30	18.3	24	0.00895	37.92
3/8"	_	9.5	-		60	18.7	21.5	0.00640	33.37
No.4	_	4.75	-		120	19.8	19.5	0.00452	30.06
No.10	-	2	100.0	<=Split	250	21	17	0.00313	25.85
No.20	0.01	0.85	100.0		388	22.1	14.5	0.00252	21.60
No.40	0.03	0.425	99.9		1283	21.9	13	0.00140	18.69
No.60	0.18	0.25	99.7						
No.100	0.39	0.15	99.3						
No.140	0.78	0.106	98.5						
No.200	1.80	0.075	96.6						



(ASTM D4221)



Project: MWH Boring No.: WUA-TP001-01

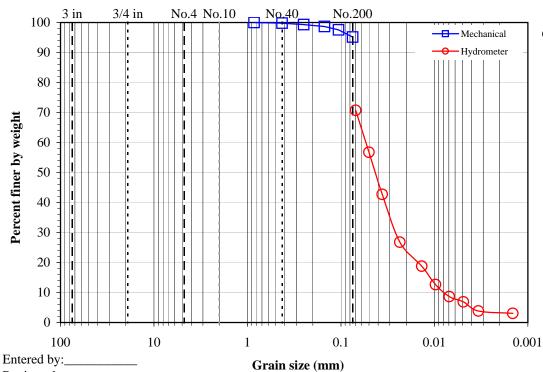
No: 00303-014 Sample:

Depth: 1-10' Location: FMC RDRA Data Gap Investigation

Date: 11/18/2013 Description: Brown silty clay

By: BRR

T T				***	1 :	O.E. (. 1110)	0.0 (110)	TT 1/37 1/	11
					content data	C.F.(+#10)		Hyd.(-No.10))
	Split sieve:				oil + tare (g):	-	92.41	92.41	
	Split sieve:			Dry so	oil + tare (g):	-	90.93	90.93	
		Moist	Dry		Tare (g):	-	37.69	37.69	
Total sar	nple wt. (g):	25.70	25.00	Water	Water content (%):		2.78	2.78	
+#10 Coarse	fraction (g):		0.00	Hyd	rometer data			Slope:	-0.1641
-#10 Split	fraction (g):	25.70	25.00		Hyd. split:	No.10		Intercept:	16.3
Hydrometer	fraction (g):	25.70	25.00		Gs:	2.65	Assumed	α:	1.00
S	plit fraction:	1.000			Bulb No.	2	Н	yd. fraction:	100.00
	_			Vacuum p	period (min):	10	Disper	rsion device:	None
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	21.8	17	0.06941	70.74
6"	-	150	-		1	21.8	13.5	0.05011	56.74
4"	-	100	-		2	21.8	10	0.03615	42.74
3"	-	75	-		5	21.8	6	0.02337	26.75
1.5"	_	37.5	-		15	21.8	4	0.01364	18.75
3/4"	_	19	-		30	21.7	2.5	0.00973	12.62
3/8"	_	9.5	-		60	21.7	1.5	0.00692	8.62
No.4	_	4.75	-		120	21.9	1	0.00489	6.89
No.10	_	2	_	<=Split	250	22.6	0	0.00338	3.82
No.20	_	0.85	100.0		1377	22	0	0.00145	3.02
No.40	0.06	0.425	99.8						
No.60	0.17	0.25	99.3						
No.100	0.34	0.15	98.6						
No.140	0.62	0.106	97.5						
No.200	1.21	0.075	95.2						



Reviewed:_

 $Z: \label{locality} Z: \label{locality} PROJECTS \label{locality} O0303_Montgomery_Watson \label{locality} O14_FMC_Pocatello \label{locality} [GSD+hyd_double.xls] 1b$

Gravel (%): 0.0 **Sand (%):** 4.8 Fines (%): 95.2

Comments:

Vacuum applied and no flocculating agent used.

Dispersive Characteristics of Clay Soil by Double Hydrometer



(ASTM D 4221)

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Boring No.: WUA-TP002-01 **Project:** MWH

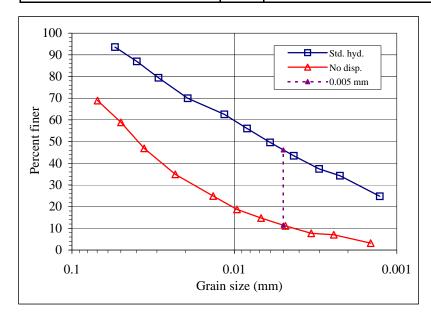
No: 00303-014 Sample:

Depth: 1-10' Location: FMC RDRA Data Gap Investigation

Description: Brown clay Date: 11/18/2013

By: BRR

Percent passing 5 um (ASTM D 4221) = 11.46									
	-	_							
	Percent pass		n (ASTM D 422) = cent Dispersion =	46.20					
	24.8								
Standard Hyd. (AST	ГМ D 422)		Double Hyd. (ASTM D 4221)						
I	J		I	J					
Particle size	Percent		Particle size	Percent					
(mm)	finer		(mm)	finer					
0.0543	93.6		0.0695	68.9					
0.0399	87.0		0.0499	58.9					
0.0293	79.4		0.0359	46.9					
0.0194	70.0		0.0231	34.9					
0.0115	62.5		0.0135	24.9					
0.0084	56.0		0.0096	18.8					
0.0060	49.6		0.0069	14.8					
0.0043	43.5		0.0049	11.2					
0.0030	37.4		0.0034	7.7					
0.0022	34.3		0.0024	7.0					
0.0013	24.8		0.0014	3.2					



Entered by:_ Reviewed:_

(ASTM D422)



Project: MWH Boring No.: WUA-TP002-01

No: 00303-014 Sample:

Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown clay

By: BRR

0.01

0.02

0.04

0.17

0.38

0.83

No.20

No.40

No.60

No.100

No.140 No.200 0.85

0.425

0.25

0.15

0.106

0.075

100.0

100.0

99.9 99.7

99.3

98.4

2).	DIXIX								
				Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
	Split sieve:	Yes		Moist so	oil + tare (g):	-	72.43	72.43	
	Split sieve:	#10		Dry so	oil + tare (g):	-	71.25	71.25	
		Moist	Dry		Tare (g):	-	37.74	37.74	
Total sar	mple wt. (g):	54.81	52.95	Water	content (%):	0.00	3.52	3.52	
+#10 Coarse	fraction (g):		0.00	Hyd	rometer data			Slope:	-0.1641
-#10 Split	fraction (g):	54.81	52.95		Hyd. split:	No.10		Intercept:	16.3
Hydrometer	fraction (g):	54.81	52.95		Gs:	2.65	Assumed	α:	1.00
S	plit fraction:	1.000			Bulb No.	2	Н	yd. fraction:	100.00
				Dispersion p	period (min):	15	Disper	sion device:	Air-jet
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	17.9	53.5	0.05434	93.59
6"	-	150	-		1	17.9	50	0.03986	86.98
4"	-	100	-		2	17.9	46	0.02931	79.42
3"	-	75	-		5	17.9	41	0.01938	69.98
1.5"	-	37.5	-		15	18.2	37	0.01153	62.55
3/4"	-	19	-		30	18.4	33.5	0.00836	56.02
3/8"	-	9.5	-		60	18.9	30	0.00603	49.62
No.4	-	4.75	-		120	20	26.5	0.00431	43.46
No.10	_	2	100.0	<=Split	250	21.3	23	0.00301	37.39

445

1469

22.9

22.8

21

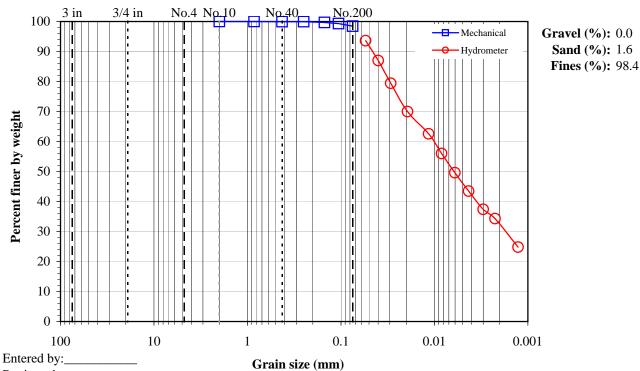
16

0.00224

0.00127

34.27

24.79



Reviewed:_____

(ASTM D4221)



Project: MWH Boring No.: WUA-TP002-01

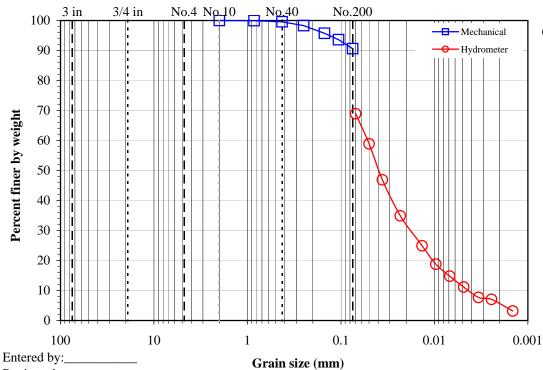
No: 00303-014 Sample:

Depth: 1-10' Location: FMC RDRA Data Gap Investigation

Description: Brown clay Date: 11/18/2013

By: BRR

	- J ·								
				Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
	Split sieve:	Yes		Moist so	oil + tare (g):	-	72.43	72.43	
	Split sieve:	#10		Dry so	oil + tare (g):	-	71.25	71.25	
		Moist	Dry		Tare (g):	-	37.74	37.74	
To	tal sample wt. (g):	25.88	25.00	Water	content (%):	0.00	3.52	3.52	
+#10 C	oarse fraction (g):		0.00	Hyd	rometer data			Slope:	-0.1641
-#10	Split fraction (g):	25.88	25.00		Hyd. split:	No.10		Intercept:	16.3
Hydro	meter fraction (g):	25.88	25.00		Gs:	2.65	Assumed	α:	1.00
	Split fraction:	1.000			Bulb No.	2	Н	lyd. fraction:	100.00
				Vacuum p	period (min):	10	Disper	rsion device:	None
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Siev	ve Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	21.9	16.5	0.06955	68.89
6"	-	150	-		1	21.9	14	0.04991	58.89
4"	-	100	-		2	21.9	11	0.03591	46.89
3"	-	75	-		5	21.9	8	0.02309	34.89
1.5	-	37.5	-		15	21.9	5.5	0.01351	24.89
3/4	-	19	-		30	21.8	4	0.00964	18.75
3/8	-	9.5	-		60	21.8	3	0.00685	14.75
No.	4 -	4.75	-		120	22.1	2	0.00485	11.15
No.1		2	100.0	<=Split	250	22.5	1	0.00336	7.69
No.2	0.01	0.85	100.0		465	23.5	0.5	0.00244	7.03
No.4	0.10	0.425	99.6		1375	22.1	0	0.00145	3.15
No.6	0.43	0.25	98.3						
No.1	00 1.06	0.15	95.8						
No.1	40 1.60	0.106	93.6						
No.2	00 2.34	0.075	90.6						



Reviewed:_

Comments: Vacuum applied and no flocculating agent used.

Gravel (%): 0.0 **Sand (%):** 9.4

Fines (%): 90.6

 $Z: \label{locality} Z: \label{locality} PROJECTS \cite{Converse} Watson \cite{Converse} All Leading \cite{Conver$

Dispersive Characteristics of Clay Soil by Double Hydrometer



(ASTM D 4221)

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Project: MWH Boring No.: WUA-TP003-01

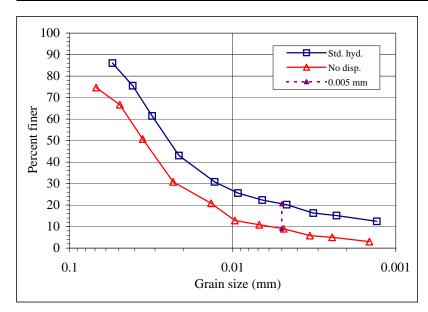
No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silty clay

By: BRR

Percent passing 5 um (ASTM D 4221) =	9.13	
Percent passing 5 um (ASTM D 422) =	20.62	
Percent Dispersion =	44.3	

Standard Hyd. (AST	M D 422)	Double Hyd. (ASTM	I D 4221)
I	J	I	J
Particle size	Percent	Particle size	Percent
(mm)	finer	(mm)	finer
0.0547	86.0	0.0689	74.7
0.0411	75.5	0.0493	66.7
0.0312	61.5	0.0357	50.7
0.0214	43.0	0.0232	30.8
0.0129	30.8	0.0136	20.8
0.0093	25.6	0.0097	12.8
0.0066	22.4	0.0069	10.9
0.0047	20.2	0.0049	9.0
0.0032	16.3	0.0034	5.8
0.0023	15.1	0.0025	5.0
0.0013	12.5	0.0015	3.0



(ASTM D422)



Gravel (%): 0.3

Sand (%): 4.1

Fines (%): 95.6

Boring No.: WUA-TP003-01 **Project: MWH**

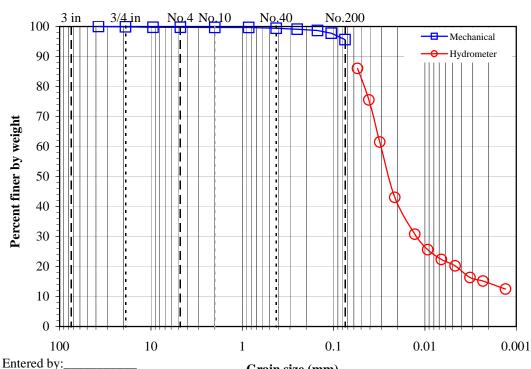
No: 00303-014 **Sample:**

Depth: 1-10' Location: FMC RDRA Data Gap Investigation

Description: Brown silty clay Date: 11/18/2013

By: BRR

				Water	content data	C.F.(+3/8")	S.F.(-3/8")	Hyd.(+No.10)	Hyd.(-No.10)
	Split sieve	: Yes		Moist so	oil + tare (g):	178.88	626.37	37.82	72.08
	Split sieve	: 3/8"		Dry so	oil + tare (g):	178.66	597.15	37.82	71.58
		Moist	Dry		Tare (g):	127.16	127.12	37.77	37.47
То	tal sample wt. (g)	: 18843.42	17743.34	Water	content (%):	0.43	6.22	0.00	1.47
+3/8" C	oarse fraction (g)	: 51.32	51.10	Hyd	rometer data			Slope:	-0.1641
-3/8"	Split fraction (g)	: 463.00	463.00		Hyd. split:	No.10		Intercept:	16.3
Hydro	meter fraction (g)	: 57.65	56.82		Gs:	2.65	Assumed	α:	1.00
	Split fraction	: 0.997			Bulb No.	2		Hyd. fraction:	99.70
				Dispersion p	eriod (min):	15		ersion device:	Air-jet
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sie		g) (mm)	Finer]	(min)	(°C)	Reading	(mm)	Suspension
8'		200	-		0.5	17.8	53	0.05471	86.04
6'		150	-		1	17.8	47	0.04111	75.51
4'		100	-		2	17.8	39	0.03122	61.47
3'		75	-		5	17.8	28.5	0.02139	43.04
1.5		37.5	100.0		15	17.9	21.5	0.01293	30.80
3/4	21.15	19	99.9		30	18.1	18.5	0.00929	25.61
3/8	51.10	9.5	99.7	<=Split	60	18.8	16.5	0.00660	22.37
No	.4 -	4.75	99.7		118	20	15	0.00467	20.20
No.	10 0.05	2	99.7	<=Split hyd.	250	21.3	12.5	0.00321	16.31
No.	20 0.02	0.85	99.7		470	22.8	11.5	0.00231	15.13
No.	40 0.15	0.425	99.4		1494	22.7	10	0.00131	12.46
No.	60 0.34	0.25	99.1						
No.1	0.60	0.15	98.6						
No.1	1.12	0.106	97.7						
No.2	200 2.32	0.075	95.6						



Grain size (mm)

Reviewed:_

(ASTM D422)



Boring No.: WUA-TP003-01 **Project: MWH**

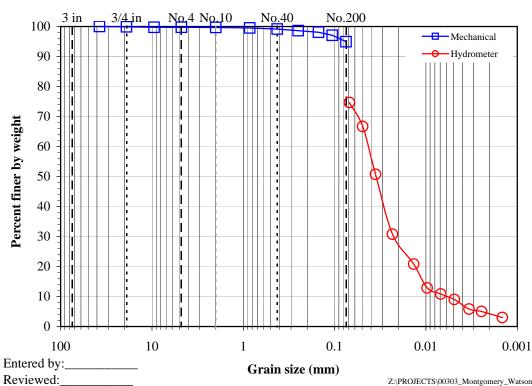
No: 00303-014 **Sample:**

Depth: 1-10' Location: FMC RDRA Data Gap Investigation

Description: Brown silty clay Date: 11/18/2013

By: BRR

				Water	content data	C.F.(+3/8")	S.F.(-3/8")	Hyd.(+No.10)	Hyd.(-No.10)
	Split sieve:	Yes		Moist so	il + tare (g):	178.88	626.37	37.82	72.08
	Split sieve:	3/8"		Dry so	il + tare (g):	178.66	597.15	37.82	71.58
	_	Moist	Dry		Tare (g):	127.16	127.12	37.77	37.47
Total san	nple wt. (g):	18843.42	17743.34	Water	Water content (%):		6.22	0.00	1.47
+3/8" Coarse	fraction (g):	51.32	51.10	Hydı	ometer data			Slope:	-0.1641
-3/8" Split	fraction (g):	463.00	463.00		Hyd. split:	No.10		Intercept:	16.3
Hydrometer	fraction (g):	25.37	25.00		Gs:	2.65	Assumed	α:	1.00
Sı	plit fraction:	0.997			Bulb No.	2		Hyd. fraction:	99.70
				Vacuum p	eriod (min):	10	Disp	ersion device:	None
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	21.9	18	0.06891	74.65
6"	-	150	-		1	21.9	16	0.04933	66.68
4"	-	100	-		2	21.9	12	0.03571	50.73
3"	-	75	-		5	21.9	7	0.02322	30.79
1.5"	-	37.5	100.0		15	21.9	4.5	0.01359	20.82
3/4"	21.15	19	99.9		30	21.9	2.5	0.00971	12.85
3/8"	51.10	9.5	99.7	<=Split	60	21.9	2	0.00688	10.85
No.4	-	4.75	99.7		120	22	1.5	0.00487	8.99
No.10	0.05	2	99.7	<=Split hyd.	250	22.6	0.5	0.00337	5.81
No.20	0.04	0.85	99.5		462	23.5	0	0.00246	5.02
No.40	0.14	0.425	99.1		1372	22	0	0.00145	3.01
No.60	0.27	0.25	98.6						
No.100	0.40	0.15	98.1						
No.140	0.66	0.106	97.1						
No.200	1.19	0.075	95.0						



Gravel (%): 0.3 **Sand (%):** 4.8 Fines (%): 95.0

Comments:

Vacuum applied and no flocculating agent used.

 $Z: \label{local_projects} Z: \label{local_projects} Watson \label{local_projects} An unique to \label{local_projects} Is a constant of \label{local_projects} An unique to \label{local_projects} Is a constant \label{local_projects} Is a constant \label{local_projects} An unique to \label{local_projects} Is a constant \label{local_projects} Is a constant \label{local_projects} Is a constant \label{local_projects} Is a constant \label{local_projects} An unique to \label{local_projects} Is a constant \label{local_projects} Is$

Dispersive Characteristics of Clay Soil by Double Hydrometer



(ASTM D 4221)

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Project: MWH Boring No.: WUA-TP004-01

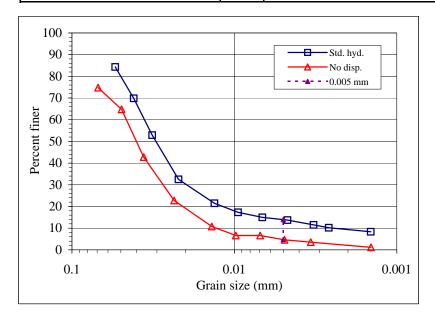
No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silt

By: BRR

Percent passing 5 um (ASTM D 4221) =	4.72
Percent passing 5 um (ASTM D 422) =	13.93
Percent Dispersion =	33.9

Standard Hyd. (AST	Standard Hyd. (ASTM D 422)			I D 4221)
I	J		I	J
Particle size	Percent	P	article size	Percent
(mm)	finer		(mm)	finer
0.0541	84.3		0.0690	74.8
0.0417	69.9		0.0495	64.8
0.0321	52.9		0.0361	42.8
0.0221	32.5		0.0235	22.8
0.0133	21.5		0.0138	10.8
0.0095	17.3		0.0098	6.6
0.0067	15.0		0.0069	6.6
0.0047	13.7		0.0049	4.6
0.0033	11.5		0.0034	3.6
0.0026	10.2		0.0014	1.1
0.0014	8.3			



(ASTM D422)



Project: MWH Boring No.: WUA-TP004-01

No: 00303-014 Sample:

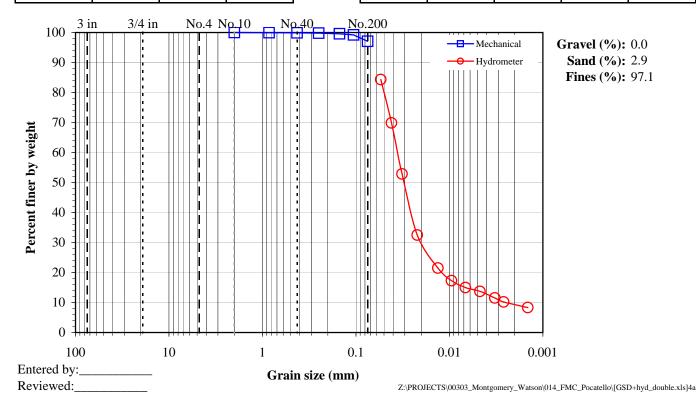
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silt

By: BRR

	21111								
	•			Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
	Split sieve:	Yes		Moist so	oil + tare (g):	-	48.39	48.39	
	Split sieve:	#10		Dry so	oil + tare (g):	-	48.28	48.28	
		Moist	Dry		Tare (g):	-	37.39	37.39	
Total san	nple wt. (g):	59.44	58.85	Water	content (%):	0.00	1.01	1.01	
+#10 Coarse	fraction (g):		0.00	Hyd	rometer data			Slope:	-0.1641
-#10 Split	fraction (g):	59.44	58.85		Hyd. split:	No.10		Intercept:	16.3
Hydrometer	fraction (g):	59.44	58.85		Gs:	2.65	Assumed	α:	1.00
Sı	plit fraction:	1.000			Bulb No.	2	Н	lyd. fraction:	100.00
				Dispersion p	period (min):	15	Disper	rsion device:	Air-jet
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	_	200	-	1	0.5	18.2	53.5	0.05413	84.32
6"	_	150	-		1	18.2	45	0.04167	69.87

	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	18.2	53.5	0.05413	84.32
6"	-	150	-		1	18.2	45	0.04167	69.87
4"	_	100	-		2	18.2	35	0.03207	52.88
3"	-	75	-		5	18.2	23	0.02209	32.49
1.5"	_	37.5	-		15	18.3	16.5	0.01327	21.48
3/4"	-	19	-		30	18.5	14	0.00950	17.30
3/8"	-	9.5	-		60	19.1	12.5	0.00673	14.98
No.4	-	4.75	-		120	20.3	11.5	0.00471	13.73
No.10	-	2	100.0	<=Split	250	21.2	10	0.00326	11.51
No.20	0.02	0.85	100.0		380	22.2	9	0.00262	10.18
No.40	0.05	0.425	99.9		1275	21.8	8	0.00145	8.34
No.60	0.13	0.25	99.8						
No.100	0.24	0.15	99.6						
No.140	0.48	0.106	99.2						
No.200	1.73	0.075	97.1						



(ASTM D4221)



Project: MWH Boring No.: WUA-TP004-01

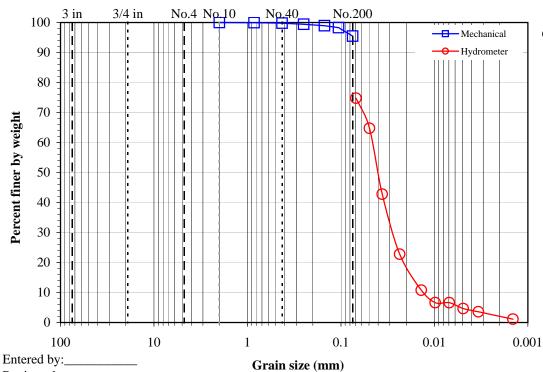
No: 00303-014 Sample:

Depth: 1-10' Location: FMC RDRA Data Gap Investigation

Description: Brown silt Date: 11/18/2013

By: BRR

				Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
	Split sieve:	Yes			oil + tare (g):	-	48.39	48.39	,
	Split sieve:				oil + tare (g):	_	48.28	48.28	
	•	Moist	Dry		Tare (g):	_	37.39	37.39	
Total sar	mple wt. (g):	25.25	25.00	Water	content (%):	0.00	1.01	1.01	
+#10 Coarse	_		0.00	Hyd	rometer data			Slope:	-0.1641
-#10 Split	fraction (g):	25.25	25.00		Hyd. split:	No.10		Intercept:	16.3
Hydrometer	fraction (g):	25.25	25.00		Gs:	2.65	Assumed	α:	1.00
S	plit fraction:	1.000			Bulb No.	2	Н	yd. fraction:	100.00
_				Vacuum p	period (min):	10	Disper	sion device:	None
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	ı		0.5	21.8	18	0.06899	74.76
6"	-	150	-		1	21.8	15.5	0.04952	64.76
4"	_	100	-		2	21.8	10	0.03615	42.76
3"	-	75	-		5	21.8	5	0.02349	22.75
1.5"	-	37.5	-		15	21.8	2	0.01378	10.75
3/4"	_	19	-		30	21.7	1	0.00981	6.62
3/8"	-	9.5	-		60	21.7	1	0.00694	6.62
No.4	_	4.75	-		120	21.7	0.5	0.00492	4.62
No.10	_	2	100.0	<=Split	250	22.4	0	0.00339	3.56
No.20	0.01	0.85	100.0		1440	20.6	0	0.00144	1.14
No.40	0.05	0.425	99.8						
No.60	0.14	0.25	99.4						
No.100	0.27	0.15	98.9						
No.140	0.43	0.106	98.3						
No.200	1.13	0.075	95.5						



Reviewed:_

Gravel (%): 0.0 **Sand (%):** 4.5

Comments:

Fines (%): 95.5

Vacuum applied and no

flocculating agent used.

 $Z: \label{local_projects} Z: \label{local_projects} Watson \label{local_projects} Id_FMC_Pocatello \cite{GSD+hyd_double.xls} \cite{Absolution} Absolute \cite{GSD+hyd_double.xls} \cite{Absolute} Absolute \cite{GSD+hyd_double.xls} \c$

Dispersive Characteristics of Clay Soil by Double Hydrometer



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(ASTM D 4221)

Project: MWH Boring No.: WUA-TP005-01

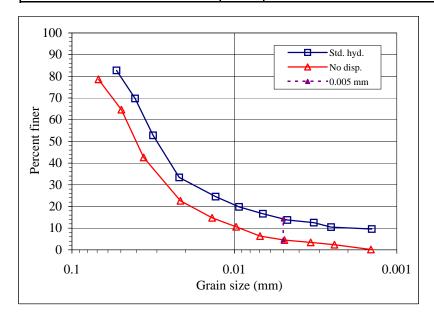
No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silt

By: BRR

Percent passing 5 um (ASTM D 4221) =	4.57
Percent passing 5 um (ASTM D 422) =	14.25
Percent Dispersion =	32.1

Standard Hyd. (AST	M D 422)	Double Hyd. (ASTM D 422	:1)
I	J	I	J
Particle size	Percent	Particle size F	Percent
(mm)	finer	(mm)	finer
0.0532	82.7	0.0687	78.6
0.0409	69.8	0.0496	64.6
0.0317	52.8	0.0362	42.6
0.0219	33.4	0.0215	22.6
0.0131	24.5	0.0137	14.8
0.0094	19.8	0.0098	10.6
0.0067	16.7	0.0069	6.4
0.0047	13.8	0.0049	4.5
0.0032	12.5	0.0034	3.4
0.0025	10.5	0.0024	2.4
0.0014	9.6	0.0014	0.1



Entered by:______
Reviewed:_____

(ASTM D422)



Project: MWH Boring No.: WUA-TP005-01

No: 00303-014 Sample:

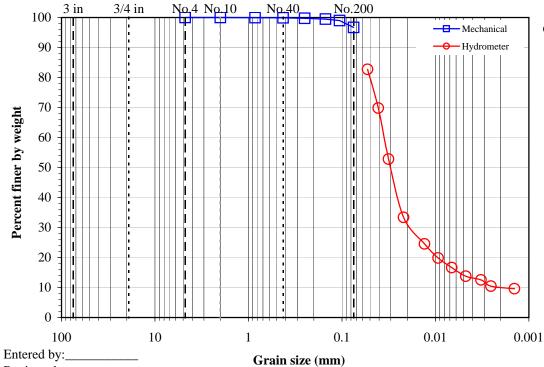
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silt

By: BRR

				Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
Split sieve: Yes			Moist so	il + tare (g):	37.86	120.67	120.67		
	Split sieve: #10			Dry so	il + tare (g):	37.86	119.56	119.56	
	Moist Dry			Tare (g):	37.84	37.75	37.75		
Total sample wt. (g):		563.63	556.09	Water	content (%):	0.00	1.36	1.36	
+#10 Coarse	fraction (g):	0.01	0.01	Hydi	Hydrometer data Slope				-0.1641
-#10 Split fraction (g):		62.65	61.81		Hyd. split: No.10 Inte		Intercept:	16.3	
Hydrometer fraction (g):		62.65	61.81	Gs: 2.65 Assu		Assumed	α:	1.00	
S	Split fraction:			Bulb No.		2	Hyd. fraction:		100.00
				Dispersion period (min): 15 Dispersion device		rsion device:	Air-jet		
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-	1	0.5	18.3	55	0.05319	82.73
6"	_	150	-		1	18.3	47	0.04086	69.79
4"	_	100	-		2	18.3	36.5	0.03166	52.80
3"	_	75	_		5	18.3	24.5	0.02185	33.39

Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-	1	0.5	18.3	55	0.05319	82.73
6"	-	150	-		1	18.3	47	0.04086	69.79
4"	-	100	-		2	18.3	36.5	0.03166	52.80
3"	-	75	-		5	18.3	24.5	0.02185	33.39
1.5"	-	37.5	-		15	18.4	19	0.01305	24.53
3/4"	-	19	-		30	18.8	16	0.00936	19.82
3/8"	-	9.5	-		60	19	14	0.00668	16.65
No.4	-	4.75	100.0		120	20	12	0.00472	13.77
No.10	0.01	2	100.0	<=Split	250	21.1	11	0.00324	12.54
No.20	0.03	0.85	99.9		404	22.1	9.5	0.00254	10.47
No.40	0.08	0.425	99.9		1297	21.9	9	0.00143	9.59
No.60	0.17	0.25	99.7						
No.100	0.32	0.15	99.5						
No.140	0.61	0.106	99.0						
No.200	2.03	0.075	96.7]					



Reviewed:_____

Gravel (%): 0.0 Sand (%): 3.3

Fines (%): 96.7

(ASTM D4221)



Project: MWH Boring No.: WUA-TP005-01

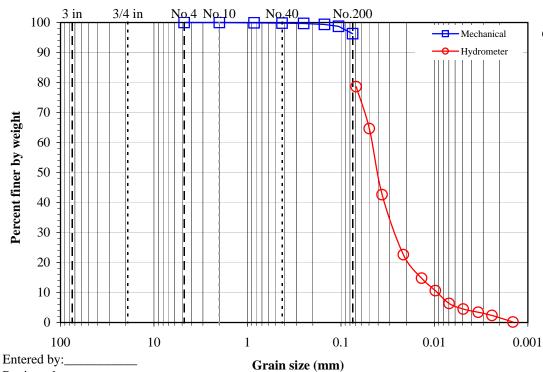
No: 00303-014 Sample:

Depth: 1-10' Location: FMC RDRA Data Gap Investigation

Description: Brown silt Date: 11/18/2013

By: BRR

					Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
		Split sieve:	Yes		Moist so	oil + tare (g):	37.86	120.67	120.67	
		Split sieve:	#10		Dry so	oil + tare (g):	37.86	119.56	119.56	
			Moist	Dry		Tare (g):	37.84	37.75	37.75	
	Total sar	nple wt. (g):	563.63	556.09	Water	content (%):	0.00	1.36	1.36	
-	#10 Coarse	fraction (g):	0.01	0.01	Hyd	rometer data			Slope:	-0.1641
	-#10 Split	fraction (g):	25.34	25.00		Hyd. split:	No.10		Intercept:	16.3
	Hydrometer	fraction (g):	25.34	25.00		Gs:	2.65	Assumed	α:	1.00
	S	plit fraction:	1.000			Bulb No.	2	Н	yd. fraction:	100.00
					Vacuum p	period (min):	10		rsion device:	None
		Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
	Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
	8"	-	200	=		0.5	21.7	19	0.06867	78.61
	6"	-	150	-		1	21.7	15.5	0.04960	64.62
	4"	-	100	-		2	21.7	10	0.03621	42.62
	3"	-	75	-		6	21.7	5	0.02148	22.62
	1.5"	-	37.5	-		15	21.8	3	0.01371	14.75
	3/4"	_	19	=		30	21.7	2	0.00976	10.62
	3/8"	-	9.5	-		60	21.5	1	0.00695	6.35
	No.4	_	4.75	100.0		120	21.6	0.5	0.00492	4.48
	No.10	0.01	2	100.0	<=Split	250	22.3	0	0.00339	3.42
	No.20	0.02	0.85	99.9		484	23	-0.5	0.00242	2.36
	No.40	0.05	0.425	99.8		1440	20.6	-0.25	0.00144	0.14
	No.60	0.08	0.25	99.7						
	No.100	0.16	0.15	99.4						
	No.140	0.32	0.106	98.7						
I	No.200	0.93	0.075	96.3						



Reviewed:_

 $Z: \label{locality} Z: \label{locality} PROJECTS \cite{Converse} Watson \cite{Converse} All Leading \cite{Conver$

Gravel (%): 0.0 **Sand (%):** 3.7 Fines (%): 96.3

Comments:

Vacuum applied and no flocculating agent used.

Dispersive Characteristics of Clay Soil by Double Hydrometer



(ASTM D 4221)

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Project: MWH Boring No.: WUA-TP006-01

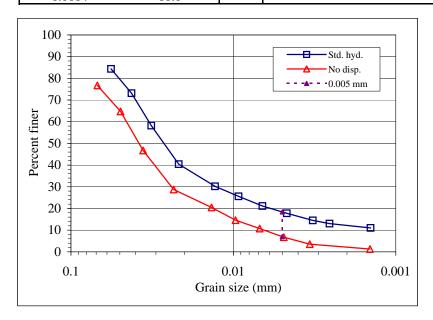
No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silty clay

By: BRR

Percent passing 5 um (ASTM D 4221) =	7.00
Percent passing 5 um (ASTM D 422) =	18.40
Percent Dispersion =	38.0

Standard Hyd. (AST	M D 422)	D	Double Hyd. (ASTM D 4221)			
I	I J		I	J		
Particle size	Percent		Particle size	Percent		
(mm)	finer		(mm)	finer		
0.0567	84.4		0.0688	76.7		
0.0424	73.2		0.0495	64.7		
0.0320	58.2		0.0359	46.7		
0.0217	40.4		0.0233	28.7		
0.0130	30.2		0.0136	20.5		
0.0093	25.6		0.0097	14.6		
0.0066	21.1		0.0069	10.8		
0.0047	17.8		0.0049	6.8		
0.0032	14.5		0.0034	3.6		
0.0026	13.0		0.0014	1.3		
0.0014	11.0					



(ASTM D422)



Project: MWH Boring No.: WUA-TP006-01

No: 00303-014 Sample:

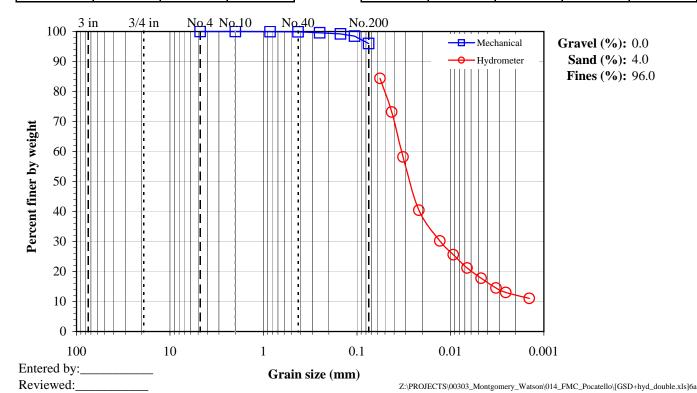
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silty clay

By: BRR

				Water content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
	Split sieve:	Yes		Moist soil + tare (g):	37.60	102.43	102.43	
	Split sieve: #10		Dry soil + tare (g):	37.60	99.79	99.79		
		Moist	Dry	Tare (g):	37.57	37.31	37.31	
Total sar	otal sample wt. (g): 575.27 551.95		Water content (%):	0.00	4.23	4.23		
+#10 Coarse	fraction (g):	0.01	0.01	Hydrometer data			Slope:	-0.1641
-#10 Split	-#10 Split fraction (g): 55.76 53.50		Hyd. split:	No.10		Intercept:	16.3	
Hydrometer fraction (g):		55.76	53.50	Gs:	2.65	Assumed	α:	1.00
Split fraction:		1.000		Bulb No.	2	Н	yd. fraction:	100.00
			Dispersion period (min):	15	Dispersion device:		Air-jet	
	Accum.	Grain Size	Percent	Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Ciarra	W/t Dat (a)	(******)	Einan	(min)	(°C)	Danding	(2222)	Cuananaian

				Dispersion p	berioa (min):	15	Disper	sion device:	Air-jet
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	_	200	-		0.5	18.3	49	0.05667	84.37
6"	_	150	-		1	18.3	43	0.04239	73.16
4"	-	100	-		2	18.3	35	0.03204	58.20
3"	_	75	-		5	18.3	25.5	0.02171	40.45
1.5"	_	37.5	-		15	18.4	20	0.01297	30.21
3/4"	_	19	-		30	18.6	17.5	0.00929	25.62
3/8"	_	9.5	-		60	19.1	15	0.00663	21.15
No.4	_	4.75	100.0		120	20	13	0.00469	17.78
No.10	0.01	2	100.0	<=Split	250	21.1	11	0.00324	14.49
No.20	0.02	0.85	100.0		396	22.1	10	0.00256	13.03
No.40	0.06	0.425	99.9		1290	21.8	9	0.00143	11.04
No.60	0.22	0.25	99.6						
No.100	0.44	0.15	99.2						
No.140	0.82	0.106	98.5						
No.200	2.13	0.075	96.0						



(ASTM D4221)



Project: MWH Boring No.: WUA-TP006-01

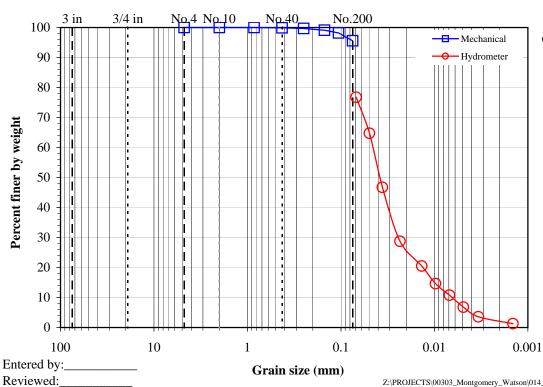
No: 00303-014 Sample:

Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silty clay

By: BRR

						~ - /	~ =		
					content data			Hyd.(-No.10))
	Split sieve:			Moist so	oil + tare (g):	37.60	102.43	102.43	
	Split sieve:	#10		Dry so	oil + tare (g):	37.60	99.79	99.79	
		Moist	Dry		Tare (g):	37.57	37.31	37.31	
Total sar	nple wt. (g):	575.27	551.95	Water	content (%):	0.00	4.23	4.23	
+#10 Coarse	fraction (g):	0.01	0.01	Hyd	rometer data			Slope:	-0.1641
-#10 Split	fraction (g):	26.06	25.00		Hyd. split:	No.10		Intercept:	16.3
Hydrometer	fraction (g):	26.06	25.00		Gs:	2.65	Assumed	α:	1.00
S	plit fraction:	1.000			Bulb No.	2	Н	yd. fraction:	100.00
_				Vacuum p	period (min):	10	Disper	sion device:	None
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-]	0.5	21.8	18.5	0.06877	76.74
6"	_	150	-		1	21.8	15.5	0.04952	64.74
4"	_	100	-		2	21.8	11	0.03595	46.75
3"	_	75	-		5	21.8	6.5	0.02331	28.75
1.5"	_	37.5	-		15	21.6	4.5	0.01364	20.48
3/4"	_	19	-		30	21.7	3	0.00971	14.62
3/8"	_	9.5	-		60	21.8	2	0.00689	10.75
No.4	_	4.75	100.0		120	21.8	1	0.00490	6.75
No.10	0.01	2	100.0	<=Split	250	22.4	0	0.00339	3.56
No.20	_	0.85	100.0		1436	20.7	0	0.00144	1.28
No.40	0.02	0.425	99.9						
No.60	0.08	0.25	99.7						
No.100	0.22	0.15	99.1						
No.140	0.45	0.106	98.2						
No.200	1.10	0.075	95.6						



flocculating agent used.

Vacuum applied and no

Gravel (%): 0.0 **Sand (%):** 4.4

Comments:

Fines (%): 95.6

Dispersive Characteristics of Clay Soil by Double Hydrometer



(ASTM D 4221)

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Project: MWH Boring No.: WUA-TP007-01

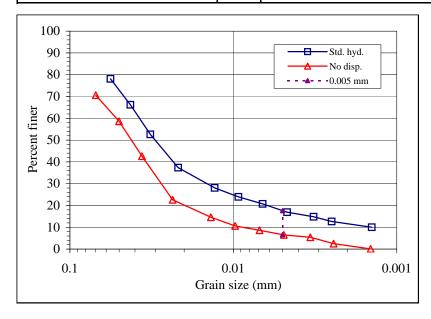
No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silt

By: BRR

Percent passing 5 um (ASTM D 4221) =	6.60
Percent passing 5 um (ASTM D 422) =	17.63
Percent Dispersion =	37.4

Standard Hyd. (AST	M D 422)	Double Hyd. (ASTM	I D 4221)
I	J	I	J
Particle size	Percent	Particle size	Percent
(mm)	finer	(mm)	finer
0.0565	78.1	0.0695	70.6
0.0427	66.2	0.0500	58.6
0.0322	52.7	0.0362	42.6
0.0218	37.4	0.0235	22.6
0.0130	28.1	0.0137	14.6
0.0093	24.0	0.0098	10.6
0.0066	20.7	0.0069	8.6
0.0047	16.9	0.0049	6.5
0.0032	14.8	0.0034	5.4
0.0025	12.7	0.0024	2.5
0.0014	10.0	0.0014	0.1



Entered by:______
Reviewed:_____

(ASTM D422)

No.4

No.10

No.20

No.40

No.60

No.100

No.140

0.25

1.38

0.23

0.73

1.81

3.65

4.97

4.75

2

0.85

0.425

0.25

0.15

0.106

99.9

99.7

99.3

98.5

96.6

93.5

91.3

<=Split



Project: MWH Boring No.: WUA-TP007-01

No: 00303-014 Sample:

Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silt

By: BRR

				Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10	0)
	Split sieve:	Yes		Moist so	oil + tare (g):	41.56	96.71	96.71	
	Split sieve:	#10		Dry so	oil + tare (g):	41.53	95.71	95.71	
		Moist	Dry		Tare (g):	38.15	37.76	37.76	
Total sa	mple wt. (g):	471.57	463.58	Water	content (%):	0.89	1.73	1.73	
+#10 Coarse	fraction (g):	1.38	1.37	Hyd	rometer data			Slope:	-0.1641
-#10 Split	fraction (g):	59.77	58.76		Hyd. split:	No.10		Intercept:	16.3
Hydrometer fraction (g): 59.77 58.76		58.76		Gs:	2.65	Assumed	α:	1.00	
Split fraction:		0.997			Bulb No.	2	Н	yd. fraction:	99.70
•			Dispersion p	period (min):	15	Disper	sion device:	Air-jet	
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-]	0.5	17.8	50	0.05645	78.11
6"	-	150	-		1	17.8	43	0.04266	66.23
4"	-	100	-		2	17.8	35	0.03223	52.65
3"	-	75	-		5	17.8	26	0.02177	37.38
1.5"	-	37.5	-		15	17.9	20.5	0.01301	28.09
3/4"	-	19	-		30	18.2	18	0.00931	23.95
3/8"	-	9.5	100.0		60	18.7	16	0.00662	20.75
1	I			I	I		I	0 00 4 40	

120

250

412

1305

19.8

21

22.1

21.8

13.5

12

10.5

9

0.00469

0.00323

0.00250

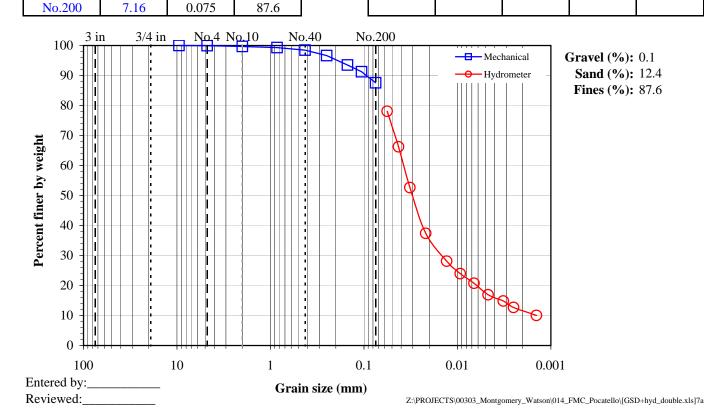
0.00142

16.91

14.81

12.68

10.02



(ASTM D4221)



Project: MWH Boring No.: WUA-TP007-01

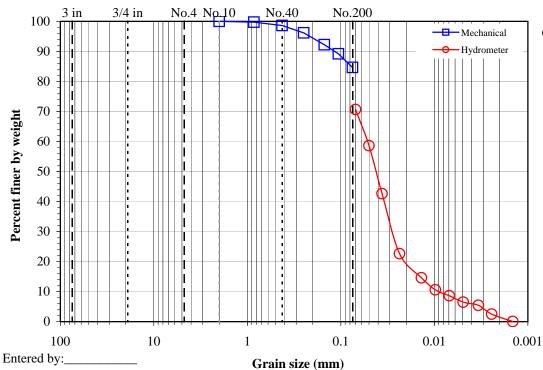
No: 00303-014 Sample:

Depth: 1-10' Location: FMC RDRA Data Gap Investigation

Description: Brown silt Date: 11/18/2013

By: BRR

<i>J</i> .									
				Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
	Split sieve:	Yes		Moist so	oil + tare (g):	-	96.71	96.71	
	Split sieve:	#10		Dry so	oil + tare (g):	-	95.71	95.71	
		Moist	Dry		Tare (g):		37.76	37.76	
Total sa	mple wt. (g):	25.43	25.00	Water	content (%):	0.00	1.73	1.73	
+#10 Coarse	fraction (g):		0.00	Hyd	rometer data			Slope:	-0.1641
-#10 Split	fraction (g):	25.43	25.00	Hyd. split:		No.10		Intercept:	16.3
Hydrometer	fraction (g):	25.43	25.00	Gs:		2.65	Assumed	α:	1.00
S	plit fraction:	1.000			Bulb No.	2	Н	yd. fraction:	100.00
				Vacuum p	period (min):	10	Disper	rsion device:	None
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-]	0.5	21.7	17	0.06952	70.62
6"	-	150	-		1	21.7	14	0.05004	58.62
4"	-	100	-		2	21.7	10	0.03621	42.62
3"	-	75	-		5	21.7	5	0.02353	22.62
1.5"	-	37.5	-		15	21.7	3	0.01373	14.62
3/4"	-	19	-		30	21.7	2	0.00976	10.62
3/8"	-	9.5	-		60	21.7	1.5	0.00692	8.62
No.4	-	4.75	-		120	21.6	1	0.00491	6.49
No.10	-	2	100.0	<=Split	250	22.3	0.5	0.00338	5.42
No.20	0.07	0.85	99.7		477	23.1	-0.5	0.00244	2.50
No.40	0.35	0.425	98.6		1432	20.7	-0.3	0.00145	0.08
No.60	0.96	0.25	96.2						
No.100	1.94	0.15	92.2						
No.140	2.70	0.106	89.2						
No.200	3.84	0.075	84.6						



Gravel (%): 0.0 Sand (%): 15.4 Fines (%): 84.6

Comments:

Vacuum applied and no flocculating agent used.

Reviewed:_

 $Z: \label{local_projects} Z: \label{local_projects} Watson \label{local_projects} Id_FMC_Pocatello \cite{GSD+hyd_double.xls} \cite{GSD+hyd_double.$

Dispersive Characteristics of Clay Soil by Double Hydrometer



(ASTM D 4221)

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Project: MWH Boring No.: WUA-TP008-01

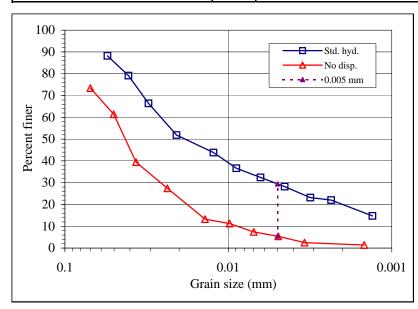
No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silt

By: BRR

Percent passing 5 um (ASTM D 4221) =	5.46
Percent passing 5 um (ASTM D 422) =	29.43
Percent Dispersion =	18.6

Standard Hyd. (AST	TM D 422)	Double Hyd. (ASTM	I D 4221)
I	J	I	J
Particle size	Percent	Particle size	Percent
(mm)	finer	(mm)	finer
0.0549	88.2	0.0698	73.4
0.0409	79.1	0.0503	61.4
0.0308	66.4	0.0367	39.4
0.0207	51.9	0.0236	27.4
0.0123	43.8	0.0139	13.3
0.0089	36.6	0.0098	11.3
0.0064	32.4	0.0070	7.4
0.0045	28.2	0.0050	5.4
0.0032	23.2	0.0034	2.5
0.0024	22.0	0.0015	1.4
0.0013	14.8		



Entered by:______
Reviewed:_____

(ASTM D422)



Project: MWH Boring No.: WUA-TP008-01

No: 00303-014 Sample:

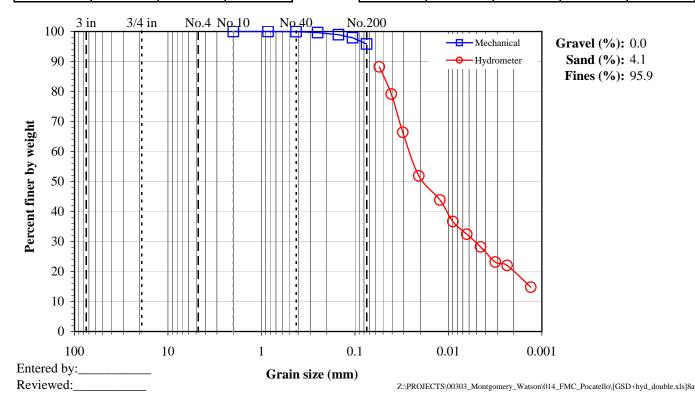
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silt

By: BRR

_										
Γ		•		•	Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10)
		Split sieve:	Yes		Moist so	oil + tare (g):	-	111.09	111.09	
		Split sieve:	#10		Dry so	oil + tare (g):	_	109.59	109.59	
			Moist	Dry		Tare (g):	-	37.30	37.30	
	Total san	nple wt. (g):	56.17	55.03	Water	content (%):	0.00	2.07	2.07	
	+#10 Coarse	fraction (g):		0.00	Hyd	rometer data			Slope:	-0.1641
	-#10 Split fraction (g):		56.17	55.03		Hyd. split:	No.10		Intercept:	16.3
	Hydrometer	fraction (g):	56.17	55.03		Gs:	2.65	Assumed	a:	1.00
	S_1	plit fraction:	1.000			Bulb No.	2	Н	yd. fraction:	100.00
					Dispersion period (min):		15	Dispersion device:		Air-jet
ſ		Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
	Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
ſ	8"	_	200	-]	0.5	17.9	52.5	0.05493	88.23
	6"	_	150	-		1	17.9	47.5	0.04086	79.14
1	4.11		100			2	17.0	40.5	0.02070	((10

	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	17.9	52.5	0.05493	88.23
6"	-	150	-		1	17.9	47.5	0.04086	79.14
4"	-	100	-		2	17.9	40.5	0.03078	66.42
3"	_	75	-		5	17.9	32.5	0.02075	51.88
1.5"	_	37.5	-		15	18.2	28	0.01233	43.83
3/4"	-	19	-		30	18.4	24	0.00894	36.64
3/8"	_	9.5	-		60	19.2	21.5	0.00636	32.41
No.4	-	4.75	-		120	20	19	0.00452	28.19
No.10	-	2	100.0	<=Split	250	21.1	16	0.00315	23.17
No.20	0.01	0.85	100.0		436	22.8	15	0.00235	22.03
No.40	0.02	0.425	100.0		1461	22.8	11	0.00131	14.76
No.60	0.22	0.25	99.6						
No.100	0.60	0.15	98.9						
No.140	1.14	0.106	97.9						
No.200	2.28	0.075	95.9						



(ASTM D4221)



Project: MWH Boring No.: WUA-TP008-01

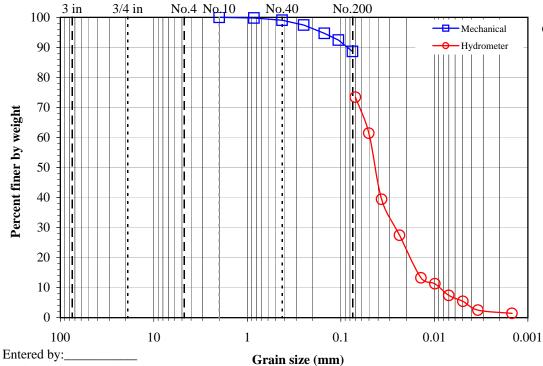
No: 00303-014 Sample:

Depth: 1-10' Location: FMC RDRA Data Gap Investigation

Description: Brown silt Date: 11/18/2013

By: BRR

				Water	content data	C.F.(+#10)	S.F.(-#10)	Hyd.(-No.10))
	Split sieve:	Yes		Moist so	oil + tare (g):	-	111.09	111.09	
	Split sieve:	#10		Dry so	oil + tare (g):	-	109.59	109.59	
		Moist	Dry		Tare (g):	-	37.30	37.30	
Total sa	imple wt. (g):	25.52	25.00	Water	Water content (%):		2.07	2.07	
+#10 Coarse	e fraction (g):		0.00	Hydrometer data				Slope:	-0.1641
-#10 Split fraction (g):		25.52	25.00	Hyd. split:		No.10		Intercept:	16.3
Hydromete	Hydrometer fraction (g):		25.00		Gs:	2.65	Assumed	α:	1.00
	Split fraction:	1.000			Bulb No.	2	Н	yd. fraction:	100.00
				Vacuum p	period (min):	10	Disper	rsion device:	None
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	20.8	18	0.06984	73.41
6"	-	150	-		1	20.8	15	0.05029	61.41
4"	-	100	-		2	20.8	9.5	0.03670	39.41
3"	-	75	-		5	20.8	6.5	0.02360	27.41
1.5"	-	37.5	-		15	20.7	3	0.01389	13.28
3/4"	-	19	-		30	20.7	2.5	0.00985	11.28
3/8"	-	9.5	-		60	20.8	1.5	0.00699	7.41
No.4	_	4.75	-		120	20.8	1	0.00496	5.41
No.10	-	2	100.0	<=Split	250	21.6	0	0.00342	2.48
No.20	0.05	0.85	99.8		1370	20.8	0	0.00147	1.41
No.40	0.24	0.425	99.0						
No.60	0.64	0.25	97.4						
No.100	1.33	0.15	94.7						
No.140	1.89	0.106	92.4						
No.200	2.84	0.075	88.6						



Gravel (%): 0.0 Sand (%): 11.4 Fines (%): 88.6

Comments:

Vacuum applied and no flocculating agent used.

Reviewed:_

 $Z: \label{local_projects} Z: \label{local_projects} A convers_Watson \label{local_projects} A conversion \label{local_projects} A conven$

Dispersive Characteristics of Clay Soil by Double Hydrometer



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(ASTM D 4221)

Boring No.: WUA-TP009-01

No: 00303-014 **Sample:**

Location: FMC RDRA Data Gap Investigation **Depth:** 1-10'

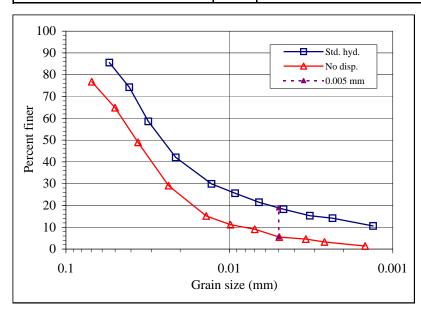
Date: 11/18/2013 Description: Brown silty clay

By: BRR

Project: MWH

Percent passing 5 um (ASTM D 4221) =	5.62
Percent passing 5 um (ASTM D 422) =	18.93
Percent Dispersion =	29.7

Standard Hyd. (AST	M D 422)	Double Hyd. (ASTM	I D 4221)
I	J	I	J
Particle size	Percent	Particle size	Percent
(mm)	finer	(mm)	finer
0.0542	85.6	0.0695	76.8
0.0409	74.3	0.0500	64.9
0.0313	58.6	0.0362	49.0
0.0213	42.1	0.0236	29.1
0.0129	29.9	0.0139	15.2
0.0092	25.6	0.0098	11.2
0.0066	21.5	0.0070	9.1
0.0047	18.3	0.0049	5.5
0.0032	15.3	0.0034	4.6
0.0023	14.2	0.0026	3.3
0.0013	10.6	0.0015	1.4



Entered by:______
Reviewed:_____

(ASTM D422)



Project: MWH Boring No.: WUA-TP009-01

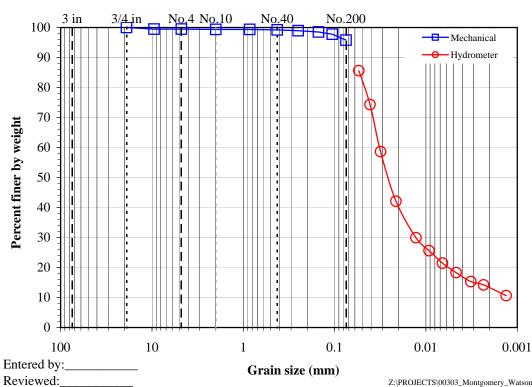
No: 00303-014 Sample:

Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silty clay

By: BRR

Ĭ				Water	content data	C.F.(+3/8")	S.F.(-3/8")	Hyd.(+No.10)	Hyd.(-No.10)
	Split sieve:	Yes		Moist so	il + tare (g):	241.03	660.11	38.52	55.26
	Split sieve:	3/8"		Dry so	il + tare (g):	240.59	619.64	38.51	54.97
		Moist	Dry		Tare (g):	126.36	123.24	37.81	37.72
Total san	nple wt. (g):	22005.77	20355.03	Water	content (%):	0.39	8.15	1.43	1.68
+3/8" Coarse	fraction (g):	112.96	112.53	Hydrometer data				Slope:	-0.1641
-3/8" Split	fraction (g):	518.78	511.47		Hyd. split:	No.10		Intercept:	16.3
Hydrometer	fraction (g):	58.07	57.11		Gs:	2.65	Assumed	α:	1.00
S_1	plit fraction:	0.994		Bulb No.		2	-	Hyd. fraction:	99.37
				Dispersion period (min):		15	Disp	ersion device:	Air-jet
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer]	(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	18.5	53	0.05422	85.58
6"	-	150	-		1	18.5	46.5	0.04094	74.27
4"	-	100	-		2	18.5	37.5	0.03132	58.61
3"	-	75	-		5	18.5	28	0.02127	42.08
1.5"	-	37.5	-		15	18.6	21	0.01286	29.94
3/4"	-	19	100.0		30	18.7	18.5	0.00922	25.62
3/8"	112.53	9.5	99.4	<=Split	60	19.2	16	0.00658	21.46
No.4	-	4.75	99.4		120	20	14	0.00466	18.29
No.10	0.39	2	99.4	<=Split hyd.	250	21.3	12	0.00322	15.30
No.20	0.01	0.85	99.4		461	22.9	11	0.00234	14.17
No.40	0.11	0.425	99.2		1486	22.7	9	0.00132	10.62
No.60	0.25	0.25	98.9						
No.100	0.50	0.15	98.5						
No.140	0.92	0.106	97.8						
No.200	2.07	0.075	95.8						



Gravel (%): 0.6

Sand (%): 3.7

Fines (%): 95.8

(ASTM D422)



Project: MWH Boring No.: WUA-TP009-01

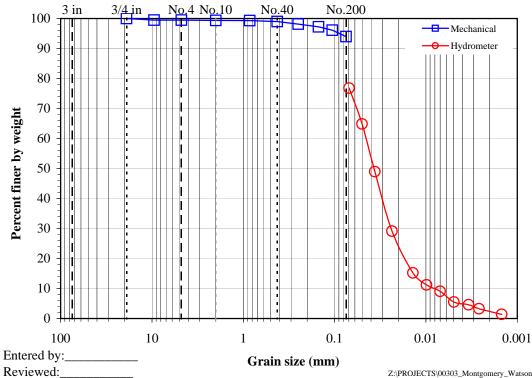
No: 00303-014 Sample:

Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silty clay

By: BRR

				Water	content data	C.F.(+3/8")	S.F.(-3/8")	Hyd.(+No.10)	Hyd.(-No.10)
	Split sieve:	Yes		Moist so	il + tare (g):	241.03	660.11	38.52	55.26
	Split sieve:	3/8"		Dry so	il + tare (g):	240.59	619.64	38.51	54.97
		Moist	Dry		Tare (g):	126.36	123.24	37.81	37.72
Total s	sample wt. (g):	22005.77	20355.03	Water	content (%):	0.39	8.15	1.43	1.68
+3/8" Coar	se fraction (g):	112.96	112.53	Hydi	rometer data			Slope:	-0.1641
-3/8" Sp	lit fraction (g):	518.78	511.47		Hyd. split:	No.10		Intercept:	16.3
Hydromet	er fraction (g):	25.42	25.00	Gs:		2.65	Assumed	α:	1.00
	Split fraction:	0.994		Bulb No.		2]	Hyd. fraction:	99.37
	_			Vacuum period (min):		10	Dispe	ersion device:	None
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	20.7	19	0.06948	76.79
6"	-	150	-		1	20.7	16	0.05004	64.87
4"	-	100	-		2	20.7	12	0.03622	48.97
3"	-	75	-		5	20.7	7	0.02356	29.09
1.5"	-	37.5	-		15	20.7	3.5	0.01386	15.18
3/4"	-	19	100.0		30	20.7	2.5	0.00985	11.21
3/8"	112.53	9.5	99.4	<=Split	60	20.6	2	0.00699	9.09
No.4	-	4.75	99.4		120	20.9	1	0.00495	5.51
No.10	0.39	2	99.4	<=Split hyd.	250	21.7	0.5	0.00341	4.59
No.20	0.02	0.85	99.3		420	22.2	0	0.00262	3.27
No.40	0.10	0.425	99.0		1367	20.8	0	0.00148	1.40
No.60	0.31	0.25	98.1						
No.100	0.54	0.15	97.2						
No.140	0.82	0.106	96.1						
No.200	1.36	0.075	94.0						



Gravel (%): 0.6 Sand (%): 5.5 Fines (%): 94.0

Comments:

Vacuum applied and no flocculating agent used.

 $Z: \label{lem:converse} Z: \label{lem:converse} PROJECTS \label{lem:converse} O303_Montgomery_Watson \label{lem:converse} O14_FMC_Pocatello \label{lem:converse} IGSD+hyd_double.xls \label{lem:converse} O30303_Montgomery_Watson \label{lem:converse} O14_FMC_Pocatello \label{lem:converse} O1$

Dispersive Characteristics of Clay Soil by Double Hydrometer



(ASTM D 4221)

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Project: MWH Boring No.: WUA-TP010-01

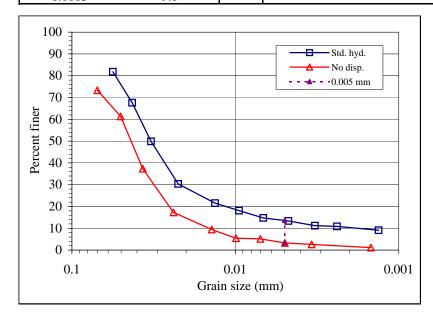
No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/18/2013 Description: Brown silt

By: BRR

Percent passing 5 um (ASTM D 4221) =	3.31
Percent passing 5 um (ASTM D 422) =	13.58
Percent Dispersion =	24.4

Standard Hyd. (AST	M D 422)	Double Hyd. (ASTM D 4221)
I	J	I J
Particle size	Percent	Particle size Percent
(mm)	finer	(mm) finer
0.0562	81.8	0.0699 73.4
0.0428	67.6	0.0503 61.3
0.0328	49.9	0.0368 37.3
0.0224	30.4	0.0239 17.3
0.0133	21.5	0.0139 9.4
0.0095	18.1	0.0099 5.4
0.0067	14.8	0.0070 5.2
0.0047	13.4	0.0050 3.3
0.0033	11.2	0.0034 2.6
0.0024	10.9	0.0015 1.1
0.0013	9.1	



Entered by:______
Reviewed:_____

(ASTM D422)



Boring No.: WUA-TP010-01 **Project: MWH**

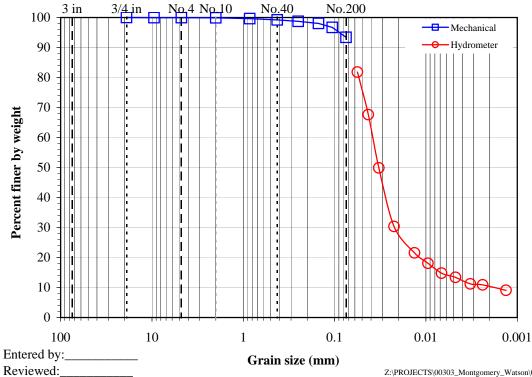
No: 00303-014 **Sample:**

Depth: 1-10' Location: FMC RDRA Data Gap Investigation Description: Brown silt Date: 11/18/2013

By: BRR

2) .	Ditti								
	_	•		Water	content data	C.F.(+3/8")	S.F.(-3/8")	Hyd.(+No.10	Hyd.(-No.10)
	Split sieve:	Yes		Moist so	oil + tare (g):	140.19	485.30	36.95	60.98
	Split sieve:	3/8"		Dry so	oil + tare (g):	140.06	464.88	36.95	60.64
		Moist	Dry		Tare (g):	124.07	124.07	36.93	37.60
Total sar	mple wt. (g):	21537.22	20320.52	Water	content (%):	0.81	5.99	0.00	1.48
+3/8" Coarse	fraction (g):	16.12	15.99	Hyd	rometer data			Slope:	-0.1641
-3/8" Split	fraction (g):	373.84	373.84		Hyd. split:	No.10		Intercept:	16.3
Hydrometer	fraction (g):	57.15	56.32		Gs:	2.65	Assumed	α:	1.00
S	plit fraction:	0.999			Bulb No.	2]	Hyd. fraction:	99.92
	Dispersion 1			Dispersion p	period (min):	15	Disp	ersion device:	Air-jet
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	18.2	50	0.05616	81.82
6"		150			1 1	10.2	42	0.04291	67.62

					().				
	Accum.	Grain Size	Percent		Elapsed time	Temp.	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	18.2	50	0.05616	81.82
6"	-	150	-		1	18.2	42	0.04281	67.63
4"	-	100	-		2	18.2	32	0.03281	49.88
3"	-	75	-		5	18.2	21	0.02238	30.37
1.5"	-	37.5	-		15	18.3	16	0.01331	21.54
3/4"	-	19	100.0		30	18.6	14	0.00949	18.10
3/8"	15.99	9.5	99.9	<=Split	60	19.1	12	0.00675	14.75
No.4	-	4.75	99.9		120	20.1	11	0.00474	13.36
No.10	0.01	2	99.9	<=Split hyd.	250	21.4	9.5	0.00326	11.21
No.20	0.15	0.85	99.7		453	22.8	9	0.00239	10.86
No.40	0.40	0.425	99.2		1477	22.8	8	0.00133	9.09
No.60	0.67	0.25	98.7						
No.100	1.06	0.15	98.0						
No.140	1.82	0.106	96.7						
No.200	3.67	0.075	93.4						



Grain size (mm)

 $Z: \label{local_projects} Z: \label{local_projects} \label{local_projects} O 303_Montgomery_Watson \\ \label{local_projects} O 14_FMC_Pocatello \\ \label{local_projects} [GSD+hyd_double.xls] \\ 10a \label{local_projects} O 14_FMC_Pocatello \\ \$

Gravel (%): 0.1

Sand (%): 6.5

Fines (%): 93.4

(ASTM D422)



Project: MWH Boring No.: WUA-TP010-01

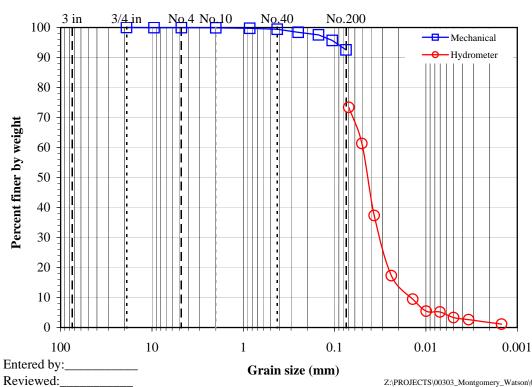
No: 00303-014 Sample:

Location: FMC RDRA Data Gap Investigation
Date: 11/18/2013

Depth: 1-10'
Description: Brown silt

By: BRR

	Diat			Water	content data	C.F.(+3/8")	S.F.(-3/8")	Hyd.(+No.10)	Hyd.(-No.10)
	Split sieve:	Yes			il + tare (g):	140.19	485.30	36.95	60.98
	Split sieve:	3/8"		Dry so	il + tare (g):	140.06	464.88	36.95	60.64
		Moist	Dry		Tare (g):	124.07	124.07	36.93	37.60
Total san	nple wt. (g):	21537.22	20320.52	Water	content (%):	0.81	5.99	0.00	1.48
+3/8" Coarse	fraction (g):	16.12	15.99	Hyd	rometer data			Slope:	-0.1641
-3/8" Split	fraction (g):	373.84	373.84		Hyd. split:	No.10		Intercept:	16.3
Hydrometer	fraction (g):	25.32	24.95		Gs:	2.65	Assumed	α:	1.00
S_1	plit fraction:	0.999			Bulb No.	2]	Hyd. fraction:	99.92
				Vacuum p	eriod (min):	10		ersion device:	None
	Accum.	Grain Size			Elapsed time	-	Hydrometer	Grain Size	% Soil in
Sieve	Wt. Ret. (g)	(mm)	Finer		(min)	(°C)	Reading	(mm)	Suspension
8"	-	200	-		0.5	20.7	18	0.06991	73.36
6"	-	150	-		1	20.7	15	0.05034	61.35
4"	-	100	-		2	20.7	9	0.03684	37.32
3"	-	75	-		5	20.7	4	0.02394	17.30
1.5"	-	37.5	-		15	20.8	2	0.01395	9.42
3/4"	-	19	100.0		30	20.8	1	0.00991	5.42
3/8"	15.99	9.5	99.9	<=Split	60	20.6	1	0.00703	5.15
No.4	-	4.75	99.9		120	20.7	0.5	0.00497	3.28
No.10	0.01	2	99.9	<=Split hyd.	250	21.7	0	0.00341	2.62
No.20	0.05	0.85	99.7		1363	20.6	0	0.00148	1.15
No.40	0.13	0.425	99.4						
No.60	0.38	0.25	98.4						
No.100	0.59	0.15	97.6						
No.140	1.06	0.106	95.7						
No.200	1.85	0.075	92.5						



Gravel (%): 0.1 Sand (%): 7.4 Fines (%): 92.5

Comments:

Vacuum applied and no flocculating agent used.



(ASTM D6572)

Project: MWH Boring No.: WUA-TP001-01

No: 00303-014 Sample: Location: FMC RDRA Data Gap Investigation **Depth: 1-10'**

Date: 12/3/2013 Sample Description: Brown silty clay By: BRR

Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs: 2.65 Assumed 0 minutes Curing Time: Water used: Distilled Water content: Natural Wet soil + tare (g)61.86 Dry soil + tare (g) 58.92 Tare (g) 37.78 Water content, w (%) 13.9

Initial water temperature: 20.1 $^{\circ}\mathrm{C}$

Date test started: 11/20/2013

Time at beginning of test: 9:31

Specimen _	2 m	2 minutes		hour	6 hours	
Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)
1	2	20.2	2	19.6	2	19.4
2	2	20	2	19.3	2	19.5
3	1	19.5	1	18.8	2	20
4	1	19.7	1	19	2	20.2

Dispersive classification: Grade 2-Intermediate

Entered:	
Reviewed:	



(ASTM D6572)

Project: MWH Boring No.: WUA-TP002-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 12/3/2013 Sample Description: Brown clay
By: BRR Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs: 2.65 Assumed
Curing Time: 0 minutes

Water used: Distilled
Water content: Natural

Wet soil + tare (g) 51.71
Dry soil + tare (g) 49.86

Dry soil + tare (g) 49.86

Tare (g) 36.95

Water content, w (%) 14.3

Initial water temperature: 20 °C

Date test started: 11/20/2013

Time at beginning of test: 9:32

Specimen _	2 m	2 minutes		hour	6 hours	
Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)
1	2	20	2	19.2	2	19.6
2	2	20	2	19.2	2	19.6
3	1	19.5	1	18.9	2	19.9
4	2	19.7	2	19	2	20

Dispersive classification: Grade 2-Intermediate

Entered:	
Reviewed:	



(ASTM D6572)

Project: MWH Boring No.: WUA-TP003-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 12/3/2013 Sample Description: Brown silty clay
By: BRR Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs: 2.65 Assumed

Curing Time: 0 minutes

Water used: Distilled

Water content: Natural

Wet soil + tare (g) 76.19

Dry soil + tare (g) 74.20

Tare (g) 37.76

Water content, w (%) 5.5

Initial water temperature: 19.9 °C

Date test started: 11/20/2013

Time at beginning of test: 9:32

Specimen	2 m	2 minutes		hour	6 hours	
Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)
1	3	19.9	3	19.1	2	19.5
2	3	20	3	19.1	2	19.7
3	1	20.1	1	19.3	1	18.5
4	1	20	1	19.2	1	18.5

Dispersive classification: Grade 3-Dispersive

Entered:	
Reviewed:	



(ASTM D6572)

Project: MWH Boring No.: WUA-TP004-01

No: 00303-014

Location: FMC RDRA Data Gap Investigation
Date: 12/3/2013

Sample:

Depth: 1-10'
Sample Description: Brown silt

By: BRR Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs: 2.65 Assumed
Curing Time: 0 minutes

Water used: Distilled
Water content: Natural

Wet soil + tare (g) 59.79

Dry soil + tare (g) 58.67

Tare (g) 37.72

Water content, w (%) 5.3

Initial water temperature: 19.6 °C

Date test started: 11/21/2013

Time at beginning of test: 9:06

Specimen	2 m	inutes	1	hour	6 hours	
Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)
1	1	19.7	2	18.1	1	18.3
2	2	19.6	1	18	1	18.3

Dispersive classification: Grade 1-Nondispersive

Entered:	
Reviewed:	



(ASTM D6572)

Project: MWH Boring No.: WUA-TP005-01

No: 00303-014

Location: FMC RDRA Data Gap Investigation
Date: 12/3/2013

Sample:

Depth: 1-10'
Sample Description: Brown silt

By: BRR Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs:	2.65	Assumed	
Curing Time:	0	minutes	
Water used:	Distilled		
Water content:	Natural		
Wet soil + tare (g)	63.86		
Dry soil + tare (g)	62.44		
Tare (g)	37.70		
Water content, w (%)	5.7		

Initial water temperature: 19.5 °C

Date test started: 11/21/2013

Time at beginning of test: 9:06

Specimen	2 m	2 minutes		1 hour		6 hours	
Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)	
1	1	19.5	1	17.8	1	18.3	
2	2	19.5	1	17.9	1	18.3	

Dispersive classification: Grade 1-Nondispersive

Entered:	
Reviewed:	



(ASTM D6572)

Project: MWH Boring No.: WUA-TP006-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 12/3/2013 Sample Description: Brown silty clay
By: BRR Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs:	2.65	Assumed	
Curing Time:	0	minutes	
Water used:	Distilled		
Water content:	Natural		
Wet soil + tare (g)	61.25		
Dry soil + tare (g)	59.25		
Tare (g)	37.25		
Water content, w (%)	9.1		

Initial water temperature: 19.6 °C

Date test started: 11/21/2013

Time at beginning of test: 9:06

Specimen	2 m	2 minutes		1 hour		6 hours	
 Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)	
1	2	19.5	2	18	2	18.3	
2	3	19.6	3	18	3	18.3	

Dispersive classification: Grade 3-Dispersive

Entered:	
Reviewed:	



(ASTM D6572)

Project: MWH Boring No.: WUA-TP007-01

No: 00303-014

Location: FMC RDRA Data Gap Investigation
Date: 12/3/2013

Sample:

Depth: 1-10'
Sample Description: Brown silt

By: BRR Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs: 2.65 Assumed 0 minutes Curing Time: Water used: Distilled Water content: Natural Wet soil + tare (g)68.30 Dry soil + tare (g) 65.27 Tare (g) 37.59 Water content, w (%) 10.9

Initial water temperature: 19 °C

Date test started: 11/22/2013

Time at beginning of test: 8:58

Specimen	2 m	2 minutes		1 hour		6 hours	
Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)	
1	1	18.9	1	18.4	1	18.2	
2	2	19	2	18.3	2	18.4	

Dispersive classification: Grade 2-Intermediate

Entered:	
Reviewed:	



(ASTM D6572)

Project: MWH Boring No.: WUA-TP008-01

No: 00303-014

Location: FMC RDRA Data Gap Investigation
Date: 12/3/2013

Sample:

Depth: 1-10'
Sample Description: Brown silt

By: BRR Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs: 2.65 Assumed 0 minutes Curing Time: Water used: Distilled Water content: Natural Wet soil + tare (g)63.64 Dry soil + tare (g) 62.32 Tare (g) 37.82 Water content, w (%) 5.4

Initial water temperature: 19.1 °C

Date test started: 11/22/2013

Time at beginning of test: 8:58

Specimen	2 minutes		1 hour		6 hours	
Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)
1	3	19.1	3	18.3	3	18.2
2	1	19	1	18.4	1	18.2

Dispersive classification: Grade 2-Intermediate

Entered:	
Reviewed:	



(ASTM D6572)

Project: MWH Boring No.: WUA-TP009-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 12/3/2013 Sample Description: Brown silty clay

By: BRR Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs:	2.65	Assumed	
Curing Time:	0	minutes	
Water used: 1	Distilled		
Water content:	Natural		
Wet soil + tare (g)	55.50		
Dry soil + tare (g)	54.17		
Tare (g)	38.14		
Water content, w (%)	8.3		

Initial water temperature: 19 °C

Date test started: 11/22/2013

Time at beginning of test: 8:58

Specimen	Specimen 2 minutes		1	hour	6 hours		
Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)	
1	1	19	1	18.4	1	18.2	
2	1	19	1	18.4	1	18.2	

Dispersive classification: Grade 1-Nondispersive

Entered:	
Reviewed:	



(ASTM D6572)

Project: MWH Boring No.: WUA-TP010-01

No: 00303-014

Location: FMC RDRA Data Gap Investigation
Date: 12/3/2013

Sample:

Depth: 1-10'
Sample Description: Brown silt

By: BRR Engineering Classification: Not requested

Specimen Type: Natural irregularly shaped crumb

Specific Gravity, Gs: 2.65 Assumed
Curing Time: 0 minutes

Water used: Distilled
Water content: Natural

Wet soil + tare (g) 55.73

Dry soil + tare (g) 54.92

Tare (g) 37.60

4.7

Initial water temperature: 19.8 °C

Date test started: 11/26/2013

Time at beginning of test: 8:58

Water content, w (%)

Specimen	Specimen 2 minutes		1	hour	6 hours		
Number	Grade	Temp. (°C)	Grade	Temp. (°C)	Grade	Temp. (°C)	
1	1	20	1	19.1	1	20.7	
2	1	19.7	1	19	1	20	

Dispersive classification: Grade 1-Nondispersive

Entered:	
Reviewed:	

(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP001-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/21/2013 Sample Description: Brown silty clay
By: MP Engineering Classification: Not requested
As-received water content (%): Not requested

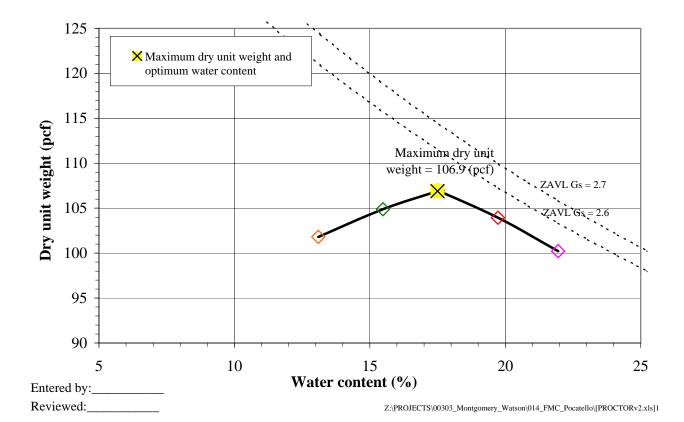
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 2 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0332 Rock Correction: No

Optimum water content (%): 17.5 Maximum dry unit weight (pcf): 106.9

Point Number	+4%	+6%	+2%	+8%	As Is		
Wt. Sample + Mold (g)	6055.2	6036.4	5986.4	6003.0	5896.2		
Wt. of Mold (g)	4160.1	4160.1	4160.1	4160.1	4160.1		
Wet Unit Wt., γ _m (pcf)	125.7	124.4	121.1	122.2	115.1		
Wet Soil + Tare (g)	565.86	646.42	627.72	578.78	537.19		
Dry Soil + Tare (g)	499.95	563.05	560.18	497.56	489.13		
Tare (g)	123.73	140.46	123.93	127.54	122.22		
Water Content, w (%)	17.5	19.7	15.5	22.0	13.1		
Dry Unit Wt., γ _d (pcf)	106.9	103.9	104.9	100.2	101.8		



(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP002-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/21/2013 Sample Description: Brown clay
By: DKS Engineering Classification: Not requested
As-received water content (%): Not requested

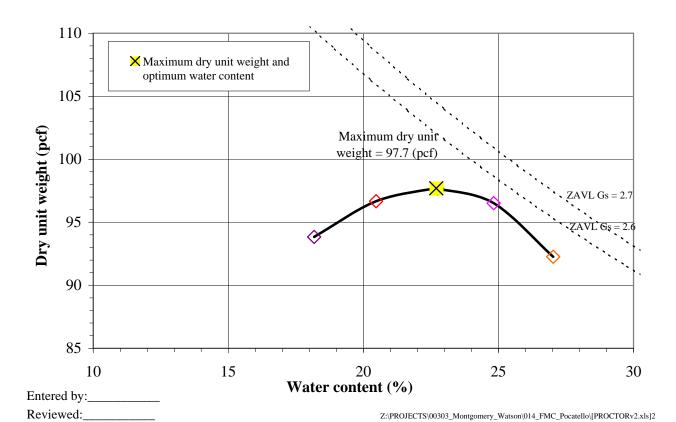
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 2 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0332 Rock Correction: No

Optimum water content (%): 22.7 Maximum dry unit weight (pcf): 97.7

Point Number	+4%	+6%	+8%	+10%	+12%		
Wt. Sample + Mold (g)	5832.2	5916.0	5967.7	5976.6	5927.2		
Wt. of Mold (g)	4160.1	4160.1	4160.1	4160.1	4160.1		
Wet Unit Wt., γ _m (pcf)	110.9	116.5	119.9	120.5	117.2		
Wet Soil + Tare (g)	629.80	842.24	824.58	833.17	945.37		
Dry Soil + Tare (g)	551.61	723.01	694.50	691.81	790.71		
Tare (g)	121.43	140.49	122.65	122.35	218.49		
Water Content, w (%)	18.2	20.5	22.7	24.8	27.0		
Dry Unit Wt., γ _d (pcf)	93.8	96.7	97.7	96.5	92.3		



(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP003-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/21/2013 Sample Description: Brown silty clay
By: MP/DKS Engineering Classification: Not requested
As-received water content (%): Not requested

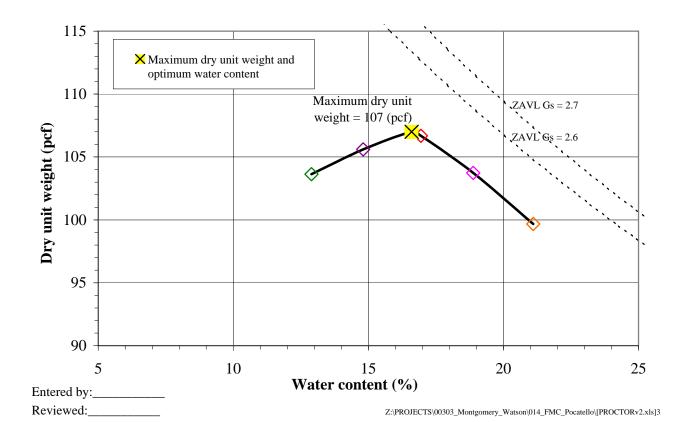
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 2 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0332 Rock Correction: No

Optimum water content (%): 16.6 Maximum dry unit weight (pcf): 107

Point Number	+8%	+10%	+6%	+12%	+14%		
Wt. Sample + Mold (g)	5988.2	6041.3	5924.3	6019.6	5980.3		
Wt. of Mold (g)	4160.1	4160.1	4160.1	4160.1	4160.1		
Wet Unit Wt., γ_m (pcf)	121.2	124.8	117.0	123.3	120.7		
Wet Soil + Tare (g)	866.98	843.94	686.43	765.24	862.82		
Dry Soil + Tare (g)	770.44	740.20	622.12	665.90	734.68		
Tare (g)	118.56	127.94	123.43	139.73	127.41		
Water Content, w (%)	14.8	16.9	12.9	18.9	21.1		
Dry Unit Wt., γ _d (pcf)	105.6	106.7	103.6	103.7	99.7		



(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP004-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/21/2013 Sample Description: Brown silt

By: MP/DKS Engineering Classification: Not requested

As-received water content (%): Not requested

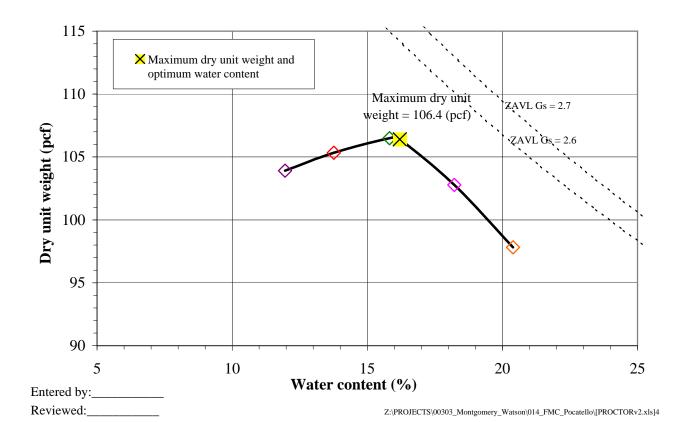
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 2 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0332 Rock Correction: No

Optimum water content (%): 16.2 Maximum dry unit weight (pcf): 106.4

Point Number	+6%	+8%	+10%	+12%	+14%		
Wt. Sample + Mold (g)	5914.3	5967.1	6019.8	5992.2	5936.0		
Wt. of Mold (g)	4160.1	4160.1	4160.1	4160.1	4160.1		
Wet Unit Wt., γ _m (pcf)	116.3	119.8	123.3	121.5	117.8		
Wet Soil + Tare (g)	793.31	785.16	729.94	720.77	811.93		
Dry Soil + Tare (g)	721.64	705.54	647.18	631.53	704.92		
Tare (g)	122.18	127.09	124.09	141.72	180.27		
Water Content, w (%)	12.0	13.8	15.8	18.2	20.4		
Dry Unit Wt., γ _d (pcf)	103.9	105.3	106.5	102.8	97.8		



(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP005-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/21/2013

By: BRR/DKS

Engineering Classification: Not requested

As-received water content (%): Not requested

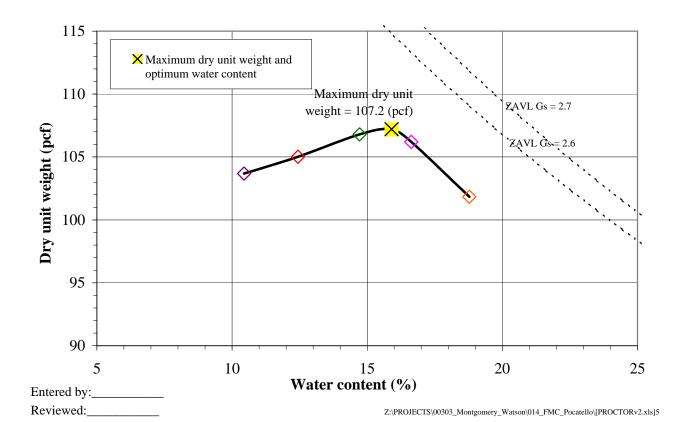
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 3 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0332 Rock Correction: No

Optimum water content (%): 15.9 Maximum dry unit weight (pcf): 107.2

Point Number	+4%	+6%	+8%	+10%	+12%		
Wt. Sample + Mold (g)	5895.4	5949.1	6015.9	6036.1	5992.4		
Wt. of Mold (g)	4169.7	4169.7	4169.7	4169.7	4169.7		
Wet Unit Wt., γ_m (pcf)	114.5	118.1	122.5	123.9	121.0		
Wet Soil + Tare (g)	877.44	816.01	868.81	804.39	907.87		
Dry Soil + Tare (g)							
Tare (g)	219.83	226.30	211.70	179.20	127.34		
Water Content, w (%)	10.4	12.4	14.7	16.6	18.8		
Dry Unit Wt., γ _d (pcf)	103.7	105.0	106.8	106.2	101.8		



(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP006-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/8/2013 Sample Description: Brown silty clay
By: ET Engineering Classification: Not requested
As-received water content (%): Not requested

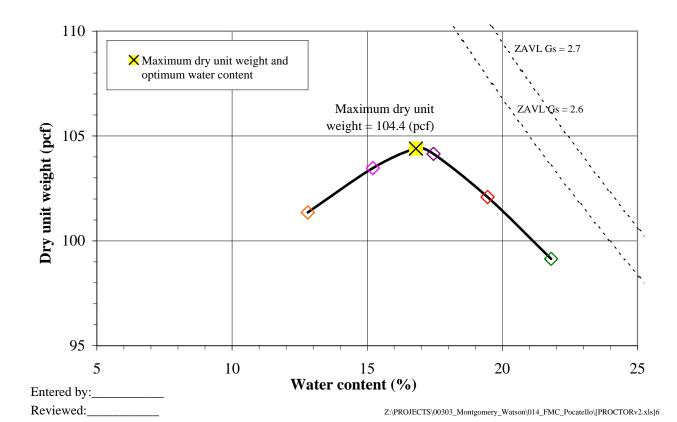
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 1 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0333 Rock Correction: No

Optimum water content (%): 16.8 Maximum dry unit weight (pcf): 104.4

Point Number	+4%	+6%	+8%	+2%	As Is		
Wt. Sample + Mold (g)	6092.6	6086.9	6068.9	6045.5	5971.9		
Wt. of Mold (g)	4245.5	4245.5	4245.5	4245.5	4245.5		
Wet Unit Wt., γ _m (pcf)	122.3	121.9	120.8	119.2	114.3		
Wet Soil + Tare (g)	722.48	636.60	623.79	729.81	633.94		
Dry Soil + Tare (g)	633.59	553.79	539.10	662.84	575.98		
Tare (g)	124.34	128.08	150.65	222.53	123.25		
Water Content, w (%)	17.5	19.5	21.8	15.2	12.8		
Dry Unit Wt., γ _d (pcf)	104.1	102.1	99.1	103.5	101.4		



(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP007-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/8/2013 Sample Description: Brown silt
By: ET Engineering Classification: Not requested
As-received water content (%): Not requested

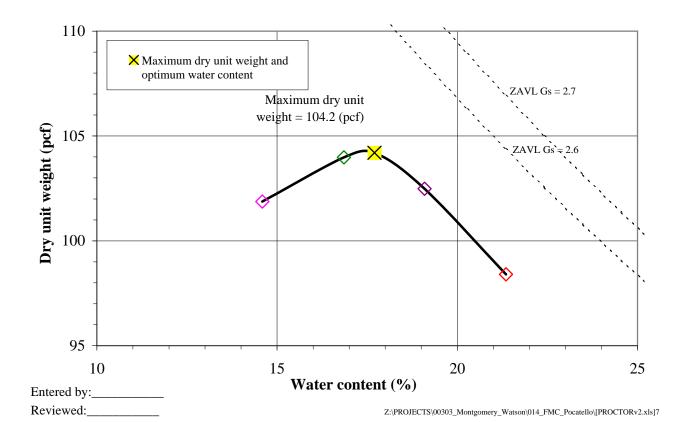
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 3 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0332 Rock Correction: No

Optimum water content (%): 17.7 Maximum dry unit weight (pcf): 104.2

Point Number	+10%	+12%	+8%	+6%		
Wt. Sample + Mold (g)	6008.9	5969.1	6000.7	5928.8		
Wt. of Mold (g)	4169.7	4169.7	4169.7	4169.7		
Wet Unit Wt., γ _m (pcf)	122.1	119.4	121.5	116.7		
Wet Soil + Tare (g)	750.80	683.42	649.06	663.82		
Dry Soil + Tare (g)	664.27	594.80	573.97	595.63		
Tare (g)	210.99	179.73	128.42	128.20		
Water Content, w (%)		21.4	16.9	14.6		
Dry Unit Wt., γ _d (pcf)	102.5	98.4	104.0	101.9		



Laboratory Compaction Characteristics of Soil

(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP008-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/11/2013

By: MP

Engineering Classification: Not requested

As-received water content (%): Not requested

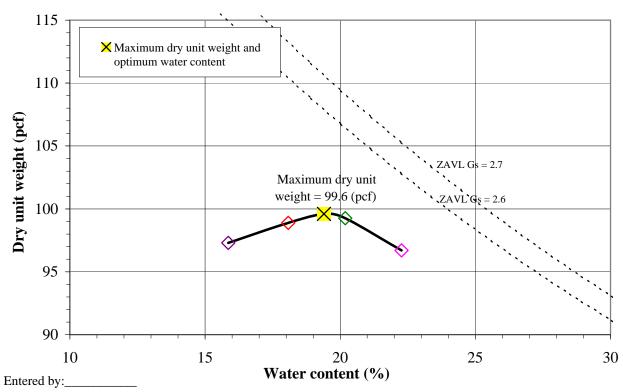
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 1 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0333 Rock Correction: No

Optimum water content (%): 19.4 Maximum dry unit weight (pcf): 99.6

Point Number	+6%	+8%	+10%	+12%		
Wt. Sample + Mold (g)	5947.5	6008.6	6046.7	6030.8		
Wt. of Mold (g)	4245.4	4245.4	4245.4	4245.4		
Wet Unit Wt., γ _m (pcf)	112.7	116.8	119.3	118.2		
Wet Soil + Tare (g)	793.10	730.81	657.43	631.47		
Dry Soil + Tare (g)	702.11	637.30	567.80	538.32		
Tare (g)	128.38	120.00	123.83	120.08		
Water Content, w (%)		18.1	20.2	22.3		
Dry Unit Wt., γ _d (pcf)	97.3	98.9	99.3	96.7		



Reviewed:_____

Laboratory Compaction Characteristics of Soil

(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP009-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/11/2013 Sample Description: Brown silty clay
By: MP Engineering Classification: Not requested
As-received water content (%): Not requested

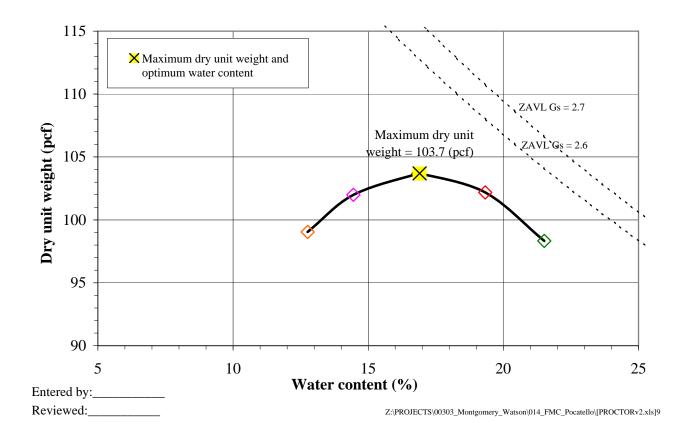
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 1 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0333 Rock Correction: No

Optimum water content (%): 16.9 Maximum dry unit weight (pcf): 103.7

Point Number	+8%	+10%	+12%	+6%	+4%		
Wt. Sample + Mold (g)	6074.9	6086.5	6049.5	6008.0	5931.7		
Wt. of Mold (g)	4245.4	4245.4	4245.4	4245.4	4245.4		
Wet Unit Wt., γ_m (pcf)	121.2	121.9	119.5	116.7	111.7		
Wet Soil + Tare (g)	596.34	653.19	684.40	585.10	677.28		
Dry Soil + Tare (g)	528.63	567.41	584.85	527.23	626.00		
Tare (g)	126.90	123.67	122.09	126.80	224.06		
Water Content, w (%)		19.3	21.5	14.5	12.8		
Dry Unit Wt., γ _d (pcf)	103.7	102.2	98.3	102.0	99.0		



Laboratory Compaction Characteristics of Soil

(ASTM D698 / D1557)



Project: MWH Boring No.: WUA-TP010-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 11/11/2013 Sample Description: Brown silt

By: MP Engineering Classification: Not requested

As-received water content (%): Not requested

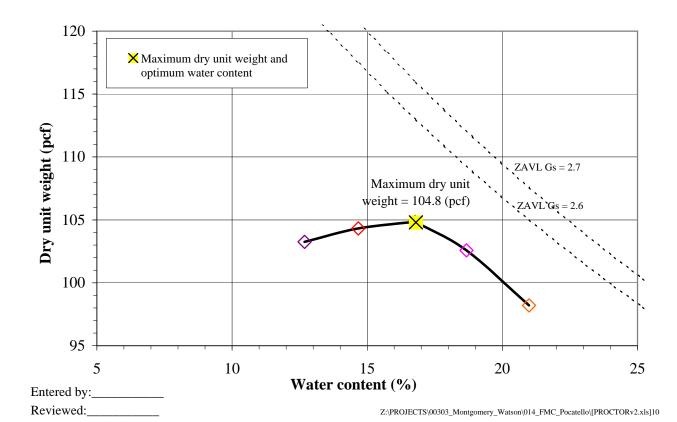
Method: ASTM D698 B Preparation method: Moist

Mold Id. Inc 1 Rammer: Mechanical-circular face

Mold volume (ft³): 0.0333 Rock Correction: No

Optimum water content (%): 16.8 Maximum dry unit weight (pcf): 104.8

Point Number	160%	+8%	+10%	1120%	+14%		
Wt. Sample + Mold (g)	6002.2	6051.8	6093.8	6083.6	6039.4		
Wt. of Mold (g)	4245.4	4245.4	4245.4	4245.4	4245.4		
Wet Unit Wt., γ _m (pcf)	116.3	119.6	122.4	121.7	118.8		
Wet Soil + Tare (g)	609.52	667.87	818.15	672.08	834.00		
Dry Soil + Tare (g)							
Tare (g)	118.33	128.44	123.65	129.44	211.70		
Water Content, w (%)	12.7	14.7	16.8	18.7	21.0		
Dry Unit Wt., γ _d (pcf)	103.3	104.3	104.8	102.6	98.2		



Initial (o) Final (f)



Wall Permeameter, Method C (ASTM D5084)

Project: MWH
No: 00303-014

Location: FMC RDRA Data Gap Investigation

Date: 11/19/2013

By: JDF

Boring No.: WUA-TP001-01

Sample:

Depth: 1-10'

Sample Description: Brown silty clay

Sample Type: Laboratory Compacted

Compaction Specifications: 85 (%) Dry unit weight

at 8.5 (%) w

Optimum water content (%) 17.5 Maximum dry unit weight (pcf) 106.9

Gs 2.67 Assumed

5.076

Cell No. 2 Station No. 1

Permeant liquid used De-aired tap water

Total backpressure (psi) 30 Effective horiz. consolidation stress (psi) 5

Effective vert. consolidation stress (psi) _____5

Conversion, reading to cm head (cm/rd)

4 ,		
	Initial (o)	Final (f)
B value	0.86	0.96
External Burette (cm ³)	8.30	16.70
Cell Pressure (psi)	0.0	35.0
Backpressure bottom (psi)	30.0	
Backpressure top (psi)	30.0	
System volume coefficient (cm³/psi)	0.158	
System volume change (cm ³)	5.52	
Net sample volume change (cm ³)	-2.88	
Bottom burette ground length, l _b (cm)	82.00	
Top burette ground length, l_t (cm)	82.1	
Burette area, a (cm ²)	0.197	

 ^a Saturation set to 100% for phase calculations ^b K corrected to 20°C 					
Average K ^b (cm/sec)	3.3E-05				
Saturation (%), for assumed Gs	26.6	100 ^a			
Void ratio, e, for assumed Gs	0.83	0.79			
Dry Unit Wt, γ _d (pcf)	90.9	92.1			
Water Content, w (%)	8.30	29.44			
Weight of solids, Ws (g)	326.90	326.90			
Tare (g)	126.81	128.2			
Dry Soil + Tare (g)	242.16	455.37			
Wet Soil + Tare (g)	251.73	551.68			
Wet Unit Wt., γ_m (pcf)	98.5	119.2			
Wt. Rings (g)	0	0			
Wt. Rings + Wet Soil (g)	354.02	423.13			
Sample Volume, V (cm ³)	224.41	221.52			
Sample Area, A (cm ²)	29.332	29.017			
Sample Length, L (cm)	7.650	7.634			
Sample Diameter, D (in)	2.406	2.39			
Sample Height, H (in)	3.012	3.006			

Elapsed	Bottom Burette	Top Burette	h ₁	h_2	K	Temp	Visc. Ratio	K ^b
time (sec)	(cm ³)	(cm^3)	(cm)	(cm)	(cm/sec)	(°C)	$R_{\rm f}$	(cm/sec
1080.0	1.20 4.12	8.72 5.80	38.07	8.43	3.6E-05	22.4	0.94	3.4E-05
1260.0	0.38 4.18	9.62 5.80	46.80	8.12	3.6E-05	22.8	0.93	3.4E-05
1020.0	0.42 3.78	9.54 6.20	46.19	12.18	3.4E-05	21.5	0.96	3.3E-05
960.0	0.44 3.70	9.54 6.28	46.09	13.00	3.4E-05	21.5	0.96	3.3E-05
60.0	0.00 0.40	10.00 9.60	50.66	46.60	3.6E-05	22.6	0.94	3.4E-05
960.0	0.40 3.70	9.60 6.28	46.60	13.00	3.4E-05	22.6	0.94	3.2E-05

Entered by:_	
Daviaryadı	



Wall Permeameter, Method C (ASTM D5084)

Project: MWH No: 00303-014

Location: FMC RDRA Data Gap Investigation

Date: 11/19/2013

By: JDF

Boring No.: WUA-TP004-01

Sample:

Depth: 1-10'

Sample Description: Brown silt

Sample Type: Laboratory Compacted

Compaction Specifications: 85 (%) Dry unit weight

> 9.0 (%) w

Optimum water content (%) 16.2 Maximum dry unit weight (pcf) 106.4

> Gs 2.67 Assumed

T1 Cell No. Station No. 2

Permeant liquid used De-aired tap water

Total backpressure (psi) 30

Effective horiz. consolidation stress (psi) 5 5 Effective vert. consolidation stress (psi)

Initial (o) Final (f) 0.94 B value

0.98 External Burette (cm³) 12.20 21.40 Cell Pressure (psi) 0.0 35.0 Backpressure bottom (psi) 30.0 Backpressure top (psi) 30.0 System volume coefficient (cm³/psi) 0.119 System volume change (cm³) 4.17

Net sample volume change (cm³) -5.03

Bottom burette ground length, l_b (cm) 81.99 Top burette ground length, l_t (cm) 81.97 Burette area, a (cm²)

Conversion, reading to cm head (cm/rd) 5.076

0.197

	Initial (o)	Final (f)			
Sample Height, H (in)	3.011	3.000			
Sample Diameter, D (in)	2.403	2.38			
Sample Length, L (cm)	7.648	7.619			
Sample Area, A (cm^2)	29.259	28.709			
Sample Volume, V (cm ³)	223.77	218.74			
Wt. Rings + Wet Soil (g)	1111.29	423.74			
Wt. Rings (g)	758.93	0			
Wet Unit Wt., γ _m (pcf)	98.3	120.9			
Wet Soil + Tare (g)	328.04	535.3			
Dry Soil + Tare (g)	312.2	436.67			
Tare (g)	139.72	121.57			
Weight of solids, Ws (g)	322.72	322.72			
Water Content, w (%)	9.18	31.30			
Dry Unit Wt, γ _d (pcf)	90.0	92.1			
Void ratio, e, for assumed Gs	0.85	0.84			
Saturation (%), for assumed Gs	28.8	100 ^a			
Average K ^b (cm/sec)	1.4F	E-04			
^a Saturation set to 100% for phase calculations ^b K corrected to 20°C					

Start Date and	1 Time: 11/18/13	8:40						
Elapsed	Bottom Burette	Top Burette	h_1	h_2	K	Temp	Visc. Ratio	K^{b}
time (sec)	(cm ³)	(cm^3)	(cm)	(cm)	(cm/sec)	(°C)	R_{f}	(cm/sec)
60.0	0.00	10.00	50.78	35.96	1.5E-04	22.0	0.95	1.4E-04
00.0	1.48	8.56	30.78	33.90	1.3E-04	22.0	0.93	1.4E-04
240.0	1.48	8.56	35.96	9.46	1.5E-04	22.1	0.95	1.4E-04
240.0	4.12	5.98	33.70	7.40	1.JL-0 1	22.1	0.73	
60.0	0.00	10.00	50.78	8 36.06 1.5E-	1.5E-04	E-04 21.0	0.98	1.5E-04
00.0	1.44 8.54	30.00	1.52 01	-1.0	0.50	1.02 0.		
240.0	1.44	8.54	36.06	36.06 9.26	1.5E-04	20.8	0.98	1.5E-04
210.0	4.10	5.92	30.00					
60.0	0.00	10.00	50.78	36.26	1.5E-04	22.9	0.93	1.4E-04
00.0	1.42	8.56	30.70	30.20	1.52 01	22.7	0.75	1.12 01
240.0	1.42	8.56	36.26	9.16	1.5E-04	21.9	0.95	1.4E-04
240.0	4.10	5.90	30.20	7.10	1.512-04	21.7	0.75	1.46-04

Entered by:	
Reviewed:	

Final (f)

2.996

2.36

7.610

28.322

215.51

411.81

0

119.3

534.21

440.58

122.43

318.17

29.43

92.2

0.79 100 a

Initial (o)

3.014

2.401

7.656

29.211

223.62

346.12

0

96.6

304.54

289.91

123.34

318.17

8.78

88.8

0.88

26.8

2.3E-05



Wall Permeameter, Method C (ASTM D5084)

Sample Height, H (in)

Sample Diameter, D (in)

Sample Length, L (cm)

Sample Area, A (cm²)

Sample Volume, V (cm³)

Wt. Rings + Wet Soil (g)

Wet Unit Wt., γ_m (pcf)

Weight of solids, Ws (g)

Void ratio, e, for assumed Gs

Saturation (%), for assumed Gs

Average K^b (cm/sec)

K corrected to 20°C

Water Content, w (%)

Dry Unit Wt, γ_d (pcf)

Saturation set to 100% for phase calculations

Wet Soil + Tare (g)

Dry Soil + Tare (g)

Wt. Rings (g)

Tare (g)

Project: MWH No: 00303-014

Location: FMC RDRA Data Gap Investigation

Date: 11/19/2013

By: JDF

Boring No.: WUA-TP006-01

Sample:

Depth: 1-10'

Sample Description: Brown silty clay

Sample Type: Laboratory Compacted

Compaction Specifications: 85 (%) Dry unit weight

> 8.5 (%) w

Optimum water content (%) 16.8 Maximum dry unit weight (pcf) 104.4

> Gs 2.67 Assumed

T2 Cell No. Station No. 3

Permeant liquid used De-aired tap water

Total backpressure (psi) 30 Effective horiz. consolidation stress (psi) 5

Effective vert. consolidation stress (psi)

	Initial (o)	Final (f)
B value	0.88	0.96
External Burette (cm ³)	10.50	22.40
Cell Pressure (psi)	0.0	35.0
Backpressure bottom (psi)	30.0	
Backpressure top (psi)	30.0	
System volume coefficient (cm³/psi)	0.108	
System volume change (cm ³)	3.79	
Net sample volume change (cm ³)	-8.11	
Bottom burette ground length, l_b (cm)	82.10	
Top burette ground length, l_t (cm)	81.9	
Dynastic area a (am ²)	0.107	

	minai (0)	1 mai (1)
B value	0.88	0.96
External Burette (cm ³)	10.50	22.40
Cell Pressure (psi)	0.0	35.0
Backpressure bottom (psi)	30.0	
Backpressure top (psi)	30.0	
System volume coefficient (cm³/psi)	0.108	
System volume change (cm ³)	3.79	
Net sample volume change (cm ³)	-8.11	
Bottom burette ground length, l _b (cm)	82.10	
Top burette ground length, l_t (cm)	81.9	
Burette area, a (cm ²)	0.197	
Conversion, reading to cm head (cm/rd)	5.076	

Start Date and		9:12						h
Elapsed	Bottom Burette	Top Burette	h_1	h_2	K	Temp	Visc. Ratio	K^{b}
time (sec)	(cm ³)	(cm ³)	(cm)	(cm)	(cm/sec)	(°C)	R_{f}	(cm/sec
180.0	0.00	10.00	50.96	43.04	2.5E-05	22.2	0.95	2.4E-05
160.0	0.76	9.20	30.50	45.04	2.3E-03	22.2	0.93	2.4E-0.
1080.0	0.76	9.20	43.04	16.04	2.4E-05	21.8	0.96	2.3E-05
1000.0	3.42	6.54	+J.UT	10.07	2. 4 L-03	21.0	0.70	2.JL-0.
600.0	3.42	6.54	16.04	9.13	2.5E-05	21.2	0.97	2.4E-0
000.0	4.10	5.86		7.13	2.51 05	21.2		2.70 0.
60.0	0.00	10.00	50.96	48.42	8.42 2.3E-05	22.1	0.95	2.1E-05
00.0	0.28	9.78	30.90	∓ 0.∓∠	2.31 03	22.1		
1320.0	0.28	9.78	48.42	15.33	2.3E-05	22.5	0.94	2.2E-05
1320.0	3.56	6.54	70.12	TO.T2 13.33 2.3E-03 22.3	15.55 2.515-05	22.5	0.71	2.21
60.0	0.00	10.00	50.96	48.22	2.4E-05	21.0	0.98	2.4E-0
00.0	0.26	9.72	30.70	70.22	2.TL 03	21.0	0.70	2.71
900.0	0.26	9.72	48.22	21.82	2.3E-05	22.0	0.95	2.2E-0
700.0	2.86	7.12	70.22	21.02			0.75	

C

Entered by:_	
Daviorade	



Wall Permeameter, Method C (ASTM D5084)

Project: MWH No: 00303-014

Location: FMC RDRA Data Gap Investigation

Date: 11/19/2013

By: JDF

Boring No.: WUA-TP007-01

Sample:

Depth: 1-10'

Sample Description: Brown silt

Sample Type: Laboratory Compacted

Compaction Specifications: 85 (%) Dry unit weight

at 8.5 (%) w

Optimum water content (%) 17.7 Maximum dry unit weight (pcf) 104.2

Gs 2.65 Assumed

5.076

Cell No. T3
Station No. 4

Permeant liquid used De-aired tap water

Total backpressure (psi) 30 Effective horiz. consolidation stress (psi) 5

Effective vert. consolidation stress (psi) 5

Initial (o) Final (f)

Conversion, reading to cm head (cm/rd)

	minual (0)	Tillal (1)
B value	0.84	1.00
External Burette (cm ³)	7.30	17.10
Cell Pressure (psi)	0.0	35.0
Backpressure bottom (psi)	30.0	
Backpressure top (psi)	30.0	
System volume coefficient (cm³/psi)	0.105	
System volume change (cm ³)	3.69	
Net sample volume change (cm ³)	-6.11	
Bottom burette ground length, l _b (cm)	81.90	
Top burette ground length, l_t (cm)	81.98	
Burette area, a (cm ²)	0.197	

	Initial (o)	Final (f)		
Sample Height, H (in)	3.007	2.993		
Sample Diameter, D (in)	2.409	2.38		
Sample Length, L (cm)	7.638	7.603		
Sample Area, A (cm ²)	29.406	28.735		
Sample Volume, V (cm ³)	224.59	218.48		
Wt. Rings + Wet Soil (g)	345.51	418.30		
Wt. Rings (g)	0	0		
Wet Unit Wt., γ _m (pcf)	96.0	119.5		
Wet Soil + Tare (g)	304.93	545.67		
Dry Soil + Tare (g)	291.11	446.57		
Tare (g)	123	127.09		
Weight of solids, Ws (g)	319.26	319.26		
Water Content, w (%)	8.22	31.02		
Dry Unit Wt, γ _d (pcf)	88.7	91.2		
Void ratio, e, for assumed Gs	0.86	0.82		
Saturation (%), for assumed Gs	25.2	100 ^a		
Average K ^b (cm/sec) 5.8E-05				
^a Saturation set to 100% for phase	e calculatio	ons		
^b K corrected to 20°C				

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	41.75 42.56 50.68	(cm) 10.88 9.87	(cm/sec) 5.8E-05 5.8E-05	(°C) 21.6 22.5	R _f 0.96 0.94	5.6E-05
600.0 3.96 6.12 660.0 0.80 9.20 4.04 6.00 60.0 0.00 10.00	41.75	9.87				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	42.56	9.87				
4.04 6.00 60.0 0.00 10.00	42.56) 50.68		5.8E-05	22.5	0.94	5.4E-05
4.04 6.00 60.0 0.00 10.00	50.68		J.6E-03	22.3	0.54	J.4L-03
60.0	5U 68					J.4L-03
0.70 9.30		3 43.57	6.6E-05	22.5	0.94	6.2E-05
0.70	20.00	73.37				
600.0 0.70 9.30	43.57	10.58	6.1E-05	22.5	0.94	5.8E-05
3.94 6.04	73.37	10.50	0.12 03	22.5	0.54	3.0L 03
60.0 0.00 10.00	50.68	43.88	6.3E-05	22.6	0.94	5.9E-05
0.72 9.38	50.00	13.00	0.52 05	22.0	0.51	3.7E 03
600.0 0.72 9.38	43.88	9.56	6.6E-05	22.6	0.94	6.2E-05
4.00 5.90	13.00	7.50	0.02 03	22.0	0.51	0.21 03

Entered by:_	
Daviarradi	



Wall Permeameter, Method C (ASTM D5084)

Project: MWH No: 00303-014

Location: FMC RDRA Data Gap Investigation

Date: 11/19/2013

By: JDF

Boring No.: WUA-TP008-01

Sample:

Depth: 1-10'

Sample Description: Brown silt

Sample Type: Laboratory Compacted

Compaction Specifications: 85 (%) Dry unit weight

at 8.5 (%) w

Optimum water content (%) 19.4 Maximum dry unit weight (pcf) 99.6

Gs 2.65 Assumed

Cell No. 3
Station No. 5

Permeant liquid used De-aired tap water

Total backpressure (psi) 30 Effective horiz. consolidation stress (psi) 5

Effective vert. consolidation stress (psi) 5

Conversion, reading to cm head (cm/rd)

	Initial (o)	Final (f)
B value	0.86	0.98
External Burette (cm ³)	12.60	23.20
Cell Pressure (psi)	0.0	35.0
Backpressure bottom (psi)	30.0	
Backpressure top (psi)	30.0	
System volume coefficient (cm³/psi)	0.151	
System volume change (cm ³)	5.29	
Net sample volume change (cm ³)	-5.31	
Bottom burette ground length, l_b (cm)	81.85	
Top burette ground length, l_t (cm)	81.9	
Burette area, a (cm ²)	0.197	

	Initial (o)	Final (f)		
Sample Height, H (in)	3.010	2.998		
Sample Diameter, D (in)	2.405	2.38		
Sample Length, L (cm)	7.645	7.615		
Sample Area, A (cm ²)	29.308	28.727		
Sample Volume, V (cm ³)	224.07	218.77		
Wt. Rings + Wet Soil (g)	330.21	410.65		
Wt. Rings (g)	0	0		
Wet Unit Wt., γ _m (pcf)	92.0	117.2		
Wet Soil + Tare (g)	379.66	536.54		
Dry Soil + Tare (g)	360.76	430.39		
Tare (g)	140.47	127.37		
Weight of solids, Ws (g)	304.12	304.12		
Water Content, w (%)	8.58	35.03		
Dry Unit Wt, γ _d (pcf)	84.7	86.8		
Void ratio, e, for assumed Gs	0.95	0.93		
Saturation (%), for assumed Gs	23.9	100 ^a		
Average K ^b (cm/sec) 7.8E-05				
^a Saturation set to 100% for phase	e calculatio	ons		
^b K corrected to 20°C				

11/15/13

9:35

Elapsed	Bottom Burette	Top Burette	h_1	h_2	K	Temp	Visc. Ratio	K^{b}
time (sec)	(cm^3)	(cm ³)	(cm)	(cm)	(cm/sec)	(°C)	$R_{ m f}$	(cm/sec)
420.0	1.68	8.30	33.55	8.68	8.4E-05	21.0	0.98	8.2E-05
420.0	4.12	5.84	33.33	0.00	0.4L-03	21.0 0.98	0.50	0.2L-03
480.0	0.96	9.06	41.07	9.29	8.1E-05	22.1	0.95	7.7E-05
460.0	4.10	5.94	41.07	7.49	0.1L-03	22.1	0.33	7.7L-03
480.0	0.92	9.08	41.37	9.59	59 7.9E-05 21.2 0.9	21.2	0.97	7.7E-05
400.0	4.06	5.96	41.57	7.57		0.77	7.7E-03	
480.0	0.92	9.06	41.27	9.54	e.54 8.0E-05	21.0	0.98	7.8E-05
460.0	4.05	5.94	41.27	9.54	8.0L-03			7.6E-03

Entered by:	
Reviewed:	

Start Date and Time:



Wall Permeameter, Method C (ASTM D5084)

Project: MWH No: 00303-014

Location: FMC RDRA Data Gap Investigation

Date: 12/2/2013

By: JDF

Boring No.: SB-7

Sample:

Depth: 6-8'

Sample Description: light brown silt

Sample Type: Undisturbed

	Initial (o)	Final (f)		
Sample Height, H (in)	2.770	2.767		
Sample Diameter, D (in)	2.884	2.88		
Sample Length, L (cm)	7.036	7.027		
Sample Area, A (cm^2)	42.145	41.907		
Sample Volume, V (cm ³)	296.52	294.49		
Wt. Rings + Wet Soil (g)	628.36	571.21		
Wt. Rings (g)	152.04	0		
Wet Unit Wt., γ _m (pcf)	100.3	121.1		
Wet Soil + Tare (g)	296.8	689.62		
Dry Soil + Tare (g)	287.4	568.94		
Tare (g)	128.47	122.22		
Weight of solids, Ws (g)	449.72	449.72		
Water Content, w (%)	5.91	27.01		
Dry Unit Wt, γ _d (pcf)	94.7	95.3		
Void ratio, e, for assumed Gs	0.75	0.72		
Saturation (%), for assumed Gs	21.0	100 ^a		
Average K ^b (cm/sec) 6.2E-05				
^a Saturation set to 100% for phase	e calculatio	ons		
^b K corrected to 20°C				

Gs	2.65	Assumed
Cell No.	1	
Station No.	1	
Permeant liquid used	De-aired to	ap water
Total backpressure (psi)	49.5	
Effective horiz. consolidation stress (psi)	5	
Effective vert. consolidation stress (psi)	5	
	Initial (o)	Final (f)

. ,	` '
0.54	0.96
9.90	20.10
0.0	54.5
49.5	•
49.5	
0.150	
8.16	
-2.04	
82.00	
82.1	
0.197	
5.076	
	9.90 0.0 49.5 49.5 0.150 8.16 -2.04 82.00 82.1 0.197

Start Date and	1 Time: 11/27/13	12:26			8		,	
Elapsed	Bottom Burette	Top Burette	h ₁	h_2	K	Temp	Visc. Ratio	K^{b}
time (sec)	(cm ³)	(cm ³)	(cm)	(cm)	(cm/sec)	(°C)	R_{f}	(cm/sec
180.0	0.00 2.56	10.00 7.42	50.66	24.57	6.6E-05	23.6	0.92	6.1E-05
180.0	0.00 2.58	10.00 7.42	50.66	24.47	6.7E-05	23.6	0.92	6.1E-05
180.0	0.00 2.64	10.00 7.35	50.66	23.81	6.9E-05	23.6	0.92	6.4E-05
180.0	0.00 2.64	10.00 7.35	50.66	23.81	6.9E-05	23.6	0.92	6.4E-05

Entered by:______
Reviewed:_____



Wall Permeameter, Method C (ASTM D5084)

Project: MWH
No: 00303-014

Boring No.: SB7
Sample:

Location: FMC RDRA Data Gap Investigation Depth: 12-14'

Date: 12/16/2013 Sample Description: Light brown silt By: JDF Sample Type: Undisturbed

	Initial (o)	Final (f)
Sample Height, H (in)	4.443	4.429
Sample Diameter, D (in)	2.798	2.76
Sample Length, L (cm)	11.285	11.249
Sample Area, A (cm^2)	39.669	38.653
Sample Volume, V (cm ³)	447.67	434.79
Wt. Rings + Wet Soil (g)	800.26	811.17
Wt. Rings (g)	168.6	0
Wet Unit Wt., γ _m (pcf)	88.1	116.5
Wet Soil + Tare (g)	405.17	1098.2
Dry Soil + Tare (g)	389.85	890.05
Tare (g)	128.62	311.06
Weight of solids, Ws (g)	596.67	596.67
Water Content, w (%)	5.86	35.95
Dry Unit Wt, γ _d (pcf)	83.2	85.7
Void ratio, e, for assumed Gs	0.99	0.95
Saturation (%), for assumed Gs	15.7	100 ^a
Average K ^b (cm/sec)	3.1E	E-04
^a Saturation set to 100% for phase	e calculatio	ons
^b K corrected to 20°C		

Gs	2.65	Assumed
Cell No.	H1	
Station No.	1	
Permeant liquid used	De-aired t	ap water
Total backpressure (psi)	35	
Effective horiz. consolidation stress (psi)	5	
Effective vert. consolidation stress (psi)	5	
	Initial (o)	Final (f)
B value	Initial (o) 0.56	Final (f) 0.98
B value External Burette (cm ³)	` ′	
	0.56 8.80	0.98
External Burette (cm ³)	0.56 8.80	0.98 29.90
External Burette (cm ³) Cell Pressure (psi)	0.56 8.80 0.0	0.98 29.90
External Burette (cm³) Cell Pressure (psi) Backpressure bottom (psi)	0.56 8.80 0.0 35.0	0.98 29.90

-12.88

82.00

82.1

Burette area, a (cm²) 0.197 Conversion, reading to cm head (cm/rd) 5.076

Net sample volume change (cm³)

Top burette ground length, l_t (cm)

Bottom burette ground length, l_b (cm)

Elapsed	Bottom Burette	Top Burette	h_1	h_2	K	Temp	Visc. Ratio	K^{b}
time (sec)	(cm ³)	(cm ³)	(cm)	(cm)	(cm/sec)	(°C)	R_{f}	(cm/sec)
180.0	0.00	10.00	50.66	6.60	3.2E-04	21.8	0.96	3.1E-04
100.0	4.32	5.64	20.00	0.00	3.22 0 .	21.0	0.50	3.1E 0 1
180.0	0.00	10.00	50.66	6.70	3.2E-04	21.7	0.96	3.1E-04
100.0	4.32	5.66	20.00	0.70	3.22 0 .	21.7	0.50	3.1 L 0 1
180.0	0.00	10.00	50.66	6.60	3.2E-04	22.6	0.94	3.0E-04
100.0	4.34	5.66	20.00	0.00	3.22 0 .	22.0	0.5.	5.02 01
180.0	0.00	10.00	50.66	6.40	3.3E-04	23.1	0.93	3.1E-04
100.0	4.36	5.64	50.00	0.40	3.32 04	23.1	0.73	J.1L 04

Entered by:_	
Paviawad.	

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Wall Permeameter, Method C (ASTM D5084)

Project: MWH No: 00303-014

Location: FMC RDRA Data Gap Investigation

Date: 12/17/2013 By: NB/JDF Sample Description: Light brown silt with gravel and sand

Sample Type: Remolded
Compaction Specifications: 105.4 pcf

Boring No.: **SB3**

Sample:

Depth:

at 0 (%) w

Gs

2.65

Assumed

	Initial (o)	Final (f)
Sample Height, H (in)	2.471	2.436
Sample Diameter, D (in)	2.387	2.32
Sample Length, L (cm)	6.276	6.188
Sample Area, A (cm^2)	28.871	27.253
Sample Volume, V (cm ³)	181.20	168.65
Wt. Rings + Wet Soil (g)	305.97	362.76
Wt. Rings (g)	0	0
Wet Unit Wt., γ _m (pcf)	105.4	134.3
Wet Soil + Tare (g)	1	489.34
Dry Soil + Tare (g)	1	432.79
Tare (g)	0	128.09
Weight of solids, Ws (g)	305.97	305.97
Water Content, w (%)	0.00	18.56
Dry Unit Wt, γ _d (pcf)	105.4	113.3
Void ratio, e, for assumed Gs	0.57	0.49
Saturation (%), for assumed Gs	0.0	100 ^a
Average K ^b (cm/sec)	2.6H	E-06
^a Saturation set to 100% for phase	e calculatio	ons
^b K corrected to 20°C		

05	2.00	1 100 011110 0
Cell No.	3	
Station No.	3	
Permeant liquid used	De-aired to	ap water
Total backpressure (psi)	30	
Effective horiz. consolidation stress (psi)	11.3	
Effective vert. consolidation stress (psi)	11.3	
	Initial (o)	Final (f)
B value	0.98	1.00
External Burette (cm ³)	14.50	33.30
Cell Pressure (psi)	0.0	41.3
Backpressure bottom (psi)	30.0	
Backpressure top (psi)	30.0	
System volume coefficient (cm³/psi)	0.151	
System volume change (cm ³)	6.25	
Net sample volume change (cm ³)	-12.55	
Bottom burette ground length, l _b (cm)	82.10	
Top burette ground length, l_t (cm)	81.9	
Burette area, a (cm ²)	0.197	
Conversion, reading to cm head (cm/rd)	5.076	

Elapsed	Bottom Burette	Top Burette	\mathbf{h}_1	h_2	K	Temp	Visc. Ratio	K^{b}	
time (sec)	(cm ³)	(cm^3)	(cm)	(cm)	(cm/sec)	(°C)	$R_{ m f}$	(cm/sec)	
1620.0	0.00	10.00	50.96	41.22	2.9E-06	22.8	0.93	2.7E-06	
1020.0	0.94	9.02	30.90	41.22	2.9E-00	22.8	0.93	2.7E-00	
5160.0	0.94	9.02	41.22	21.93	2.7E-06	21.9	0.95	2.6E-06	
3100.0	2.84	7.12	41.22	21.93	2.7E-00	21.9	0.93	2.0E-00	
3600.0	2.84	7.12	21.93	14.11	2.7E-06	22.3	0.95	2.6E-06	
3000.0	3.62	6.36	21.73	17,11	2.72 00	22.3	0.55	2.0L 00	
4560.0	3.62	6.36	14.11	8.22	2.6E-06	22.4	0.94	2.5E-06	
4500.0	4.20	5.78	17,11	0.22	2.01 00	22,4	0.74	2.3L 00	
1680.0	4.20	5.78	8.22	6.80	2.5E-06	22.5	0.94	2.4E-06	
1000.0	4.34	5.64	0.22	0.00	2.31 00	22.3	0.51	2.71 00	
960.0	0.00	10.00	50.96	45.58	2.6E-06	22.5	0.94	2.4E-06	
700.0	0.48	9.42	30.70	45.56	30 2.0E 00	22.3	0.54		
5940.0	0.48	9.42	45.58	21.82	2.8E-06	22.7	0.94	2.6E-06	
37 10.0	2.86	7.12	13.30	21.02	2.02 00	22.1	0.74	2.0L 00	

Entered by:_	
Daviarradı	



Using Pressure Extractor

(In general accordance with ASTM D6836)

Project: MWH Boring No.: WUA-TP001-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 1/15/2014

By: NB/MP

Description: Brown silty clay

Sample type: Laboratory compacted

Dry unit weight 90.9 pcf

Specific gravity, Gs: 2.650 Assumed at 8.5 (%) w

Compaction specifications: 85% of

ASTM D698B

								ASTM Dos		
		Test No.	1	2	3	4	5	6	7*	8*
		Tension (psi)	0.5	1.0	2.0	6.0	18.0	72.0	1235.72	11655.23
		Sample height, H (in)	0.5035	0.5035	0.5035	0.5035	0.5035	0.5035	0.1897	0.1872
		Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416	1.4720	1.4720
		Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001	0.0002	0.0002
		Wt. rings/cup + wet soil (g)	102.97	102.97	102.97	102.97	102.97	102.97	32.838	32.448
	ion	Wt. rings/cup (g)	43.33	43.33	43.33	43.33	43.33	43.33	24.598	24.578
	ıdit	Moist soil, Ws (g)	59.64	59.64	59.64	59.64	59.64	59.64	8.240	7.870
	Initial Condition	Dry soil (g)	55.07	55.07	55.07	55.07	55.07	55.07	7.683	7.587
	ial	Moist unit wt., γ _m (pcf)	98.43	98.43	98.43	98.43	98.43	98.43	97.24	94.11
A A	Init	Wet soil + tare (g)	251.73	251.73	251.73	251.73	251.73	251.73	32.838	32.448
Sample A		Dry soil + tare (g)	242.16	242.16	242.16	242.16	242.16	242.16	32.281	32.165
Sar		Tare (g)	126.81	126.81	126.81	126.81	126.81	126.81	24.598	24.578
		Moisture Content, w (%)	8.3	8.3	8.3	8.3	8.3	8.3	7.25	3.73
		Dry Unit Wt., γ _d (pcf)	90.89	90.89	90.89	90.89	90.89	90.89	90.66	90.73
	u	Wet soil + ring/cup (g)	116.74	115.88	114.20	109.96	107.35	105.41	32.831	32.445
	itio	Dry soil + ring/cup (g)	98.40	98.40	98.40	98.40	98.40	98.40	32.281	32.165
	puc	Ring/cup (g)	43.33	43.33	43.33	43.33	43.33	43.33	24.598	24.578
	Final Condition	Dry soil (g)	55.07	55.07	55.07	55.07	55.07	55.07	7.683	7.587
	ina	Moisture Content, w (%)	33.30	31.74	28.69	20.99	16.25	12.73	7.16	3.69
	F	Volumetric Water Content, θ	0.485	0.462	0.418	0.306	0.237	0.185	0.104	0.054
		Sample height, H (in)	0.5035	0.5035	0.5035	0.5035	0.5035	0.5035		
		Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416		
		Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001		
	ion	Wt. rings/cup + wet soil (g)	102.40	102.40	102.40	102.40	102.40	102.40		
	Initial Condition	Wt. rings/cup (g)	42.60	42.60	42.60	42.60	42.60	42.60		
	CO	Moist unit wt., γ_m (pcf)	98.70	98.70	98.70	98.70	98.70	98.70		
	tial	Wet soil + tare (g)	251.73	251.73	251.73	251.73	251.73	251.73		
e B	Ini	Dry soil + tare (g)	242.16	242.16	242.16	242.16	242.16	242.16		
Sample B		Tare (g)	126.81	126.81	126.81	126.81	126.81	126.81		
Sa		Moisture Content, w (%)	8.3	8.3	8.3	8.3	8.3	8.3		
		Dry Unit Wt., γ _d (pcf)	91.13	91.13	91.13	91.13	91.13	91.13		
	u	Wet soil + ring/cup (g)	116.01	114.81	113.80	109.78	107.12	105.19		
	litio	Dry soil + ring/cup (g)	97.82	97.82	97.82	97.82	97.82	97.82		
	Final Condition	Ring/cup (g)	42.60	42.60	42.60	42.60	42.60	42.60		
	ıl C	Dry soil (g)	55.22	55.22	55.22	55.22	55.22	55.22		
	Fina	Moisture Content, w (%)	32.94	30.77	28.94	21.66	16.84	13.35		
		Volumetric Water Content, θ	0.481	0.449	0.423	0.316	0.246	0.195		
		Average Volumetric Moisture:	0.483	0.456	0.420	0.311	0.241	0.190	0.104	0.054

Comments:

Entered by:_	
Reviewed:	

^{*}Points 7 and 8 were performed on a Chilled Mirror Hygrometer



Using Pressure Extractor

(In general accordance with ASTM D6836)

Project: MWH

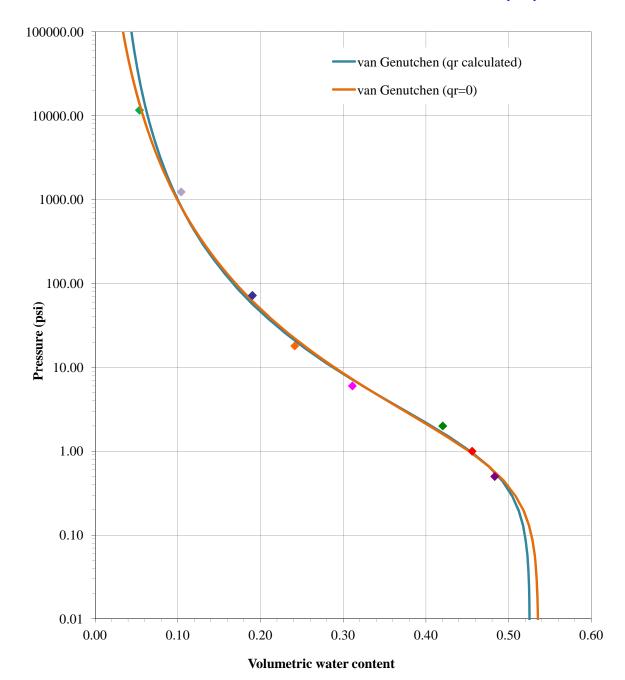
No: 00303-014
Location: FMC RDRA Data Gap Investigation

Date: 1/15/2014

Boring No.: WUA-TP001-01

Sample:
Depth: 1-10'

Description: Brown silty clay



van Genuchten fitting parameters (using SWRC fit, Seki, K. (2007)):

van Genae	enten mung pu	rumeters (using b	WICE III, DEK
θ_r calculat	ed	Setting θ_r	=0
$\theta_{\rm s}$	0.5257	$\Theta_{ m s}$	0.5358
$\theta_{\rm r}$	0.0207	$\Theta_{ m r}$	0
α	1.0624	α	1.3558
n	1.2659	n	1.2337
m	0.2100	m	0.1894
R^2	0.9963	\mathbb{R}^2	0.9960



Using Pressure Extractor

(In general accordance with ASTM D6836)

Project: **MWH** Boring No.: WUA-TP004-01

No: 00303-014 Sample: Location: FMC RDRA Data Gap Investigation **Depth: 1-10'**

Description: Brown silt Date: 1/15/2014 By: NB/MP Sample type: Laboratory compacted

Dry unit weight pcf Specific gravity, Gs: 2.650 Assumed (%) w

Compaction specifications: 85% of

90.4

ASTM D698B

								ASTM Dos		
		Test No.	1	2	3	4	5	6	7*	8*
		Tension (psi)	0.5	1.0	2.0	6.0	18.0	72.0	929.69	11344.85
		Sample height, H (in)	0.5035	0.5035	0.5035	0.5035	0.5035	0.5035	0.1897	0.1883
		Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416	1.4717	1.4718
		Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001	0.0002	0.0002
		Wt. rings/cup + wet soil (g)	102.56	102.56	102.56	102.56	102.56	102.56	32.694	32.139
	ion	Wt. rings/cup (g)	42.68	42.68	42.68	42.68	42.68	42.68	24.766	24.371
	ndit	Moist soil, Ws (g)	59.88	59.88	59.88	59.88	59.88	59.88	7.928	7.768
	Initial Condition	Dry soil (g)	54.84	54.84	54.84	54.84	54.84	54.84	7.594	7.602
	tial	Moist unit wt., γ_m (pcf)	98.83	98.83	98.83	98.83	98.83	98.83	93.60	92.37
Sample A	Ini	Wet soil + tare (g)	328.04	328.04	328.04	328.04	328.04	328.04	32.694	32.139
ldu		Dry soil + tare (g)	312.20	312.20	312.20	312.20	312.20	312.20	32.360	31.973
Sar		Tare (g)	139.72	139.72	139.72	139.72	139.72	139.72	24.766	24.371
		Moisture Content, w (%)	9.2	9.2	9.2	9.2	9.2	9.2	4.40	2.18
		Dry Unit Wt., γ _d (pcf)	90.51	90.51	90.51	90.51	90.51	90.51	89.65	90.40
	u	Wet soil + ring/cup (g)	114.28	113.48	112.54	110.27	103.80	101.73	32.683	32.137
	itio	Dry soil + ring/cup (g)	97.52	97.52	97.52	97.52	97.52	97.52	32.360	31.973
	puo	Ring/cup (g)	42.68	42.68	42.68	42.68	42.68	42.68	24.766	24.371
	I C	Dry soil (g)	54.84	54.84	54.84	54.84	54.84	54.84	7.594	7.602
	Final Condition	Moisture Content, w (%)	30.55	29.09	27.38	23.24	11.44	7.67	4.25	2.16
		Volumetric Water Content, θ	0.443	0.422	0.397	0.337	0.166	0.111	0.061	0.031
		Sample height, H (in)	0.5035	0.5035	0.5035	0.5035	0.5035	0.5035		
		Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416		
		Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001		
	ion	Wt. rings/cup + wet soil (g)	102.75	102.75	102.75	102.75	102.75	102.75		
	Initial Condition	Wt. rings/cup (g)	42.84	42.84	42.84	42.84	42.84	42.84		
	ပ္ပ	Moist unit wt., γ_m (pcf)	98.88	98.88	98.88	98.88	98.88	98.88		
	tial	Wet soil + tare (g)	328.04	328.04	328.04	328.04	328.04	328.04		
Sample B	Ini	Dry soil + tare (g)	312.20	312.20	312.20	312.20	312.20	312.20		
ldm		Tare (g)	139.72	139.72	139.72	139.72	139.72	139.72		
Sa		Moisture Content, w (%)	9.2	9.2	9.2	9.2	9.2	9.2		
		Dry Unit Wt., γ _d (pcf)	90.56	90.56	90.56	90.56	90.56	90.56		
	ű	Wet soil + ring/cup (g)	114.69	113.81	112.65	109.02	103.31	101.57		
	litio	Dry soil + ring/cup (g)	97.71	97.71	97.71	97.71	97.71	97.71		
	Final Condition	Ring/cup (g)	42.84	42.84	42.84	42.84	42.84	42.84		
	ıl C	Dry soil (g)	54.87	54.87	54.87	54.87	54.87	54.87		
	Fins	Moisture Content, w (%)	30.94	29.34	27.23	20.61	10.20	7.03		
		Volumetric Water Content, θ	0.449	0.426	0.395	0.299	0.148	0.102		
		Average Volumetric Moisture:	0.446	0.424	0.396	0.318	0.157	0.107	0.061	0.031

Comments:

Entered by:	
Reviewed:	

^{*}Points 7 and 8 were performed on a Chilled Mirror Hygrometer



Using Pressure Extractor

(In general accordance with ASTM D6836)

Project: MWH

No: 00303-014

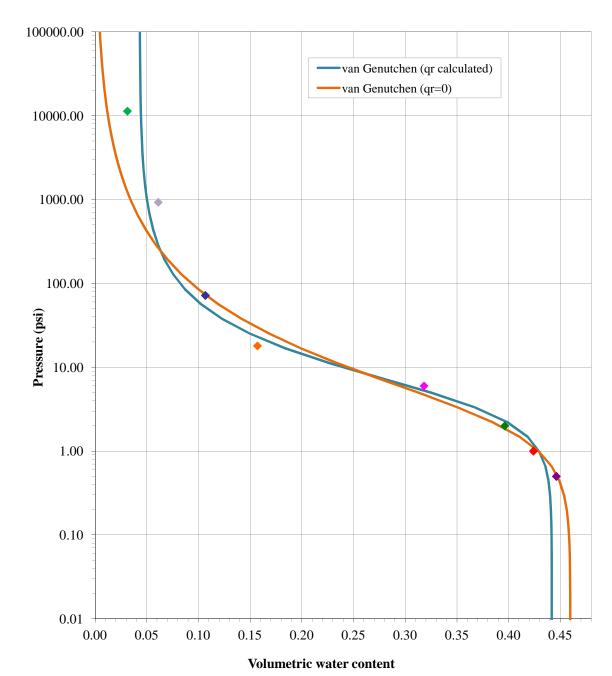
Date: 1/15/2014

Location: FMC RDRA Data Gap Investigation

Sample:
Depth: 1-10'

Boring No.: WUA-TP004-01

Description: Brown silt



van Genuchten fitting parameters (using SWRC fit, Seki, K. (2007)):

$\theta_{\rm r}$ calcul	ated		
$\theta_{\rm s}$	0.4417	θ_{s}	0.4597
$\theta_{\rm r}$	0.0431	Θ_{r}	0
α	0.2293	α	0.3874
n	1.7409	n	1.4358
m	0.4256	m	0.3035
\mathbb{R}^2	0.9963	\mathbb{R}^2	0.9872



Using Pressure Extractor

(In general accordance with ASTM D6836)

Project: MWH Boring No.: WUA-TP006-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 1/15/2014

By: NB/MP

Description: Brown silty clay

Sample type: Laboratory compacted

Dry unit weight 88.7 pcf

Specific gravity, Gs: 2.650 Assumed at 8.5 (%) w

Compaction specifications: 85% of

ASTM D698B

								ASTM D69	OD	
		Test No.	1	2	3	4	5	6	7*	8*
		Tension (psi)	0.5	1.0	2.0	6.0	18.0	72.0	462.67	6381.66
		Sample height, H (in)	0.5035	0.5035	0.5035	0.5035	0.5035	0.5035	0.1883	0.1875
		Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416	1.4715	1.4725
		Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001	0.0002	0.0002
		Wt. rings/cup + wet soil (g)	101.62	101.62	101.62	101.62	101.62	101.62	32.585	32.480
	ion	Wt. rings/cup (g)	43.06	43.06	43.06	43.06	43.06	43.06	24.595	24.774
	ndit	Moist soil, Ws (g)	58.56	58.56	58.56	58.56	58.56	58.56	7.990	7.706
	Initial Condition	Dry soil (g)	53.83	53.83	53.83	53.83	53.83	53.83	7.446	7.429
	tial	Moist unit wt., γ_m (pcf)	96.65	96.65	96.65	96.65	96.65	96.65	95.05	91.94
e A	Ini	Wet soil + tare (g)	304.54	304.54	304.54	304.54	304.54	304.54	32.585	32.480
Sample A		Dry soil + tare (g)	289.91	289.91	289.91	289.91	289.91	289.91	32.041	32.203
Saı		Tare (g)	123.34	123.34	123.34	123.34	123.34	123.34	24.595	24.774
		Moisture Content, w (%)	8.8	8.8	8.8	8.8	8.8	8.8	7.31	3.73
		Dry Unit Wt., γ _d (pcf)	88.85	88.85	88.85	88.85	88.85	88.85	88.58	88.64
	Ē	Wet soil + ring/cup (g)	114.15	113.24	112.02	109.13	105.67	103.28	32.578	32.478
	Final Condition	Dry soil + ring/cup (g)	96.89	96.89	96.89	96.89	96.89	96.89	32.041	32.203
	puo	Ring/cup (g)	43.06	43.06	43.06	43.06	43.06	43.06	24.595	24.774
	ıl C	Dry soil (g)	53.83	53.83	53.83	53.83	53.83	53.83	7.446	7.429
	ing	Moisture Content, w (%)	32.06	30.37	28.10	22.73	16.31	11.87	7.21	3.70
		Volumetric Water Content, θ	0.456	0.432	0.400	0.324	0.232	0.169	0.102	0.053
		Sample height, H (in)	0.5035	0.5035	0.5035	0.5035	0.5035	0.5035		
		Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416		
	_	Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001		
	tion	Wt. rings/cup + wet soil (g)	101.04	101.04	101.04	101.04	101.04	101.04		
	ipu	Wt. rings/cup (g)	42.48	42.48	42.48	42.48	42.48	42.48		
	သိ	Moist unit wt., γ_m (pcf)	96.65	96.65	96.65	96.65	96.65	96.65		
	Initial Condition	Wet soil + tare (g)	304.54	304.54	304.54	304.54	304.54	304.54		
Sample B	In	Dry soil + tare (g)	289.91	289.91	289.91	289.91	289.91	289.91		
[dw		Tare (g)	123.34	123.34	123.34	123.34	123.34	123.34		
$\mathbf{S}\mathbf{a}$		Moisture Content, w (%)	8.8	8.8	8.8	8.8	8.8	8.8		
		Dry Unit Wt., γ _d (pcf)	88.85	88.85	88.85	88.85	88.85	88.85		
	'n	Wet soil + ring/cup (g)	113.86	112.86	111.67	108.66	104.88	102.81		
	litic	Dry soil + ring/cup (g)	96.31	96.31	96.31	96.31	96.31	96.31		
	Onc	Ring/cup (g)	42.48	42.48	42.48	42.48	42.48	42.48		
	Final Condition	Dry soil (g)	53.83	53.83	53.83	53.83	53.83	53.83		
	Fin	Moisture Content, w (%)	32.60	30.74	28.53	22.94	15.92	12.07		
		Volumetric Water Content, θ	0.464	0.438	0.406	0.327	0.227	0.172		
		Average Volumetric Moisture:	0.460	0.435	0.403	0.325	0.229	0.170	0.102	0.053

Comments:

Entered by:_	
Reviewed:	

^{*}Points 7 and 8 were performed on a Chilled Mirror Hygrometer



Using Pressure Extractor

(In general accordance with ASTM D6836)

Project: MWH

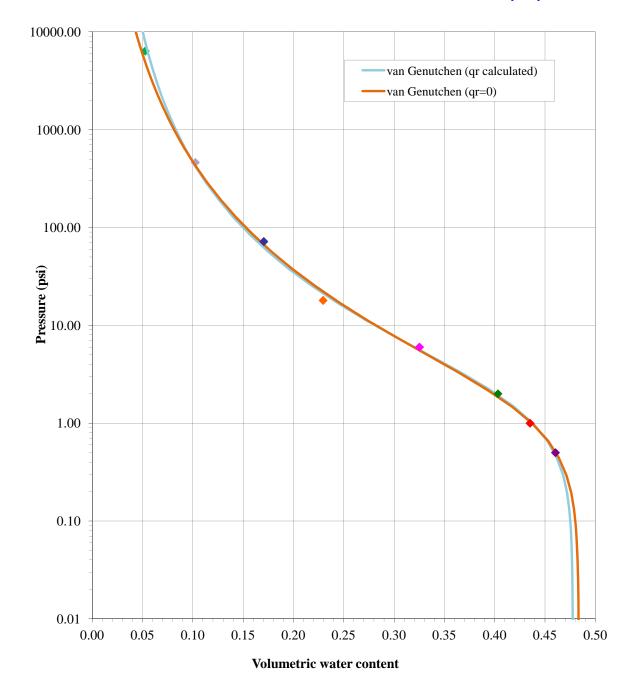
No: 00303-014
Location: FMC RDRA Data Gap Investigation

Date: 1/15/2014

Boring No.: WUA-TP006-01

Sample: Depth: 1-10'

Description: Brown silty clay



van Genuchten fitting parameters (using SWRC fit, Seki, K. (2007)):

$\theta_{\rm r}$ calcu	lated		
$\theta_{\rm s}$	0.4776	θ_{s}	0.4834
$\theta_{\rm r}$	0.0191	θ_{r}	0
α	0.5592	α	0.6705
n	1.3116	n	1.2739
m	0.2376	m	0.2150
\mathbb{R}^2	0.9988	\mathbb{R}^2	0.9985



Using Pressure Extractor

(In general accordance with ASTM D6836)

Project: MWH Boring No.: WUA-TP007-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 1/15/2014 Description: Brown silt
By: NB/MP Sample type: Laboratory compacted

Specific gravity, Gs: 2.650 Assumed at 8.5 (%) w

Compaction specifications: 85% of

ASTM D698B

pcf

88.6

Dry unit weight

$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$									ASTM DO		
Sample height, H (in)				1	2		4	_	_	_	8*
Sample diameter, D (in) 2.416 2.416 2.416 2.416 2.416 1.4717 1.4710			Tension (psi)	0.5	1.0	2.0	6.0	18.0	72.0	433.66	6612.27
Sample Volume (ft³) 0.001 0.001 0.001 0.001 0.001 0.001 0.0002 0.0002			Sample height, H (in)	0.5035	0.5035	0.5035	0.5035	0.5035	0.5035	0.1865	0.1863
Second Part			Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416	1.4717	1.4710
Fig. Wt. rings/cup (g) 42.58 42.58 42.58 42.58 42.58 42.58 42.58 24.556 24.586			Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001	0.0002	0.0002
Dry soil + tare (g) 291.11 291.11 291.11 291.11 291.11 291.11 291.11 31.924 31.929			Wt. rings/cup + wet soil (g)	100.70	100.70	100.70	100.70	100.70	100.70	32.462	32.209
Dry soil + tare (g) 291.11 291.11 291.11 291.11 291.11 291.11 291.11 31.924 31.929		ion	Wt. rings/cup (g)	42.58	42.58	42.58	42.58	42.58	42.58	24.556	24.586
Dry soil + tare (g) 291.11 291.11 291.11 291.11 291.11 291.11 291.11 31.924 31.929		ndit	Moist soil, Ws (g)	58.12	58.12	58.12	58.12	58.12	58.12	7.906	7.623
Dry soil + tare (g) 291.11 291.11 291.11 291.11 291.11 291.11 291.11 31.924 31.929		Coı	Dry soil (g)	53.71	53.71	53.71	53.71	53.71	53.71	7.368	7.343
Dry soil + tare (g) 291.11 291.11 291.11 291.11 291.11 291.11 291.11 31.924 31.929		ial	Moist unit wt., γ _m (pcf)	95.92	95.92	95.92	95.92	95.92	95.92	94.94	91.72
Moisture Content, w (%) 8.2 8.2 8.2 8.2 8.2 8.2 7.30 3.81	A A	Init	Wet soil + tare (g)	304.93	304.93	304.93	304.93	304.93	304.93	32.462	32.209
Moisture Content, w (%) 8.2 8.2 8.2 8.2 8.2 8.2 7.30 3.81	ople		Dry soil + tare (g)	291.11	291.11	291.11	291.11	291.11	291.11	31.924	31.929
Dry Unit Wt., γ _d (pcf) 88.64 88.65 32.206 32.2	San			123.00	123.00	123.00	123.00	123.00	123.00	24.556	24.586
Wet soil + ring/cup (g) 113.27 111.89 110.72 106.51 103.65 102.04 32.452 32.206			Moisture Content, w (%)	8.2	8.2	8.2	8.2	8.2	8.2	7.30	3.81
Wet soil + ring/cup (g) 113.27 111.89 110.72 106.51 103.65 102.04 32.452 32.206			Dry Unit Wt., γ _d (pcf)	88.64	88.64	88.64	88.64	88.64	88.64	88.48	88.35
Volumetric Water Content, θ 0.449 0.413 0.382 0.270 0.195 0.152 0.102 0.053		J		113.27	111.89	110.72	106.51	103.65	102.04	32.452	32.206
Volumetric Water Content, θ 0.449 0.413 0.382 0.270 0.195 0.152 0.102 0.053		tioi	Dry soil + ring/cup (g)	96.29	96.29	96.29	96.29	96.29	96.29	31.924	31.929
Volumetric Water Content, θ 0.449 0.413 0.382 0.270 0.195 0.152 0.102 0.053		ibuo	Ring/cup (g)	42.58	42.58	42.58	42.58	42.58	42.58	24.556	24.586
Volumetric Water Content, θ 0.449 0.413 0.382 0.270 0.195 0.152 0.102 0.053		ŭ	Dry soil (g)	53.71	53.71	53.71	53.71	53.71	53.71	7.368	7.343
Volumetric Water Content, θ 0.449 0.413 0.382 0.270 0.195 0.152 0.102 0.053		ina	Moisture Content, w (%)	31.63	29.06	26.88	19.04	13.71	10.72	7.17	3.77
Sample height, H (in) 0.5035 0.5035 0.5035 0.5035 0.5035 0.5035 Sample diameter, D (in) 2.416 2.416 2.416 2.416 2.416 2.416 Sample Volume (ft³) 0.001 0.001 0.001 0.001 0.001 0.001 Wt. rings/cup + wet soil (g) 101.26 101.26 101.26 101.26 101.26 101.26 Wt. rings/cup (g) 43.11 43.11 43.11 43.11 43.11 43.11 43.11 Moist unit wt., γ _m (pcf) 95.97 95.97 95.97 95.97 95.97 Wet soil + tare (g) 304.93 304.93 304.93 304.93 304.93 304.93 Dry soil + tare (g) 291.11 291.11 291.11 291.11 291.11 291.11 Tare (g) 123.00 123.00 123.00 123.00 123.00 123.00 Moisture Content, w (%) 8.2 8.2 8.2 8.2 8.2 Dry Unit Wt., γ _d (pcf) 88.68 88.68 88.68 88.68 88.68 Wet soil + ring/cup (g) 96.84 96.84 96.84 96.84 96.84 Dry soil + ring/cup (g) 43.11 43.11 43.11 43.11 43.11 43.11 Dry soil (g) 53.73 53.73 53.73 53.73 53.73 53.73 Moisture Content, w (%) 31.89 30.48 27.58 19.03 14.05 11.53 Volumetric Water Content, θ 0.453 0.433 0.392 0.271 0.200 0.164		Щ	Volumetric Water Content, θ	0.449	0.413	0.382	0.270	0.195	0.152	0.102	0.053
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				0.5035	0.5035		0.5035	0.5035	0.5035		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$			Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416		
$ \begin{array}{ c c c c c } \hline \text{Bo} \\ \hline \text{Fig} \\ \hline F$			Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		lon		101.26	101.26	101.26	101.26	101.26	101.26		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		nditi	Wt. rings/cup (g)	43.11	43.11	43.11	43.11		43.11		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		Cor	Moist unit wt., γ_m (pcf)	95.97	95.97	95.97	95.97	95.97	95.97		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$		ial		304.93	304.93	304.93	304.93	304.93	304.93		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	B	Init	Dry soil + tare (g)	291.11	291.11	291.11	291.11	291.11	291.11		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	ople		Tare (g)	123.00	123.00	123.00	123.00	123.00	123.00		
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	Sar		Moisture Content, w (%)	8.2	8.2	8.2	8.2	8.2	8.2		
Wet soil + ring/cup (g) 113.98 113.22 111.66 107.07 104.39 103.04			Dry Unit Wt., γ _d (pcf)	88.68	88.68	88.68	88.68	88.68	88.68		
Volumetric Water Content, θ 0.453 0.433 0.392 0.271 0.200 0.164		u		113.98	113.22	111.66	107.07	104.39	103.04		
Volumetric Water Content, θ 0.453 0.433 0.392 0.271 0.200 0.164		itio	Dry soil + ring/cup (g)	96.84	96.84	96.84	96.84	96.84	96.84		
Volumetric Water Content, θ 0.453 0.433 0.392 0.271 0.200 0.164		ondi	Ring/cup (g)	43.11	43.11	43.11	43.11	43.11	43.11		
Volumetric Water Content, θ 0.453 0.433 0.392 0.271 0.200 0.164		ľČ	Dry soil (g)	53.73	53.73	53.73	53.73	53.73	53.73		
Volumetric Water Content, θ 0.453 0.433 0.392 0.271 0.200 0.164		ina	Moisture Content, w (%)	31.89	30.48	27.58	19.03	14.05	11.53		
Average Volumetric Moisture: 0.451 0.423 0.387 0.270 0.197 0.158 0.102 0.053		Ļ	Volumetric Water Content, θ					0.200			
			Average Volumetric Moisture:	0.451	0.423	0.387	0.270	0.197	0.158	0.102	0.053

Comments:

Entered by:_	
Reviewed:	

^{*}Points 7 and 8 were performed on a Chilled Mirror Hygrometer



Using Pressure Extractor

(In general accordance with ASTM D6836)

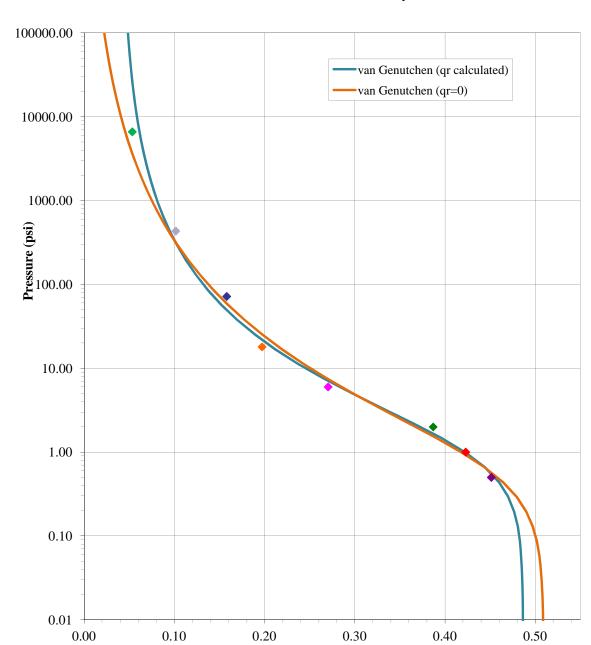
Project: MWH

No: 00303-014
Location: FMC RDRA Data Gap Investigation

Date: 1/15/2014

Boring No.: WUA-TP007-01

Sample:
Depth: 1-10'
Description: Brown silt



van Genuchten fitting parameters (using SWRC fit, Seki, K. (2007)):

$\theta_{\rm r}$ calcul	ated		
$\theta_{\rm s}$	0.4865	θ_{s}	0.5091
$\theta_{\rm r}$	0.0409	$\Theta_{ m r}$	0
α	0.8571	α	1.4349
n	1.3562	n	1.2632
m	0.2626	m	0.2084
\mathbb{R}^2	0.9947	\mathbb{R}^2	0.9926

Volumetric water content



Using Pressure Extractor

(In general accordance with ASTM D6836)

Project: MWH Boring No.: WUA-TP008-01

No: 00303-014 Sample:
Location: FMC RDRA Data Gap Investigation Depth: 1-10'

Date: 1/15/2014 Description: Brown silt

By: NB/MP Sample type: Laboratory compacted
Dry unit weight 84.7 pcf

Specific gravity, Gs: 2.650 Assumed at 8.5 (%) w

Compaction specifications: 85% of

ASTM D698B

								ASTM Dos		
		Test No.	1	2	3	4	5	6	7*	8*
		Tension (psi)	0.5	1.0	2.0	6.0	18.0	72.0	577.25	12281.80
		Sample height, H (in)	0.5035	0.5035	0.5035	0.5035	0.5035	0.5035	0.1900	0.1892
		Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416	1.4713	1.4718
		Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001	0.0002	0.0002
		Wt. rings/cup + wet soil (g)	100.65	100.65	100.65	100.65	100.65	100.65	32.165	31.985
	ion	Wt. rings/cup (g)	44.89	44.89	44.89	44.89	44.89	44.89	24.447	24.557
	Initial Condition	Moist soil, Ws (g)	55.76	55.76	55.76	55.76	55.76	55.76	7.718	7.428
	Coı	Dry soil (g)	51.35	51.35	51.35	51.35	51.35	51.35	7.147	7.152
	ial	Moist unit wt., γ _m (pcf)	92.03	92.03	92.03	92.03	92.03	92.03	91.02	87.91
e A	Ini	Wet soil + tare (g)	379.66	379.66	379.66	379.66	379.66	379.66	32.165	31.985
Sample A		Dry soil + tare (g)	360.76	360.76	360.76	360.76	360.76	360.76	31.594	31.709
Sar		Tare (g)	140.47	140.47	140.47	140.47	140.47	140.47	24.447	24.557
		Moisture Content, w (%)	8.6	8.6	8.6	8.6	8.6	8.6	7.99	3.86
		Dry Unit Wt., γ _d (pcf)	84.76	84.76	84.76	84.76	84.76	84.76	84.28	84.64
	u	Wet soil + ring/cup (g)	114.84	114.05	112.48	107.60	103.87	102.26	32.152	31.979
	Final Condition	Dry soil + ring/cup (g)	96.24	96.24	96.24	96.24	96.24	96.24	31.594	31.709
	puc	Ring/cup (g)	44.89	44.89	44.89	44.89	44.89	44.89	24.447	24.557
	1 C	Dry soil (g)	51.35	51.35	51.35	51.35	51.35	51.35	7.147	7.152
	ina	Moisture Content, w (%)	36.21	34.67	31.62	22.11	14.85	11.71	7.81	3.78
	I	Volumetric Water Content, θ	0.492	0.471	0.429	0.300	0.202	0.159	0.105	0.051
		Sample height, H (in)	0.5035	0.5035	0.5035	0.5035	0.5035	0.5035		
		Sample diameter, D (in)	2.416	2.416	2.416	2.416	2.416	2.416		
		Sample Volume (ft ³)	0.001	0.001	0.001	0.001	0.001	0.001		
	ion	Wt. rings/cup + wet soil (g)	101.75	101.75	101.75	101.75	101.75	101.75		
	Initial Condition	Wt. rings/cup (g)	45.98	45.98	45.98	45.98	45.98	45.98		
	Co	Moist unit wt., γ_m (pcf)	92.04	92.04	92.04	92.04	92.04	92.04		
	tial	Wet soil + tare (g)	379.66	379.66	379.66	379.66	379.66	379.66		
Sample B	Ini	Dry soil + tare (g)	360.76	360.76	360.76	360.76	360.76	360.76		
ldm		Tare (g)	140.47	140.47	140.47	140.47	140.47	140.47		
Sa		Moisture Content, w (%)	8.6	8.6	8.6	8.6	8.6	8.6		
		Dry Unit Wt., γ _d (pcf)	84.77	84.77	84.77	84.77	84.77	84.77		
	п	Wet soil + ring/cup (g)	115.88	114.65	113.25	108.03	104.97	103.23		
	litio	Dry soil + ring/cup (g)	97.34	97.34	97.34	97.34	97.34	97.34		
	ond	Ring/cup (g)	45.98	45.98	45.98	45.98	45.98	45.98		
	Final Condition	Dry soil (g)	51.36	51.36	51.36	51.36	51.36	51.36		
	Fina	Moisture Content, w (%)	36.09	33.69	30.97	20.81	14.85	11.46		
		Volumetric Water Content, θ	0.490	0.458	0.421	0.283	0.202	0.156		
		Average Volumetric Moisture:	0.491	0.464	0.425	0.292	0.202	0.157	0.105	0.051

Comments:

Entered by:	
Reviewed:	

^{*}Points 7 and 8 were performed on a Chilled Mirror Hygrometer



Using Pressure Extractor

(In general accordance with ASTM D6836)

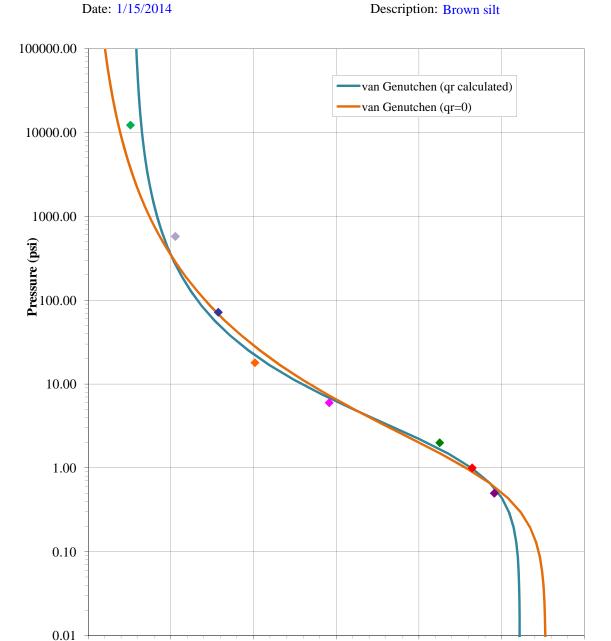
Project: MWH

No: 00303-014 Location: FMC RDRA Data Gap Investigation

Date: 1/15/2014

Boring No.: WUA-TP008-01

Sample: **Depth: 1-10'**



van Genuchten fitting parameters (using SWRC fit, Seki, K. (2007)):

0.10

0.00

0.20

0.30

Volumetric water content

0.40

$\theta_{\rm r}$ calcu	lated		
$\theta_{\rm s}$	0.5219	θ_{s}	0.5533
$\theta_{\rm r}$	0.0543	Θ_{r}	0
α	0.6665	α	1.2965
n	1.4267	n	1.2802
m	0.2991	m	0.2189
R^2	0.9946	\mathbb{R}^2	0.9898

0.50

0.60

APPENDIX E

Agronomic Testing Reports

Analytical Report

December 11, 2013

Report to: Bill to:

Chad Tomlinson Accounts Payable

MWH Americas Inc. MWH Americas Inc.

2890 E. Cottonwood Pkwy. P.O. Box 6610

Suite 300

Salt Lake City, UT 84121 Broomfield, CO 80021

Project ID: 10503311.020102 FML

ACZ Project ID: L15653

Chad Tomlinson:

Enclosed are the analytical results for sample(s) submitted to ACZ Laboratories, Inc. (ACZ) on November 20, 2013. This project has been assigned to ACZ's project number, L15653. Please reference this number in all future inquiries.

All analyses were performed according to ACZ's Quality Assurance Plan. The enclosed results relate only to the samples received under L15653. Each section of this report has been reviewed and approved by the appropriate Laboratory Supervisor, or a qualified substitute.

Except as noted, the test results for the methods and parameters listed on ACZ's current NELAC certificate letter (#ACZ) meet all requirements of NELAC.

This report shall be used or copied only in its entirety. ACZ is not responsible for the consequences arising from the use of a partial report.

All samples and sub-samples associated with this project will be disposed of after January 10, 2014. If the samples are determined to be hazardous, additional charges apply for disposal (typically \$11/sample). If you would like the samples to be held longer than ACZ's stated policy or to be returned, please contact your Project Manager or Customer Service Representative for further details and associated costs. ACZ retains analytical raw data reports for ten years.

If you have any questions or other needs, please contact your Project Manager.

Scott Habermehl has reviewed and approved this report.

S. Havermehl





Case Narrative

MWH Americas Inc. December 11, 2013

Project ID: 10503311.020102 FML

ACZ Project ID: L15653

Sample Receipt

ACZ Laboratories, Inc. (ACZ) received 3 soil samples from MWH Americas Inc. on November 20, 2013. The samples were received in good condition. Upon receipt, the sample custodian removed the samples from the cooler, inspected the contents, and logged the samples into ACZ's computerized Laboratory Information Management System (LIMS). The samples were assigned ACZ LIMS project number L15653. The custodian verified the sample information entered into the computer against the chain of custody (COC) forms and sample bottle labels.

Samples were received outside the EPA recommended temperature of 0-6 degrees C.

Holding Times

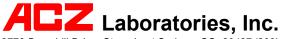
All analyses were performed within EPA recommended holding times.

Sample Analysis

These samples were analyzed for inorganic parameters. The individual methods are referenced on both, the ACZ invoice and the analytical reports. The extended qualifier reports may contain footnotes qualifying specific elements due to QC failures. In addition the following has been noted with this specific project:

1. (B1) Target analyte detected in prep blank at or above the method reporting limit. This is due to procedural contamination at the prep level. Client may opt to blank subtract at their discretion.

REPAD.03.06.05.01 Page 2 of 14



Inorganic Analytical Results

MWH Americas Inc.

Project ID:

10503311.020102 FML

Sample ID: WUA-CP01

ACZ Sample ID: L15653-01

Date Sampled: 11/05/13 10:00

Date Received: 11/20/13

Sample Matrix: Soil

Metals Analysis										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Cation Exchange Capacity (CEC)	USDA No. 60 (19)	1	8.50		*	meq/100g	0.03	0.2	12/05/13 11:36	aeb
Phosphorus, total (3050)	M6010B ICP	101	790		*	mg/Kg	10	50	12/02/13 21:44	aeb
Potassium, total (3050)) M6010B ICP	101	2410			mg/Kg	30	200	12/02/13 21:44	aeb
Soil Analysis										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Carbon, total organic (TOC)	ASA No.9 29-2.2.4 Combustion/IR	1	0.2	В	*	%	0.1	0.5	12/05/13 14:52	cra
Conductivity @25C	SM2510B									
Conductivity		1	0.442		*	mmhos/cm	0.001	0.01	11/27/13 0:00	spl
Max Particle Size		1	2000		*	um			11/27/13 0:00	spl
Organic Matter	USDA No.60 - Method 24	1	8.0	В	*	%	0.3	1	11/25/13 22:08	cra
pH, Saturated Paste	EPA 600/2-78-054, section 3.2.2									
Max Particle Size		1	2000		*	um			11/27/13 0:00	spl
рН		1	8.6		*	units	0.1	0.1	11/27/13 0:00	spl
Solids, Percent	CLPSOW390, PART F, D-98	1	94.1		*	%	0.1	0.5	11/22/13 13:54	spl
Soil Preparation										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Air Dry at 34 Degrees C	USDA No. 1, 1972				*				11/24/13 11:00	mss2
Cation Exchange Capacity Extraction	USDA No. 60 (19)				*				12/04/13 18:22	cdb
Digestion - Hot Plate	M3050B ICP								11/26/13 13:20	mss2
Potassium Chloride Extraction	ASA No. 9 33-3.2.2				*				12/04/13 15:00	spl
Saturated Paste Extraction	USDA No. 60 (2)				*				11/26/13 14:20	spl
Sieve-2000 um (2.0mm)	ASA No.9, 15-4.2.2				*				11/25/13 11:00	cra
Sieve-250 um (60 mesh)	ASA No.9, 15-4.2.2				*				11/25/13 11:00	cra
Wet Chemistry										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Nitrogen, ammonia (KCL)	M350.1 - Automated Phenate	10	10.6		*	mg/Kg	0.5	5	12/10/13 17:16	bsu

Arizona license number: AZ0102

Inorganic Analytical Results

MWH Americas Inc.

ACZ Sample ID: **L15653-02**

Project ID: 10503311.020102 FML

Date Sampled: 11/05/13 10:00

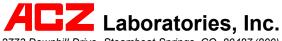
Sample ID: WUA-CP02

Date Received: 11/20/13

Sample Matrix: Soil

Metals Analysis										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Cation Exchange Capacity (CEC)	USDA No. 60 (19)	1	11.0		*	meq/100g	0.03	0.2	12/05/13 11:45	aeb
Phosphorus, total (3050)	M6010B ICP	102	780		*	mg/Kg	10	50	12/02/13 21:53	aeb
Potassium, total (3050)	M6010B ICP	102	2780			mg/Kg	30	200	12/02/13 21:53	aeb
Soil Analysis										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Carbon, total organic (TOC)	ASA No.9 29-2.2.4 Combustion/IR	1	0.2	В	*	%	0.1	0.5	12/06/13 2:37	cra
Conductivity @25C	SM2510B									
Conductivity		1	0.594		*	mmhos/cm	0.001	0.01	11/27/13 0:00	spl
Max Particle Size		1	2000		*	um			11/27/13 0:00	spl
Organic Matter	USDA No.60 - Method 24	1	0.9	В	*	%	0.3	1	11/26/13 4:17	cra
pH, Saturated Paste	EPA 600/2-78-054, section 3.2.2									
Max Particle Size		1	2000		*	um			11/27/13 0:00	spl
pН		1	8.4		*	units	0.1	0.1	11/27/13 0:00	spl
Solids, Percent	CLPSOW390, PART F, D-98	1	91.9		*	%	0.1	0.5	11/22/13 14:57	spl
Soil Preparation										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Air Dry at 34 Degrees C	USDA No. 1, 1972				*				11/24/13 11:30	mss2
Cation Exchange Capacity Extraction	USDA No. 60 (19)				*				12/04/13 23:15	cdb
Digestion - Hot Plate	M3050B ICP								11/26/13 15:20	mss2
Potassium Chloride Extraction	ASA No. 9 33-3.2.2				*				12/04/13 17:00	spl
Saturated Paste Extraction	USDA No. 60 (2)				*				11/27/13 4:16	spl
Sieve-2000 um (2.0mm)	ASA No.9, 15-4.2.2				*				11/25/13 11:30	cra
Sieve-250 um (60 mesh)	ASA No.9, 15-4.2.2				*				11/25/13 11:30	cra
Wet Chemistry										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Nitrogen, ammonia (KCL)	M350.1 - Automated Phenate	10	11.1		*	mg/Kg	0.5	5	12/10/13 17:19	bsu

Arizona license number: AZ0102



Inorganic Analytical Results

MWH Americas Inc.

ACZ Sample ID: **L15653-03**

Project ID: 10503311.020102 FML

Date Sampled: 11/05/13 10:00

Sample ID: WUA-CP03

Date Received: 11/20/13
Sample Matrix: Soil

Metals Analysis										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Cation Exchange Capacity (CEC)	USDA No. 60 (19)	1	10.0		*	meq/100g	0.03	0.2	12/05/13 11:52	aeb
Phosphorus, total (3050)	M6010B ICP	101	790		*	mg/Kg	10	50	12/02/13 21:56	aeb
Potassium, total (3050)	M6010B ICP	101	2620			mg/Kg	30	200	12/02/13 21:56	aeb
Soil Analysis										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Carbon, total organic (TOC)	ASA No.9 29-2.2.4 Combustion/IR	1	0.2	В	*	%	0.1	0.5	12/06/13 8:30	cra
Conductivity @25C	SM2510B									
Conductivity		1	0.456		*	mmhos/cm	0.001	0.01	11/27/13 0:00	spl
Max Particle Size		1	2000		*	um			11/27/13 0:00	spl
Organic Matter	USDA No.60 - Method 24	1	0.9	В	*	%	0.3	1	11/26/13 7:21	cra
pH, Saturated Paste	EPA 600/2-78-054, section 3.2.2									
Max Particle Size		1	2000		*	um			11/27/13 0:00	spl
pН		1	8.5		*	units	0.1	0.1	11/27/13 0:00	spl
Solids, Percent	CLPSOW390, PART F, D-98	1	93.0		*	%	0.1	0.5	11/22/13 16:00	spl
Soil Preparation										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Air Dry at 34 Degrees C	USDA No. 1, 1972				*				11/24/13 12:00	mss2
Cation Exchange Capacity Extraction	USDA No. 60 (19)				*				12/05/13 4:07	cdb
Digestion - Hot Plate	M3050B ICP								11/26/13 16:00	mss2
Potassium Chloride Extraction	ASA No. 9 33-3.2.2				*				12/04/13 18:00	spl
Saturated Paste Extraction	USDA No. 60 (2)				*				11/27/13 11:15	spl
Sieve-2000 um (2.0mm)	ASA No.9, 15-4.2.2				*				11/25/13 12:00	cra
Sieve-250 um (60 mesh)	ASA No.9, 15-4.2.2				*				11/25/13 12:00	cra
Wet Chemistry										
Parameter	EPA Method	Dilution	Result	Qual	XQ	Units	MDL	PQL	Date	Analyst
Nitrogen, ammonia (KCL)	M350.1 - Automated Phenate	10	10.7		*	mg/Kg	0.5	5	12/10/13 17:21	bsu

Arizona license number: AZ0102

Inorganic Reference

Report Header Explanations

Batch A distinct set of samples analyzed at a specific time

Found Value of the QC Type of interest Limit Upper limit for RPD, in %.

Lower Lower Recovery Limit, in % (except for LCSS, mg/Kg)

MDL Method Detection Limit. Same as Minimum Reporting Limit. Allows for instrument and annual fluctuations.

PCN/SCN A number assigned to reagents/standards to trace to the manufacturer's certificate of analysis

PQL Practical Quantitation Limit, typically 5 times the MDL.

QC True Value of the Control Sample or the amount added to the Spike

Rec Recovered amount of the true value or spike added, in % (except for LCSS, mg/Kg)

RPD Relative Percent Difference, calculation used for Duplicate QC Types

Upper Upper Recovery Limit, in % (except for LCSS, mg/Kg)

Sample Value of the Sample of interest

00				
[0][0]	San	nnle	H W	nes

AS	Analytical Spike (Post Digestion)	LCSWD	Laboratory Control Sample - Water Duplicate
ASD	Analytical Spike (Post Digestion) Duplicate	LFB	Laboratory Fortified Blank
CCB	Continuing Calibration Blank	LFM	Laboratory Fortified Matrix
CCV	Continuing Calibration Verification standard	LFMD	Laboratory Fortified Matrix Duplicate
DUP	Sample Duplicate	LRB	Laboratory Reagent Blank
ICB	Initial Calibration Blank	MS	Matrix Spike
ICV	Initial Calibration Verification standard	MSD	Matrix Spike Duplicate
ICSAB	Inter-element Correction Standard - A plus B solutions	PBS	Prep Blank - Soil
LCSS	Laboratory Control Sample - Soil	PBW	Prep Blank - Water
LCSSD	Laboratory Control Sample - Soil Duplicate	PQV	Practical Quantitation Verification standard
LCSW	Laboratory Control Sample - Water	SDL	Serial Dilution

QC Sample Type Explanations

Blanks Verifies that there is no or minimal contamination in the prep method or calibration procedure.

Control Samples Verifies the accuracy of the method, including the prep procedure.

Duplicates Verifies the precision of the instrument and/or method. Spikes/Fortified Matrix Determines sample matrix interferences, if any.

Standard Verifies the validity of the calibration.

ACZ Qualifiers (Qual)

- B Analyte concentration detected at a value between MDL and PQL. The associated value is an estimated quantity.
- H Analysis exceeded method hold time. pH is a field test with an immediate hold time.
- L Target analyte response was below the laboratory defined negative threshold.
- U The material was analyzed for, but was not detected above the level of the associated value.

The associated value is either the sample quantitation limit or the sample detection limit.

Method References

- (1) EPA 600/4-83-020. Methods for Chemical Analysis of Water and Wastes, March 1983.
- (2) EPA 600/R-93-100. Methods for the Determination of Inorganic Substances in Environmental Samples, August 1993.
- (3) EPA 600/R-94-111. Methods for the Determination of Metals in Environmental Samples Supplement I, May 1994.
- (4) EPA SW-846. Test Methods for Evaluating Solid Waste.
- (5) Standard Methods for the Examination of Water and Wastewater.

Comments

- (1) QC results calculated from raw data. Results may vary slightly if the rounded values are used in the calculations.
- (2) Soil, Sludge, and Plant matrices for Inorganic analyses are reported on a dry weight basis.
- (3) Animal matrices for Inorganic analyses are reported on an "as received" basis.
- (4) An asterisk in the "XQ" column indicates there is an extended qualifier and/or certification qualifier
- (5) If the MDL equals the PQL or the MDL column is omitted, the PQL is the reporting limit.

For a complete list of ACZ's Extended Qualifiers, please click:

 $\underline{http://www.acz.com/public/extquallist.pdf}$

Inorganic QC Summary

MWH Americas Inc. ACZ Project ID: L15653

Carbon, total of	ganic (T	OC)	ASA No.9	29-2.2.4 (Combustic	או /ווכ							
ACZ ID	Туре	Analyzed	PCN/SCN	QC	Sample	Found	Units	Rec	Lower	Upper	RPD	Limit	Qual
WG355912													
WG355912PBS	PBS	12/05/13 9:00				U	%		-0.3	0.3			
L15653-01DUP	DUP	12/05/13 20:45			.2	.2	%				0	20	RA ZO
Cation Exchang	ge Capac	ity (CEC)	USDA No	. 60 (19)									
ACZ ID	Туре	Analyzed	PCN/SCN	QC	Sample	Found	Units	Rec	Lower	Upper	RPD	Limit	Qual
WG355925													
WG355925ICV	ICV	12/05/13 11:17	II131113-1	100		97.97	mg/L	98	90	110			
WG355925ICB	ICB	12/05/13 11:20				U	meq/100g		-0.9	0.9			
WG355857PBS	PBS	12/05/13 11:33				U	meq/100g		-0.09	0.09			
L15653-01AS	AS	12/05/13 11:39	IICECSPIKE	10.8763	8.5	17.0846	meq/100g	78.9	75	125			
L15653-01ASD	ASD	12/05/13 11:42	IICECSPIKE	10.8763	8.5	17.4218	meq/100g	82	75	125	1.95	20	
L15653-03DUP	DUP	12/05/13 11:55			10	10.1496	meq/100g				1.5	20	
Conductivity @	25C		SM2510B										
ACZ ID	Туре	Analyzed	PCN/SCN	QC	Sample	Found	Units	Rec	Lower	Upper	RPD	Limit	Qual
WG355542													
L15653-01DUP	DUP	11/27/13 3:24			.442	.443	nmhos/cn				0.2	20	
Nitrogen, ammo	onia (KCI	L)	M350.1 - A	Automated	l Phenate								
ACZ ID	Туре	Analyzed	PCN/SCN	QC	Sample	Found	Units	Rec	Lower	Upper	RPD	Limit	Qual
WG356166													
WG356166ICV	ICV	12/10/13 12:10	WI131021-1	1.003		1.041	mg/L	103.8	90	110			
WG356166ICB	ICB	12/10/13 12:13				U	mg/L		-0.15	0.15			
WG356206													
WG356206LFB	LFB	12/10/13 17:14	WI121218-3	1		1.093	mg/L	109.3	90	110			
WG355866PBS	PBS	12/10/13 17:15				6.27	mg/Kg		-1.5	1.5			В
L15653-01DUP	DUP	12/10/13 17:17			10.6	9.9	mg/Kg				6.8	20	
145050 0040	AS						5 5	405.0	7.5	125			
L15653-02AS	,	12/10/13 17:20	WI121218-3	10	11.1	21.68	mg/Kg	105.8	75	120			
Organic Matter		12/10/13 17:20	WI121218-3 USDA No			21.68	mg/Kg	105.8	/5	120			
	Туре	12/10/13 17:20 Analyzed				21.68 Found		105.8 Rec	Lower	Upper	RPD	Limit	Qual
Organic Matter			USDA No	.60 - Meth	od 24						RPD	Limit	Qual
Organic Matter ACZ ID WG355454	Туре	Analyzed	USDA No PCN/SCN	.60 - Meth	od 24	Found	Units	Rec			RPD	Limit	Qual
Organic Matter ACZ ID WG355454 WG355454LCSS	Type	Analyzed 11/25/13 16:00	USDA No	.60 - Meth	od 24	Found	Units		Lower	Upper	RPD	Limit	Qual
Organic Matter ACZ ID WG355454	Туре	Analyzed	USDA No PCN/SCN	.60 - Meth	od 24	Found	Units	Rec			RPD 10.5	Limit 20	Qual R/
Organic Matter ACZ ID WG355454 WG355454LCSS WG355454PBS L15653-01DUP	Type LCSS PBS DUP	Analyzed 11/25/13 16:00 11/25/13 19:04	USDA No PCN/SCN	.60 - Meth	od 24 Sample	1.95 U .72	Units % %	Rec	Lower	Upper			
Organic Matter ACZ ID WG355454 WG355454LCSS WG355454PBS	Type LCSS PBS DUP	Analyzed 11/25/13 16:00 11/25/13 19:04	USDA No PCN/SCN PCN32557	.60 - Meth	od 24 Sample	1.95 U .72	Units % %	Rec	Lower	Upper			
Organic Matter ACZ ID WG355454 WG355454LCSS WG355454PBS L15653-01DUP PH, Saturated P	Type LCSS PBS DUP	Analyzed 11/25/13 16:00 11/25/13 19:04 11/26/13 1:12	USDA NO PCN/SCN PCN32557 EPA 600/	2-78-054,	od 24 Sample .8 section 3.	1.95 U .72	Wnits	Rec 97.5	Lower	Upper	10.5	20	R.
Organic Matter ACZ ID WG355454 WG355454LCSS WG355454PBS L15653-01DUP pH, Saturated P	Type LCSS PBS DUP	Analyzed 11/25/13 16:00 11/25/13 19:04 11/26/13 1:12	USDA NO PCN/SCN PCN32557 EPA 600/	2-78-054,	od 24 Sample .8 section 3.	1.95 U .72	Wnits	Rec 97.5	Lower	Upper	10.5	20	R/

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Inorganic QC Summary

MWH Americas Inc.

ACZ Project ID: L15653

Phosphorus, tota	ıl (3050)		M6010E	3 ICP									
ACZ ID	Туре	Analyzed	PCN/SCN	QC	Sample	Found	Units	Rec	Lower	Upper	RPD	Limit	Qual
WG355673													
WG355673ICV	ICV	12/02/13 21:13	II131111-1	5		5.19	mg/L	103.8	90	110			
WG355673ICB	ICB	12/02/13 21:16				U	mg/L		-0.3	0.3			
WG355503PBS	PBS	12/02/13 21:28				U	mg/Kg		-30	30			
WG355503LCSS2	LCSS	12/02/13 21:38	PCN39902	842		704	mg/Kg		673.6	1010.4			
WG355503LCSSD2	LCSSD	12/02/13 21:41	PCN39902	842		704	mg/Kg		673.6	1010.4	0	20	
L15653-01MS	MS	12/02/13 21:47	II131119-3	101.0202	790	892	mg/Kg	101	75	125			
L15653-01MSD	MSD	12/02/13 21:50	II131119-3	101.0202	790	879	mg/Kg	88.1	75	125	1.47	20	
Potassium, total	(3050)		M6010E	3 ICP									
ACZ ID	Туре	Analyzed	PCN/SCN	QC	Sample	Found	Units	Rec	Lower	Upper	RPD	Limit	Qual
WG355673													
WG355673ICV	ICV	12/02/13 21:13	II131111-1	20		19.64	mg/L	98.2	90	110			
WG355673ICB	ICB	12/02/13 21:16				U	mg/L		-0.9	0.9			
WG355503PBS	PBS	12/02/13 21:28				U	mg/Kg		-90	90			
WG355503LCSS1	LCSS	12/02/13 21:32	PCN42472	2600		2612	mg/Kg		1720	3470			
WG355503LCSSD1	LCSSD	12/02/13 21:35	PCN42472	2600		2872	mg/Kg		1720	3470	9.5	20	
L15653-01MS	MS	12/02/13 21:47	II131119-3	10094.48439	2410	13009	mg/Kg	105	75	125			
L15653-01MSD	MSD	12/02/13 21:50	II131119-3	10094.48439	2410	13059	mg/Kg	105.5	75	125	0.38	20	
Solids, Percent			CLPSO	W390, PART	F, D-98								
ACZ ID	Туре	Analyzed	PCN/SCN	QC	Sample	Found	Units	Rec	Lower	Upper	RPD	Limit	Qual
WG355296													
WG355296PBS	PBS	11/21/13 19:00				U	%		99.9	100.1			
	-					-							

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(800) 334-5493

Inorganic Extended Qualifier Report

ACZ Project ID: L15653 **MWH Americas Inc.**

ACZ ID	WORKNUM	PARAMETER	METHOD	QUAL	DESCRIPTION
L15653-01	WG355925	Cation Exchange Capacity (CEC)	USDA No. 60 (19)	ZH	Serial Dilution exceeded the acceptance criteria. Matrix interference [physical or chemical] is suspected.
	WG355912	Carbon, total organic (TOC)	ASA No.9 29-2.2.4 Combustion/IR	Q6	Sample was received above recommended temperature.
			ASA No.9 29-2.2.4 Combustion/IR	RA	Relative Percent Difference (RPD) was not used for data validation because the sample concentration is too low for accurate evaluation (< 10x MDL).
			ASA No.9 29-2.2.4 Combustion/IR	ZQ	Analyte was not evaluated in the laboratory control standard. Either the analyte is not included in the scope of the analytical method or a commercial standard containing the analyte is not available.
	WG355454	Organic Matter	USDA No.60 - Method 24	RA	Relative Percent Difference (RPD) was not used for data validation because the sample concentration is too low for accurate evaluation (< 10x MDL).
	WG356206	Nitrogen, ammonia (KCL)	M350.1 - Automated Phenate	B1	Target analyte detected in prep / method blank at or above the method reporting limit. See Case Narrative.
L15653-02	WG355925	Cation Exchange Capacity (CEC)	USDA No. 60 (19)	ZH	Serial Dilution exceeded the acceptance criteria. Matrix interference [physical or chemical] is suspected.
	WG355912	Carbon, total organic (TOC)	ASA No.9 29-2.2.4 Combustion/IR	Q6	Sample was received above recommended temperature.
			ASA No.9 29-2.2.4 Combustion/IR	RA	Relative Percent Difference (RPD) was not used for data validation because the sample concentration is too low for accurate evaluation (< 10x MDL).
			ASA No.9 29-2.2.4 Combustion/IR	ZQ	Analyte was not evaluated in the laboratory control standard. Either the analyte is not included in the scope of the analytical method or a commercial standard containing the analyte is not available.
	WG355454	Organic Matter	USDA No.60 - Method 24	RA	Relative Percent Difference (RPD) was not used for data validation because the sample concentration is too low for accurate evaluation (< 10x MDL).
	WG356206	Nitrogen, ammonia (KCL)	M350.1 - Automated Phenate	B1	Target analyte detected in prep / method blank at or above the method reporting limit. See Case Narrative.
L15653-03	WG355925	Cation Exchange Capacity (CEC)	USDA No. 60 (19)	ZH	Serial Dilution exceeded the acceptance criteria. Matrix interference [physical or chemical] is suspected.
	WG355912	Carbon, total organic (TOC)	ASA No.9 29-2.2.4 Combustion/IR	Q6	Sample was received above recommended temperature.
			ASA No.9 29-2.2.4 Combustion/IR	RA	Relative Percent Difference (RPD) was not used for data validation because the sample concentration is too low for accurate evaluation (< 10x MDL).
			ASA No.9 29-2.2.4 Combustion/IR	ZQ	Analyte was not evaluated in the laboratory control standard. Either the analyte is not included in the scope of the analytical method or a commercial standard containing the analyte is not available.
	WG355454	Organic Matter	USDA No.60 - Method 24	RA	Relative Percent Difference (RPD) was not used for data validation because the sample concentration is too low for accurate evaluation (< 10x MDL).
	WG356206	Nitrogen, ammonia (KCL)	M350.1 - Automated Phenate	B1	Target analyte detected in prep / method blank at or above the method reporting limit. See Case Narrative.

Certification Qualifiers

MWH Americas Inc. ACZ Project ID: L15653

Metals Analysis

The following parameters are not offered for certification or are not covered by AZ certificate #AZ0102.

Cation Exchange Capacity (CEC) USDA No. 60 (19)
Phosphorus, total (3050) M6010B ICP

The following parameters are not offered for certification or are not covered by NELAC certificate #ACZ.

Cation Exchange Capacity (CEC) USDA No. 60 (19)

Soil Analysis

The following parameters are not offered for certification or are not covered by AZ certificate #AZ0102.

Carbon, total organic (TOC) ASA No.9 29-2.2.4 Combustion/IR

Conductivity @25C SM2510B

Organic Matter USDA No.60 - Method 24
pH, Saturated Paste EPA 600/2-78-054, section 3.2.2
Solids, Percent CLPSOW390, PART F, D-98

The following parameters are not offered for certification or are not covered by NELAC certificate #ACZ.

Carbon, total organic (TOC) ASA No.9 29-2.2.4 Combustion/IR

Conductivity @25C SM2510B

Organic Matter USDA No.60 - Method 24
pH, Saturated Paste EPA 600/2-78-054, section 3.2.2
Solids, Percent CLPSOW390, PART F, D-98

Wet Chemistry

The following parameters are not offered for certification or are not covered by AZ certificate #AZ0102.

Nitrogen, ammonia (KCL) M350.1 - Automated Phenate

The following parameters are not offered for certification or are not covered by NELAC certificate #ACZ.

Nitrogen, ammonia (KCL) M350.1 - Automated Phenate



Sample Receipt

MWH Americas Inc. 10503311.020102 FML

Receipt Verification

ACZ Project ID: L15653

Date Received: 11/20/2013 10:28

Received By: mtb

Date Printed: 11/21/2013

	YES	NO	NA
1) Is a foreign soil permit included for applicable samples?			X
2) Is the Chain of Custody or other directive shipping papers present?	Х		
3) Does this project require special handling procedures such as CLP protocol?			Х
4) Are any samples NRC licensable material?			Х
5) If samples are received past hold time, proceed with requested short hold time analyses?	Х		
6) Is the Chain of Custody complete and accurate?	Х		
7) Were any changes made to the Chain of Custody prior to ACZ receiving the samples?		Χ	
Samples/Containers			
	YES	NO	NA
8) Are all containers intact and with no leaks?	X		
9) Are all labels on containers and are they intact and legible?	Χ		
10) Do the sample labels and Chain of Custody match for Sample ID, Date, and Time?	Х		
11) For preserved bottle types, was the pH checked and within limits?			Х
12) Is there sufficient sample volume to perform all requested work?	Χ		
13) Is the custody seal intact on all containers?			Х
14) Are samples that require zero headspace acceptable?			Х
15) Are all sample containers appropriate for analytical requirements?	Χ		
16) Is there an Hg-1631 trip blank present?			Х
17) Is there a VOA trip blank present?			Х
18) Were all samples received within hold time?	Χ		

Chain of Custody Related Remarks

Client Contact Remarks

Shipping Containers

Cooler Id	Temp (°C)	Rad (μ R/Hr)	Custody Seal Intact?
NA18751	14.8	13	N/A

Was ice present in the shipment container(s)?

No - Wet or gel ice was not present in the shipment container(s).

Client must contact an ACZ Project Manager if analysis should not proceed for samples received outside of their thermal preservation acceptance criteria.



Chain of Custody ID_

Cooler ID_

of	LABORATORY USE ONLY	SAMPLES WERE: 1 Shipped or hand delivered Notes: 2 Ambient or Chilled	Notes: 3 Temperature	ken/Lesealed) N N N Inin Inin S N N N N ample Sample	Y N NA NA NA NA Notes: Discrepancies Between Sample Labels and COC Record? Y N NA Notes:
PageAir Bill No.	•) T (DDMMYYNN)) T (DDMMYYNN)			Time
		(имууммаа) то	DJ 8A	ONS	σ.
	ANALYSES REQUESTED	103.64 AG	NS	SPECIAL INSTRUCTIONS.	Received by/Affiliation Date
	<u>(</u>	e Number au No. 6001 A No. 6001 A No. 6001 A No. 6001 A No. 6001	xinteM GampS	SO G C C C C C C C C C C C C C C C C C C	Relinquished by/Affiliation
		Collected	əmiT	sampling Technique: Composite=C Grab=G Grab=G Grab=G Grab=G France Pump=PP Paristalic Pump=PP	Time O S
		Collected	Date	123 · -	Date (30.B)
McDorough	1) 617-3200	LOIOZ FAC	e Depth Interval (ft)	1 (- 15 / 11/2) 1 - 15 / 12/2 1 - 15 / 12/2 1 Water EP/TCLP Leachate WQ - Trip Blank, EB - Equipment Blanks WW - Wastewater	Received by/Affiliation COC RES II
AC .	7-4200 FAX (80	25/20	Field Sample ID	WUA - CPO2 $WUA - CPO3$ $WUA - CPO3$ $WUA - CPO3$ $WUA - CPO3$ $WUA - CPO2$	Relinquished by/Affijiation
LABORATORY_Contact_M.C.	Phone (801) 61	Project W.S.C. Project Number Date Due	Location ID	WUU WUU WUU WW - Soull SC - Sodiment WS - Surface W	Relinqu

Analytical Quote

Chad Tomlinson MWH Americas Inc. 2890 E. Cottonwood Pkwy. Suite 300 Salt Lake City, UT 84121 Page 1 of 2 11/7/2013

Quote Number: FMC-AGRONOMIC

Matrix: Soil

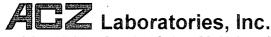
3 Samples, One Time Analysis of Soil - FMC Agronomic Testing

Parameter	Method	Detection Limit	Cost/Sample
Metals Analysis			
Cation Exchange Capacity (CEC)	USDA No. 60 (19)	0.03 meq/100g	\$24.00
Phosphorus, total (3050)	M6010B ICP	10 mg/Kg	\$10.00
Potassium, total (3050)	M6010B ICP	30 mg/Kg	\$10.00
Misc.			
Electronic Data Deliverable			\$0.00
Quality Control Summary			\$0.00
Setup charge for ICP, total			\$16.00
Sample Preparation			
Air Dry at 34 Degrees C	USDA No. 1, 1972		\$8.00
Cation Exchange Capacity Extraction	USDA No. 60 (19)		\$0.00
Digestion - Hot Plate	M3050B ICP		\$16.00
Potassium Chloride Extraction	ASA No. 9 33-3.2.2		\$12.00
Saturated Paste Extraction	USDA No. 60 (2)		\$18.00
Sieve-2000 um (2.0mm)	ASA No.9, 15-4.2.2		\$12.00
Sieve-250 um (60 mesh)	ASA No.9, 15-4.2.2		\$12.00
Soil Analysis			
Carbon, total organic (TOC)	ASA No.9 29-2.2.4 Combustion/IR	0.1 %	\$38.00
Conductivity @25C	SM2510B	0.001 mmhos/cm	\$8.00
Organic Matter	USDA No.60 - Method 24	0.3 %	\$25.00
pH, Saturated Paste	EPA 600/2-78-054, section 3.2.2	0.1 units	\$8.00
Solids, Percent	CLPSOW390, PART F, D-98	0.1 %	\$8.00
Wet Chemistry			•
Nitrogen, ammonia (KCL)	M350.1 - Automated Phenate	0.5 mg/Kg	\$11.00
		Cost/Sample:	\$236.00

This quote is based on a Standard Turnaround Time (TAT) of approximately 21 days for soil and solid matrices (15 working days). TAT may vary with seasonal heavy workload. Please contact your PM if rush TAT is required. Rush TAT needs to be pre-approved prior to sample shipment to assure that due dates can be met. Pricing includes standard reporting formats and standard ACZ EDDs. All projects received are subject to a \$125.00 Minimum Charge. Please note that method detection limits are estimates and may be elevated depending on sample matrices that require dilution. Pricing includes coolers, soil jars or bags, labels, COCs and ice-packs if needed for your analysis, shipped to your site or office via UPS ground. Return shipping is the responsibility of the client. Please allow ample time for your bottles to arrive. Please note that soil preparation charges may fluctuate depending on the condition and volume of samples upon receipt. Wet samples may increase your TAT if air-drying is needed per your analysis.

REPAD.09.06.05.01 S/ m D/

P/



Analytical Quote

Chad Tomlinson
MWH Americas Inc.
2890 E. Cottonwood Pkwy. Suite 300
Salt Lake City, UT 84121

Page 2 of 2 11/7/2013

Quote Number: FMC-AGRONOMIC

CONTRACT DETAILS

Pricing includes shipment of all standard sample containers and related paperwork by UPS Ground Service. Please allow three to five days for delivery when ordering containers. ACZ must be notified prior to receiving samples of all special requests such as electronic data deliverables or special reporting regirements. The client will be charged for special sample containers or express shipping and additional charges may apply for non-standard requests.

This quotation is valid for six months from the bid date unless specified otherwise in the bid. All bids must be signed and returned to ACZ before the project(s) is received. The authorized signature represents acceptance of the pricing as well as the general terms and conditions of ACZ Laboratories, Inc. which may be downloaded from our web site at http://www.acz.com/PDF/termsconditions.pdf. Please note that MDL's in this quote may possibly increase due to sample matrix or samples with high TDS.

All orders that require shipping of coolers are subject to a minimum charge of \$200.00. Local orders without shipping are subject to a minimum charge of \$125.00. Samples may incur a \$11.00/sample disposal fee for any samples deemed to be hazardous.

ACZ Representative (Authorized signature and date)	
Client Representative (Authorized signature and date)	

REPAD.09.06.05.01

S/ m D/

APPENDIX F

Root Density Testing Report

Table of Soil and Root Weights for FMC Vegetation Survey Sample Locations from Nov. 12 and 13, 2013.

Sample	Soil Dry Weight	Root Dry Weight	Soil Dry Weight	Grams of Roots
	with Roots	(grams)	Without Roots	per 100 grams
	(grams)		(grams)	of Soil
Grid #6—Location #1				
0-6 inches	807.45	0.15	807.30	0.019
6-12 inches	798.26	0.62	797.64	0.078
12-18 inches	786.17	0.02	786.15	0.003
Grid #6—Location #2				
0-6 inches	785.39	0.66	784.73	0.084
6-12 inches	792.90	0.15	792.75	0.019
12-18 inches	837.52	0.12	837.40	0.014
Grid #6—Location #3				
0-6 inches	744.77	0.24	744.53	0.032
6-12 inches	823.04	0.11	822.93	0.013
12-18 inches	804.68	0.04	804.64	0.005
Grid #7—Location #1				
0-6 inches	684.09	0.27	683.82	0.039
6-12 inches	813.18	0.16	813.02	0.020
12-18 inches	832.20	0.11	832.09	0.013
Grid #7—Location #2				
0-6 inches	829.41	0.30	829.11	0.036
6-12 inches	746.12	0.22	745.90	0.029
12-18 inches	844.83	0.18	844.65	0.021
Grid #7—Location #3				
0-6 inches	764.65	0.68	763.97	0.089
6-12 inches	781.57	0.19	781.38	0.024
12-18 inches	872.89	0.13	872.76	0.015
Grid #8—Location #1				
0-6 inches	769.74	0.79	768.95	0.102
6-12 inches	No sample	No sample	No sample	No sample
12-18 inches	806.99	0.16	806.83	0.020
18-24 inches	849.00	0.05	848.95	0.006
Grid #8—Location #2				
0-6 inches	762.51	0.58	761.93	0.076
6-12 inches	872.86	0.65	872.21	0.075
12-18 inches	801.06	0.10	800.96	0.013
18-24 inches	742.14	0.03	742.11	0.004
Grid #8—Location #3				
0-6 inches	797.74	0.38	797.36	0.048
6-12 inches	820.28	0.23	820.05	0.028
12-18 inches	839.66	0.11	839.55	0.013
Grid #13—Location #1				
0-6 inches	839.18	0.87	838.31	0.104
6-12 inches	699.50	0.25	699.25	0.036
12-18 inches	No sample	No sample	No sample	No sample

Sample	Soil Dry Weight	Root Dry Weight	Soil Dry Weight	Grams of Roots
	with Roots	(grams)	Without Roots	per 100 grams
	(grams)		(grams)	of Soil
Grid #13—Location #2				
0-6 inches	793.79	0.51	793.28	0.064
6-12 inches	849.62	0.27	849.35	0.032
12-18 inches	No sample	No sample	No sample	No sample
Grid #13—Location #3				
0-6 inches	725.44	0.73	724.71	0.101
6-12 inches	961.91	0.33	961.58	0.034
12-18 inches	867.40	0.12	867.28	0.014
Grid #14—Location #1				
0-6 inches	814.19	0.71	813.48	0.087
6-12 inches	833.37	0.45	832.92	0.054
12-18 inches	834.95	0.13	834.82	0.016
Grid #14—Location #2				
0-6 inches	713.84	0.78	713.06	0.109
6-12 inches	898.16	0.46	897.70	0.051
12-18 inches	797.55	0.21	797.34	0.026
Grid #14—Location #3				
0-6 inches	807.28	0.43	806.85	0.053
6-12 inches	780.36	0.31	780.05	0.040
12-18 inches	805.32	0.15	0.15 805.17	
Grid #15—Location #1				
0-6 inches	835.20	0.45	834.75	0.054
6-12 inches	772.33	0.14	772.19	0.018
12-18 inches	800.00	0.09	799.91	0.011
Grid #15—Location #2				
0-6 inches	729.58	0.56	729.02	0.077
6-12 inches	746.83	0.28	746.55	0.038
12-18 inches	848.75	0.07	848.68	0.008
Grid #15—Location #3				
0-6 inches	759.06	0.45	758.61	0.060
6-12 inches	930.29	0.21	930.08	0.023
12-18 inches	777.64	0.10	777.54	0.013
Grid #16—Location #1				
0-6 inches	822.27	0.57	821.70	0.069
6-12 inches	772.75	0.39	772.36	0.051
12-18 inches	831.66	0.13	831.53	0.016
Grid #16—Location #2				
0-6 inches	707.11	0.83	706.28	0.118
6-12 inches	844.97	0.37	844.60	0.044
12-18 inches	791.54	0.18	791.36	0.023

Sample	Soil Dry Weight with Roots (grams)	Root Dry Weight (grams)	Soil Dry Weight Without Roots (grams)	Grams of Roots per 100 grams of Soil
Grid #16—Location #3				
0-6 inches	743.60	0.62	742.98	0.083
6-12 inches	822.37	0.25	822.12	0.030
12-18 inches	773.69	0.12	773.57	0.016
Grid #17—Location #1				
0-6 inches	708.05	0.66	707.39	0.093
6-12 inches	778.98	0.19	778.79	0.024
12-18 inches	901.58	0.12	901.46	0.013
18-24 inches	810.23	0.04	810.19	0.005
Grid #17—Location #2				
0-6 inches	833.19	0.43	832.76	0.052
6-12 inches	811.03	0.16	810.87	0.020
12-18 inches	893.77	0.13	893.64	0.015
18-24 inches	877.61	0.02	877.59	0.002
Grid #17—Location #3				
0-6 inches	806.03	0.30	805.73	0.037
6-12 inches	871.40	0.27	871.13	0.031
12-18 inches	795.86	0.12	795.74	0.015
18-24 inches	796.35	0.05	796.30	0.006
Grid #18—Location #1				
0-6 inches	838.61	0.12	838.49	0.014
6-12 inches	854.60	0.15	854.45	0.018
12-18 inches	798.19	0.02	798.17	0.003
Grid #18—Location #2				
0-6 inches	776.15	0.53	775.62	0.068
6-12 inches	785.08	0.18	784.90	0.023
12-18 inches	838.00	0.11	837.89	0.013
Grid #18—Location #3				
0-6 inches	761.44	0.31	761.13	0.041
6-12 inches	731.57	0.16	731.41	0.022
12-18 inches	784.39	0.09	784.30	0.011

APPENDIX G

Stormwater Sewer Decontamination Water Laboratory Analysis Report and Video Survey

IAS EnviroChem
3314 Pole Line Rd. • Pocatello, ID 83201

Phone: (208) 237-3300 • Fax: (208) 237-3336 email: iasec3308@iasenvirochem.com • www.iasenvirochem.com

Kase Warbonnet Inc.

Date Submitted: 11/14/2013 **Date Reported:** 12/03/2013

Mark R. Smith 1477 Thunderbolt Pocatello, ID 83204

Certificate of Analysis

Sample Description: 111413-SDL Lab Tracking #: I311052-01 **Sampling Date/Time:** 11/14/13 13:40

<u>Analyte</u>	<u>Result</u>	<u>Units</u>	<u>Method</u>	<u>Analyzed</u>	<u>Analyst</u>
pH	7.6	pH Units	150.1	11/18/2013	MAD
TCLP Arsenic	< 0.05	mg/L	1311/6020A	11/29/2013	RP
TCLP Barium	0.07	mg/L	1311/6020A	11/29/2013	RP
TCLP Cadmium	< 0.05	mg/L	1311/6020A	11/29/2013	RP
TCLP Chromium	0.08	mg/L	1311/6020A	11/29/2013	RP
TCLP Lead	< 0.05	mg/L	1311/6020A	11/29/2013	RP
TCLP Mercury	< 0.01	mg/L	1311/6020A	11/29/2013	RP
TCLP Selenium	< 0.05	mg/L	1311/6020A	11/29/2013	RP
TCLP Silver	< 0.05	mg/L	1311/6020A	11/29/2013	RP

IAS EnviroChem

3314 Pole Line Rd. • Pocatello, ID 83201

Phone: (208) 237-3300 • Fax: (208) 237-3336 email: iasec3308@iasenvirochem.com • www.iasenvirochem.com

Kase Warbonnet Inc.

Date Submitted: 11/14/2013 **Date Reported:** 12/03/2013

Mark R. Smith 1477 Thunderbolt Pocatello, ID 83204

Certificate of Analysis

Sample Description: 111413-SDS **Lab Tracking #:** I311052-02 **Sampling Date/Time:** 11/14/13 13:55

<u>Analyte</u>	<u>Result</u>	<u>Units</u>	<u>Method</u>	<u>Analyzed</u>	<u>Analyst</u>
TCLP Arsenic	< 0.05	mg/L	1311/6020A	11/29/2013	RP
TCLP Barium	0.32	mg/L	1311/6020A	11/29/2013	RP
TCLP Cadmium	0.06	mg/L	1311/6020A	11/29/2013	RP
TCLP Chromium	< 0.05	mg/L	1311/6020A	11/29/2013	RP
TCLP Lead	< 0.05	mg/L	1311/6020A	11/29/2013	RP
TCLP Mercury	< 0.01	mg/L	1311/6020A	11/29/2013	RP
TCLP Selenium	< 0.05	mg/L	1311/6020A	11/29/2013	RP
TCLP Silver	< 0.05	mg/L	1311/6020A	11/29/2013	RP

StyPathe

IAS EnviroChem

3314 Pole Line Rd. • Pocatello, ID 83201

Phone: (208) 237-3300 • Fax: (208) 237-3336 email: iasec3308@iasenvirochem.com • www.iasenvirochem.com

Login Report

Customer Name: Kase Warbonnet Inc.

Work Order #: **I311052**

1477 Thunderbolt Pocatello, ID 83204

Contact Name: Mark R. Smith

Comment:

Sample Description: 111413-SDL Sampling Date/Time: 11/14/13 13:40

Lab Tracking #: **I311052-01**

Matrix: Water Date Received: 11/14/13 14:25

Sample Notes:

<u>Test</u> Method <u>Due</u> pН 150.1 11/28/13 **TCLP Arsenic** 1311/6020A 11/28/13 **TCLP Barium** 1311/6020A 11/28/13 **TCLP Cadmium** 1311/6020A 11/28/13 1311/6020A **TCLP Chromium** 11/28/13 **TCLP Lead** 1311/6020A 11/28/13 1311/6020A 11/28/13 **TCLP Mercury TCLP Selenium** 1311/6020A 11/28/13 **TCLP Silver** 1311/6020A 11/28/13

Sample Description: 111413-SDS Sampling Date/Time: 11/14/13 13:55

Lab Tracking #: **I311052-02**

Matrix: Solid Date Received: 11/14/13 14:25

Sample Notes:

<u>Test</u>	<u>Method</u>	<u>Due</u>
TCLP Arsenic	1311/6020A	11/28/13
TCLP Barium	1311/6020A	11/28/13
TCLP Cadmium	1311/6020A	11/28/13
TCLP Chromium	1311/6020A	11/28/13
TCLP Lead	1311/6020A	11/28/13
TCLP Mercury	1311/6020A	11/28/13
TCLP Selenium	1311/6020A	11/28/13
TCLP Silver	1311/6020A	11/28/13

Sample Condition Record

Samples received in a cooler?	No
Samples received intact?	Yes
The temperature recorded?	19.8
Samples received with a COC?	Yes
Samples received within holding time?	Yes
Are all samples properly preserved?	Yes
Labels and chain agree?	Yes

RP

9 **9** 1311052 Comments Kase Warbonnet Inc. Temp 19.8 C Received: 11/14/2013 YES YES 2 Samples labels and Chain Agree? Conteiner Beeled? P: (208) 237-3300 F: (208) 237-3336 • Email: lasec3308@lasenvirochem.com **Analyses Requested** IAS EnviroChem - 3314 Pole Line Rd • Pocatello, ID 83201 Special Instructions RECEIVED BY J Date/Time 111413 Printed Name 🛴 Signature d701 Number of Containers 11/4/13 1340 CCC1 21/4/17 19/14/13 1355 Date/Time Collected Send Bill or Receipt To: KASIT/IL/ANDOWNIET 83201 WARDONNET 1472 TRUNDER 60 (+ ***** ₩ 6276 SAMPLE INFORMATION RELINQUISHED BY Sample Description H Received by 1413-512 d 5 -8/1/1 208-232 Cash Cash Check# Pocate 110 Company Name KASE Payment due with samples unless cradit has been established Email Involce to: Printed Name Date/Time Signature TRK # (Lab use) ☐ Officer Amount Address Phone Email

DVD of Stormwater Sewer Piping Video Survey (included in Hard Copy Reports Only)

APPENDIX H

ProUCL 5.0 Statistical Analysis

<u>+</u>		Normal Background St	atistics for	Full Data Se	ets				
v.pd	User Selected Options				-				
l Re	From File	C:\Users\hartmanrj\Doo	cuments\FM	C Proiects\F	RD Work Pl	ans\Data G	ap WP\Field	Data\Geote	ech data for
hted	Full Precision	OFF							
the FMC OU - Highlighted Rev.pdf	Confidence Coefficient	95%							
- Hig	Coverage	90%							
00	Different or Future K Values	1							
MC	Sincrem of Fatare R values	•							
Эе									
± MÐD									
2014-03-14 FMC Data Gap Report S									
Rep	Raw S	tatistics							
зар	Numbe	er of Valid Observations	10						
ata (Number	of Distinct Observations	10						
De	Number		97.7						
FM(Minimum							
14		Maximum	107.2						
4-03		Second Largest	107						
2014		Mean	104.2						
		Geometric Mean	104.1						
		First Quartile	103.8						
		Median	104.6						
		Third Quartile	106.8						
		SD	3.215						
			0.0309						
		Skewness	-1.211						
		tribution Test							
		apiro Wilk Test Statistic	0.843						
		apiro Wilk Critical Value	0.842						
	Data appear Normal a	t 5% Significance Level							
	Background Statistics Ass	•							
		90% Percentile (z)	108.3						
		95% Percentile (z)	109.5						
		99% Percentile (z)	111.7						
		Tolerance Factor K	2.355						
	95% U	TL with 90% Coverage	111.8						
		95% UPL (t)	110.4						
Aver	age K								
	Raw S	tatistics							
	Numbe	er of Valid Observations	6						
	Number	of Distinct Observations	6						
		Minimum	2.3000E-5						
		Maximum	1.4000E-4						
		Second Largest	7.8000E-5						
			6.5667E-5						
		Geometric Mean	5.5682E-5						
								1	

<u></u>	First Quartile	3 92505-5						
FMC OU - Highlighted Rev.pdf								
Rev		6.0000E-5						
ed	Third Quartile							
ight	SD	4.1563E-5						
ighl	Coefficient of Variation	N/A						
Ŧ	Skewness	1.252						
00								
N N	Warning: A sample size of 'n' = 6 may not adequate	a anough to	compute	meaninaful	and reliable	toet etatieti	re and seti	matesl
e E	Warning. A sumple size of 11 - 6 may not adequate	o chough to	compute	incaming a	and reliable	tost statisti	os and esti	nates:
r th								
nt fo	It is suggested to collect at leas							
еро	If possible compute and collect Data Qua	ility Objectiv	res (DQO)	based san	iple size and	analytical	results.	
рВ								
Ga								
ata	Normal Distribution Test							
CD	Shapiro Wilk Test Statistic	0.901						
\geq								
4	5% Shapiro Wilk Critical Value	0.788						
2014-03-14 FMC Data Gap Report for the	Data appear Normal at 5% Significance Level							
014								
2	Background Statistics Assuming Normal Distribut	ion						
	90% Percentile (z)	1.1893E-4						
	95% Percentile (z)							
	99% Percentile (z)							
	55 % Fercentile (2)	1.0230L-4						
	Tolerance Factor K	3.006						
	95% UTL with 90% Coverage	1.9060E-4						
	95% UPL (t)	1.5613E-4						
In-sit	u Moisture							
	Raw Statistics							
	Number of Valid Observations	9						
	Number of Distinct Observations	9						
	Minimum	4.8						
	Maximum	15.5						
	Second Largest	15.1						
	Mean	8.733						
	Geometric Mean	7.987						
	First Quartile	5.9						
	Median	8.4						
	Third Quartile	9.4						
	SD	4.071						
	Coefficient of Variation	0.466						
	Skewness	0.972						
	Normal Distribution Test							
	Shapiro Wilk Test Statistic	0.839						
	5% Shapiro Wilk Critical Value	0.829						
		0.029						
	Data appear Normal at 5% Significance Level							
	Background Statistics Assuming Normal Distribut	ion						
					1	I.	I	

)df	90% Percentile (z)	13.95					
ev.p	95% Percentile (z)	15.43					
å R	99% Percentile (z)	18.2			†		
eport for the FMC OU - Highlighted Rev.pdf							
ighli	Tolerance Factor K	2.454					
Ŧ	95% UTL with 90% Coverage	18.72		 	 		<u> </u>
9							
MC	95% UPL (t)	16.71		-	-	<u> </u>	
је Е	33 % SI E (I)	. 5.7 1					
or th							
ort f							
PA-	u Density					-	
ni-sit	a solidity						
ta G	David Olari et						
) Da	Raw Statistics						
= MC	Number of Valid Observations	9					
14 F	Number of Distinct Observations	9					
-03-	Minimum	70.4					
014	Raw Statistics Number of Valid Observations Number of Distinct Observations Minimum Maximum Second Largest	94.7					
2		90.8					
	Mean	81.11					
	Geometric Mean	80.82					
	First Quartile	77.5					
	Median	79.3		†	 		
	Third Quartile	81.7					
	SD	7.368		+			
	Coefficient of Variation	0.0908		-			
	Skewness	0.0908				-	
	Normal Distribution Test Shapiro Wilk Test Statistic 5% Shapiro Wilk Critical Value	0.895 0.829					
	Data appear Normal at 5% Significance Level	520					
	The state of the s						
	Background Statistics Assuming Normal Distribution	วท				-	
	90% Percentile (z)	90.55					
	95% Percentile (z)	93.23					
	95% Percentile (z) 99% Percentile (z)	93.23	-			-	
	99% Percentile (z)	ყნ.∠5					
	_ '	0.4-					
	Tolerance Factor K	2.454					
	95% UTL with 90% Coverage	99.19					
	95% UPL (t)	95.55					
		7					
Optin	num Moisture						
	Raw Statistics						
	Number of Valid Observations	10					
	Number of Distinct Observations	9					
	Minimum	15.9		†	 		<u> </u>
	Maximum	22.7					
	Second Largest	19.4					
	SSSSII Edigost						

Commercia							
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	Jpc						
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	Rev.F						
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	ed F						
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	light						
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	ligh	Third Quartile	17.65				
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	J - L	SD	2.024				
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	000	Coefficient of Variation	0.115				
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	FM(Skewness	2.059				
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	the						
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	t for	Normal Distribution Test					
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	epor	Shapiro Wilk Test Statistic	0.756				
Tolerance Factor K 2.355 95% UTL with 90% Coverage 22.42 95% UTL with 90% Coverage 22.42 95% UPL (t) 21.54 95% UPL (t) 21.54 95% Percentile (z) 18.41 95% Percentile	p R(5% Shapiro Wilk Critical Value	0.842				
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Optimum Moisture w/o outlier Raw Statistics Number of Valid Observations Number of Distinct Observations Maximum 15.9 Maximum 19.4 Second Largest 17.7 Mean 17.09 Geometric Mean 17.06 First Quartile 16.6 Median 16.8 Third Quartile 17.5 SD 1.033 Coefficient of Variation Skewness 1.473 Normal Distribution Test Shapiro Wilk Test Statistic Shapiro Wilk Critical Value Data appear Normal at 5% Significance Level Background Statistics Assuming Normal Distribution 90% Percentile (z) 18.41 95% Percentile (z) 18.79		'					
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Raw Statistics Number of Valid Observations 9 Number of Distinct Observations 8 Number of Distinct Observations 15.9 Number of Distinct Observations 15.9 Number of Distinct Observations 17.7 Number of Distinct Observations 17.0 Number of Distinct Observations 17.0 Number of Distinct Observations 18.8 N		1					
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Shapiro Wilk Test Statistic 0.877 5% Shapiro Wilk Critical Value 0.829 Data appear Normal at 5% Significance Level Background Statistics Assuming Normal Distribution 90% Percentile (z) 18.41 95% Percentile (z) 18.79		Skewness	1.473				
Shapiro Wilk Test Statistic 0.877 5% Shapiro Wilk Critical Value 0.829 Data appear Normal at 5% Significance Level Background Statistics Assuming Normal Distribution 90% Percentile (z) 18.41 95% Percentile (z) 18.79		'					
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Tolerance Factor K

95% UPL (t)

95% UTL with 90% Coverage

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0		value: 0.4 value: 0.47										
0	critical value: 0.597 Descritical value: 0.597 Data Value 22.7 is a Potential Outlier (Upper Tail)?											
	ata Va	lue 22.7 is	s a Potential	Outlier (Upr	er Tail)?							
03-14												
	Test Statistic: 0.508											
20												
For 10% significance level, 22.7 is an outlier.												
For 5	% sign	ificance le	evel, 22.7 is a	n outlier.								
For 1	For 1% significance level, 22.7 is not an outlier.											
2. Da	ıta Valı	ue 15.9 is	a Potential (Outlier (Low	er Tail)?							
Test	Statisti	c: 0.086										
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Raw Statistics Number of Valid Observations 27							
Geometric Mean 0.0598							
Geometric Mean 0.0598							
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Geometric Mean 0.0598							
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Geometric Mean 0.0598							
Geometric Mean 0.0598							
Median 0.068							
Third Oversille 0.000							
Third Quartile 0.088							
SD 0.0285							
Coefficient of Variation 0.425							
Skewness -0.0498							
Normal Distribution Test							
Shapiro Wilk Test Statistic 0.973							
5% Shapiro Wilk Critical Value 0.923							
Data appear Normal at 5% Significance Level							
Background Statistics Assuming Normal Distribution							
90% Percentile (z) 0.103							
95% Percentile (z) 0.114							
99% Percentile (z) 0.133							
Tolerance Factor K 1.811							
95% UTL with 90% Coverage 0.119							
95% UPL (t) 0.116							
40.40 %							
12 to 18 inches							
Raw Statistics							
Number of Valid Observations 25							
Number of Valid Observations 25 Number of Distinct Observations 13							
Minimum 0.003							
Maximum 0.026							
Second Largest 0.023							
Mean 0.014							
Geometric Mean 0.0125							

Jp(First Quartile				0.013			
ev.p		0.014						
ed R	Third Quartile				0.016			
- Highlighted Rev.pdf	SD				0.00553			
ighli	Coefficient of Variation			0.396				
H - 1	Skewness			-0.11				
00 (
FMC		Normal Dist	ribution Tes	st				
the		Sh	apiro Wilk T	est Statistic	0.946			
for		5% Sha	apiro Wilk C	ritical Value	0.918			
hoda	Data appea	ar Normal at	t 5% Signific	cance Level				
p Re								
Data Gap Report for the	Background Statistics Assuming Normal Distribution							
Jata			90% P	ercentile (z)	0.021			
			95% P	ercentile (z)	0.023			
4 FI			99% P	ercentile (z)	0.0268			
2014-03-14 FMC								
14-			Toleran	ice Factor K	1.838			
20		95% U	TL with 909	% Coverage	0.0241			
			(95% UPL (t)	0.0236			
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the FMC								
	12 inches							
port								
p Re		Raw Statistics						
a Ga		Number of Valid Observations	26					
Data		Number of Distinct Observations	21					
MC		Minimum	0.013					
-14 F		Maximum	0.078					
2014-03-14 FMC Data Gap Report		Second Largest	0.075					
2014		Mean Coornatria Maan	0.0337					
-		Geometric Mean	0.0304					
		First Quartile Median	0.0223 0.0295					
		0.0295						
		0.0393						
		SD	5.5107					
	Gamma Distribution Test							
		5.026						
		k hat (MLE) k star (bias corrected MLE)	4.472					
		Theta Hat (MLE)	0.0067					
		0.00753						
		nu hat (MLE)	261.4					
	·	ased upon bias corrected estimates)	232.5					
	•	ased upon bias corrected estimates)	0.0337 0.0159					
	MLE Sd (based upon bias corrected estimates)							
		95% Percentile of Chisquare (2k)	16.84					
		A-D Test Statistic	0.497					
		5% A-D Critical Value	0.497					
		K-S Test Statistic	0.137					
		5% K-S Critical Value	0.172					
	Data appear Gamma I	Distributed at 5% Significance Level						
	Background Statistic	cs Assuming Gamma Distribution						
		90% Percentile	0.055					
		95% Percentile	0.0634					
		99% Percentile	0.0812					
	050/ 147	LUIGanto (AAALI) Arraman O	0.0040					
		Hilferty (WH) Approx. Gamma UPL	0.0643					
	95% Hawkins	s Wixley (HW) Approx. Gamma UPL	0.0648					
		Tolerance Factor K	1.824					
959	% Wilson Hilferty (WH) Approx	x. Gamma UTL with 90% Coverage	0.0663					
		x. Gamma UTL with 90% Coverage	0.0669					
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pdf	Nonparametic Background Statistics				
OU - Highlighted Rev.pdf	95% Chebyshev UPL	0.108			
ed F	95% BCA Bootstrap UTL with 90% Coverage	0.075			
light	95% Bootstrap (%) UTL with 90% Coverage	0.0765			
ligh					
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0 <u>∓</u> to	2 inches				
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t for	Raw Statistics				
pode	Number of Valid Observations	53			
p Re	Number of Distinct Observations	44			
Ga	Minimum	0.013			
)ata	Maximum	0.118			
2	Second Largest	0.109			
4 F	Mean	0.0506			
2014-03-14 FMC Data Gap Report for the Fall	Geometric Mean	0.0429			
14-(First Quartile	0.028			
20	Median	0.041			
	Third Quartile	0.075			
	SD	0.0287			
	Gamma Distribution Test				
	k hat (MLE)	3.169			
	k star (bias corrected MLE)	3.002			
	Theta Hat (MLE)	0.016			
	Theta star (bias corrected MLE)	0.0169			
	nu hat (MLE)	335.9			
	nu star (based upon bias corrected estimates)	318.2			
	MLE Mean (based upon bias corrected estimates)	0.0506			
	MLE Sd (based upon bias corrected estimates)	0.0300			
	95% Percentile of Chisquare (2k)	12.6			
	33 % Fercentile of Chisquare (2K)	12.0			
	A-D Test Statistic	0.602			
	5% A-D Critical Value	0.757			
	K-S Test Statistic	0.088			
	5% K-S Critical Value	0.123			
	Data appear Gamma Distributed at 5% Significance Level				
	Declarational Obstitution Assessment Community of				
	Background Statistics Assuming Gamma Distribution	0.0000			
	90% Percentile	0.0898			
	95% Percentile	0.106			
	99% Percentile	0.142			
	0.50/ Mill.				
	95% Wilson Hilferty (WH) Approx. Gamma UPL	0.107			
	95% Hawkins Wixley (HW) Approx. Gamma UPL	0.109			
	Tolerance Factor K	1.628			
	6 Wilson Hilferty (WH) Approx. Gamma UTL with 90% Coverage	0.104			
95%	Hawkins Wixley (HW) Approx. Gamma UTL with 90% Coverage	0.106			
	Nonparametic Background Statistics				
	95% Chebyshev UPL	0.177			

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95% BCA Bootstrap UTL with 90% Coverage

95% Bootstrap (%) UTL with 90% Coverage

0.103

0.104

FMC Responses to EPA Comments, dated and received February 20, 2014, on the Remedial Design (RD) Data Gap Report for the FMC Operable Unit (OU), submitted January 28, 2014

March 14, 2014

I. General Comment

1. Field activities and results of the investigation were detailed in the Data Gap Report. However, little discussion was provided to indicate how the new soil data will affect ET cover and gamma cap designs (i.e., acceptability of the borrow soil for its intended purpose). It is expected that such details will be provided in the draft design documents for this project and will be reviewed at that time. No change is needed on this document.

FMC Response: The purpose of the Data Gap Report was to summarize the field investigation and results of laboratory testing. The data presented in the Data Gap Report is currently being incorporated into the design of the ET covers. Given that the predominant soil type encountered was silt loess, which exhibits both high moisture capacity and low plasticity, there is nothing to suggest that the WUA is not an acceptable borrow source for cover material.

II. Specific Comments

Section 1.1, Regulatory Background, page 1-2

1. The last sentence in this section should be revised to include the date on which EPA approved the DGWP. In addition, the October 2013 version of the DGWP should be listed in the references section.

FMC Response: The Data Gap Report has been revised to address this comment.

Section 1.4, Document Organization, page 1-2

2. The first sentence in this section should be revised to refer to the Data Gap Report instead of the DGWP.

FMC Response:

The Data Gap Report has been revised to address this comment.

Table 2-1, Summary of WUA Soil Investigation, pages 2-1 and 2-2

3. The DGWP called for collection of grab samples of silt at one foot intervals to a depth of 10 feet below ground surface (bgs) in each test pit. However, in several of the test pits, gravel was encountered at depths shallower than 10 feet bgs. Accordingly, the sampling depths indicated in Table 2-1 should be revised to indicate the actual extent of grab sampling conducted (i.e., 4 feet bgs in test pit TP003, 7 feet bgs in test pit TP009, and 6 feet bgs in test pit TP010).

FMC Response: Table 3.1 of the Data Gap Work Plan (MWH, 2013) states that disturbed samples will be collected to a total depth of "10 feet or until gravels are contacted". Due to the size of the excavator used at the site, the test pits were able to be excavated to deeper depths up to 20.5 feet. Although samples were not generally collected at depths below 10 feet, the test pits were excavated deeper to provide visual observations and logging at deeper depths. Based on visual evidence of the test pit, it is clear that the soil characteristics of silt are uniform throughout the soil profile until the underlying gravels are contacted. Table 2-1 has been revised to add an additional column titled, "Maximum Depth of Grab Sample."

4. Expand the footnote to this table to indicate that the qualifier NC applies to test pits in which gravels were not contacted before the maximum depth of the excavator was reached.

FMC Response: The footnote has been revised to address the comment.

Section 2.1.1, Test Pits, page 2-24.

5. This section should be expanded to discuss the observed variability in depth to gravel within the WUA. Gravel was not encountered at all in more than half of the test pits (TP002, TP004, TP005, TP006, TP007, and TP008). Conversely, gravel was encountered at relatively shallow depths (between 4 and 7.5 feet bgs) in three of the pits (TP003, TP009, and TP010). As noted in the test pit logs (page 56 of the electronic file), this area of shallow gravel appears to cut from east to west across the center of the WUA study area. Such detail is important because it will affect the available volume of borrow soil in this location.

FMC Response: Comment noted. Figure 4-1, showing the cut isocontour map takes into consideration this east-west trending gravel lense; and therefore, does not factor this portion of the WUA into the volume calculations for available cover soil. Section 2.1.1 has been revised to further explain the presence and extent of the gravels. (See also FMC Response to Comment 17 below.)

6. For consistency with Table 2-1, correct this section to note that test pits were excavated to depths ranging from 4 to 20.5 feet below ground surface (bgs).

FMC Response: Section 2.1.1 has been revised accordingly.

Section 2.1.2, Soil Borings, page 2-3

7. As indicated in the DGWP, undisturbed silt samples were to be collected from five soil borings at depths between 2-3 and 6-8 feet below ground surface (bgs). However, Table 2-1 indicates that the only soil sample from boring SB003 was collected from 0-2 feet bgs. A review of the associated boring log in Appendix C shows that silt was encountered only in the uppermost two feet of this boring. Consequently, no undisturbed soil samples could be collected from the pre-determined depths of 2-3 and 6-8 feet bgs. While this deviation from the DGWP appears to be acceptable, an explanation for it should be provided in the text of the Data Gap Report.

- **FMC Response:** Section 2.1.2 has been revised to indicate that an undisturbed sample of silt was collected from 0 to 2 feet bgs in SB003 due to the presence of gravels below 2 feet at that boring location. In addition, a disturbed sample of gravel was collected from the drilling augers from 2 to 15 feet SB003. This sample was analyzed for hydraulic conductivity for the purposes of designing the potential infiltration basin as part of Groundwater Option B. Table 2-1 has been revised to include this sample, text has been added to Section 2.1.2 to describe the collection of this sample and the hydraulic conductivity result has been added to Table 3.2.
- 8. As shown in Table 2-1, a silt samples from the 12-14 feet bgs interval was collected from boring SB007. The text indicates that this sample was collected to provide geotechnical information on deeper silts at the WUA. It is unclear whether a single sample will adequately represent properties of deeper silt across the WUA. Given the fact that deep silt was found in numerous test pits and borings across the WUA, it is likely that deep silt will be incorporated into the planned ET and gamma caps. Section 4 of the report should compare shallow and deep silt results (as shown on Table 3-1), and clarify whether any significant differences were evident that may impact design or construction of the ET and gamma caps. If significant differences are identified, additional samples should be collected to determine the usability of deeper silt.
 - **FMC Response:** As described in Section 4 of the Data Gap Report, ProUCL statistical analysis was performed on laboratory data from both in-situ and ex-situ samples for maximum dry density and moisture content. Based on the analysis, the data distributions are normal suggesting a uniform soil type. In addition, a review of all particle size distribution (PSD) plots and Atterberg Limits Tests for disturbed samples of the silt further confirms a uniform soil type. It should be noted that index properties such as PSDs and Atterburg Limits are a key indicator of soil type. Additionally, the manner in which these silts were deposited, aeolian, further suggests that the physical properties of the soil with depth will remain consistent. Therefore, further sampling of silts at deeper depths is not warranted. Additional text has been added to Section 4.1 that describes the uniformity of the silt with depth.
- 9. According to the Table 3.1 of the DGWP, gravel samples were to be collected from the five soil borings at a depth approximately 10 feet beneath the gravel horizon. However, it does not appear that gravel samples were collected from the soil borings for permeability analysis. In fact, Section 2.1.2 of the report indicates that the only one gravel sample collected during this investigation was taken from test pit TP003, and the associated log in Appendix B (page 46 of the electronic file) suggests that the samples was collected from the top of the gravel horizon (i.e., at 4feet bgs, rather than 14 feet bgs). This deviation from the approved DGWP suggests that inadequate gravel data has been obtained. The text of the report should be revised to: (1) document these deviations in the sampling program; (2) discuss whether the single, shallow gravel sample is representative of gravel across the WUA; and (3) explain why additional gravel samples are not needed to meet RD information needs. If sufficient justification cannot be provided, additional gravel samples are recommended.

FMC Response: While preparing the Data Gap Work Plan, the depths of gravels were believed to be much shallower, on the order of ± 10 feet. However, during the test pitting, the depths of gravel were shown to be generally much deeper than 10 feet throughout the site, with the exception of the shallow east-west gravel lense. The main purpose of the gravel sampling was to determine the hydraulic conductivity of the gravels for the purpose of sizing potential infiltration basins for treated groundwater for groundwater remedy water management option B. Given that the depth of excavation required to obtain the volume of capping soil will in general be much shallower than the underlying gravels, it was determined that the controlling factor in the infiltration basins will be the in-situ hydraulic conductivity of the silts. Therefore, an undisturbed sample of the silts at deeper depth, 12-14 feet bgs, was collected from SB0007 to provide data for this purpose. Further, the gravels that were contacted appeared to be very uniform in terms of shape and size suggesting the hydraulic conductivity of these gravels will be fairly uniform. Therefore, no additional sampling is required at deeper depths for the gravels. Additional text has been added to Section 2.1.2 that incorporates this response.

10. The first sentence in this section should be corrected to note that the five soil borings advanced during this investigation were numbered SB003 through SB008, with the exception of SB005. No soil boring was conducted in the vicinity of test pit TP005.

FMC Response: The text has been revised to address the comment.

Section 2.2.1, Stormwater Sewer Survey Background and Objectives, page 2-3

11. The first paragraph in this section indicates that the selected remedy for RA-A calls for covering the area (and underground storm sewer piping) with a gamma cap. The second paragraph indicates that any segments of the storm sewer pipe that cannot be cleaned within RA-B will be plugged with concrete and covered by an ET cap. Expand this section to identify remedial action objectives (RAOs) for the storm sewer, and confirm that both types of caps will satisfactorily achieve those RAOs.

FMC Response: The relevant RAOs for the underground storm sewer piping in RA-A (and RA-B and RA-K) as taken from Table 4-2 of the Supplemental Feasibility Study Report for the FMC Plant OU – July 2010 (SFS Report) are:

- 1. Prevent external exposure to radionuclides in soils at levels that pose estimated excess risk greater than 1 x 10-4, or site-specific background levels where that is not practical.
- 2. Prevent ingestion of soils containing COCs at levels that pose estimated excess risks above 1 x 10-4, a non-cancer risk HQ of 1, or site-specific background levels where that is not practical.
- 3. Reduce the release and migration of COCs to the groundwater from facility sources that may result in concentrations in groundwater exceeding risk-based concentration (RBCs) or chemical specific Applicable or Relevant and Appropriate Requirements (ARARs), specifically Maximum Contaminant Levels (MCLs).

In addition, the following RAO was developed (as presented in Section 7.1.1 of the SFS Report) to address elemental phosphorus (P4) in subsurface soils and underground piping as a principal threat source material (PTSM):

 Prevent direct exposure to P4 under conditions that may spontaneously combust, posing a fire hazard, or resultant air emissions that represent a significant risk to human health and the environment.

Underground storm sewer piping that is successfully cleaned in-place will no longer present a threat to human health and/or the environment as all COCs potentially associated with the storm sewer piping (i.e., P4, radionuclides, metals, and leachable metals posing a threat to groundwater) will have been removed and appropriately disposed. Therefore, cleaned underground storm sewer piping by itself meets all of the above-listed RAOs. While this underground storm sewer piping resides in RA-A, which will be capped with a gamma cap as prescribed in the IRODA, the remedial action for the underground storm sewer piping is independent of the requirement for placement of the gamma cap in RA-A.

While we generally understand that the underground storm sewer piping can be cleaned with readily available technology, a contingency was included in Section 2.2.1 of the Data Gap Report, in the event sections of the piping could not be cleaned. In that event, the ET cap placed over RA-B could be extended over the un-cleaned sections of underground piping. As stated in the SFS Report and accepted in the IRODA, placement of a properly designed ET cap over underground piping would meet all of the above listed RAOs, even with the presumption that radionuclides, metals, and/or P4 remain within the un-cleaned sections of the underground storm sewer piping.

Regardless, at any level of success of cleaning of the underground storm sewer piping in RA-A, the underground piping would be plugged at the boundaries of RA-A with RA-B and RA-K to eliminate a conduit for water moving between the different capped areas.

Section 2.2.1 has been modified to clarify this achievement of the RAOs.

Section 2.2.2, Video Survey Description, pages 2-4 and 2-5

12. This section summarizes results of the storm sewer video survey which, as shown on Figure 2-2, extended across RA-A, RA-B, and RA-K. Each segment in the figure appears to have been addressed except for the one between Area Inlets 1 and 3. Confirm the status of surveying over this area and modify the Data Gap Report accordingly.

FMC Response: The Data Gap report has been revised to better clarify that while historical plant drawings indicate that the piping segment from Area Inlet #1 to Area Inlet #3 exists, visual investigation of the vault at Area Inlet #1 did not reveal the presence of a pipe entering from the south – only a pipe running towards the north to the East Discharge. Similarly, visual investigation of the vault at Area Inlet #3 only revealed pipes connected on the south side (from Manhole #1) and west side (toward Area Inlet #4); no pipe leaving to the north towards Area Inlet #1 was present. Whether the

historical drawing was incorrect or had not been updated to reflect later removal of the pipe segment cannot be determined; regardless, there is no observable evidence that a segment of piping is present between Area Inlet #3 and Area Inlet #1. Therefore, this segment was not present to survey. The figure has been revised to indicate this piping segment is not present and a bullet has been added at the end of Section 2.2.2 that incorporates this response into the text.

Section 3.1.2, Hydrological Testing, page 3-1

13. According to Table 3.2 of the DGWP, disturbed soil samples from every other test pit were to be sampled for saturated hydraulic conductivity (ASTM D5084) at 85 and 90% of the maximum dry density (MDD) level. Thus, ten samples would undergo conductivity testing. Ten water characteristic curve tests (ASTM D6836) – two tests on every other test pit sample – were also slated for completion. However, Table 3-2 of the report suggests that only five test pit samples were subjected to these analyses. A review of Appendix D indicates that all five of the test pit samples were analyzed at 85% MDD, and that no data are available for conductivity at 90% MDD. These deviations from the work plan should be noted in the text, along with an explanation as to why these changes should not be considered lingering data gaps for the investigation.

FMC Response: The DGWP specified that Soil Water Characteristic Curve Testing would be performed on disturbed samples remolded to both 85 and 90% of MDD. However, Water Characteristic Curve Testing was performed only on disturbed samples remolded to 85% MDD. The deviation was mainly due to the fact that the construction specifications for the cover soil (silt from the WUA) would target an in-place density of 85% MDD $\pm 3\%$. This specification has been chosen to limit the in-place density to below 90% MDD. Therefore, Water Characteristic Curve Testing at 90% MDD was not warranted. Section 3.1.2 has been revised to describe and justify this deviation from the Work Plan.

Section 3.2, Root Density Testing, pages 3-4 through 3-6

14. Appendix F shows that root density testing was performed on depth-specific samples collected from three locations in each of nine grids across the existing vegetable trial plot. Expand Table 3.4 of the report to also show root density results for Grid 16, Location 3; all three locations within Grid 17, and all three locations within Grid 18 (provided on page 178 of the electronic file). In addition, correct the last sentence on page 3-6 to refer to the 6- to 12-inch interval at Grid 8, which was not analyzed because it was compromised during shipping. Finally, describe the incident in which this sample was compromised and detail what was done to ensure that none of the other samples had been similarly affected.

FMC Response: Table 3.4 has been revised to list the additional samples from Grids 16, 17, and 18. The last paragraph of Section 3.2 has been revised to correct the reference to Grid 8 and explain that the sample bag was reported as torn when received at the laboratory and was evidently damaged during shipment.

Section 4.1, Geotechnical Recommendations, page 4-1

15. This section should be expanded to discuss results pertaining to the susceptibility of WUA soils to erosion and desiccation cracking, as determined during the data gap investigation. The discussion should also indicate whether the majority of WUA soils are sufficiently nondispersive for purposes of cap construction. Any limitations on use of WUA borrow soil identified as dispersive (i.e., rating a 3 via the Crumb Test) should also be specified.

FMC Response: Additional text related to the erosion and desiccation potential of the WUA soils has been added to Section 4.1. Atterberg limits and dispersive testing was performed on the majority of disturbed samples to assess the potential for desiccation cracking and erosion of the silts. Based on the Atterberg limits testing, the plasticity index (PI), ranged between 1 and 14. These results indicate that the soils have very low-plasticity and therefore are not susceptible to desiccation cracking associated with volumetric changes (shrinkage) induced by moisture fluctuations. The results of the dispersion testing both (Crumb and double hydrometer testing) indicate that the soils are generally non-dispersive to moderately dispersive based on Crumb test results characterizing the majority of samples being between a Grade 1(non-dispersive) and 2 (Intermediate) and double hydrometer testing ranging between 18.6 and 44.3-percent dispersion. Therefore, based on these results, there is nothing to preclude the WUA soils being used as capping soil.

Section 4.3, Root Density Recommendations, page 4-2

- 16. Statistical analyses presented in Appendix H indicated depth-specific root density mean values (expressed as grams of dry root material per 100 grams of soil) of:
 - 0.067 grams in the 0-6 inch sampling interval;
 - 0.0337 grams in the 6-12 inch sampling interval; and
 - 0.014 grams in the 12-18 inch sampling interval.

A statistical evaluation of all 53 soil samples collected from the 0-6 and 6-12 inch intervals yielded a mean root density value of 0.051 grams. As noted in Section 4.3, this value was selected as the design root density value to be used in RD development. However, it is unclear why results from the 12-18 inch sampling interval were not included in this analysis. If root density below the uppermost foot of soil is not considered an important factor for cap design, it is unclear why soil samples were even collected from the deeper intervals for root density analysis. Expand the text to provide justification for these omissions and to explain how use of the selected design value will affect establishment of an adequate vegetative cover layer on the ET and gamma caps.

FMC Response: Samples collected below 6-12 inches were not factored into the statistical analysis because the cover design assumes the bulk of root density is within the upper 12-inches. This is a conservative assumption given that there were roots present below 12-inches. However, due to the sparser aerial distribution of the 12-18-inch soil thickness at the re-vegetation test area, these data were not included in the statistical analysis. No changes to the text are warranted.

Section 4.5, Borrow Source Availability, page 4-2

17. This section states that approximately 2.4 million cubic yards of silt are available at the WUA for use in the ET and gamma covers. However, this estimate is unsupported by mathematical calculations or software output. Instead, this estimate was reportedly based on Figure 4-1, an isocontour map showing the depth of silt in the WUA. However, this figure is confusing, with contour lines that are unlabeled and difficult to translate into depths. It is possible that a different visual approach (e.g., using shades of color to represent silt thickness) would facilitate interpretation of Figure 4-1. Moreover, it does not appear that the figure accounted for soils deemed unusable due to dispersivity or other considerations. Revise the figure to provide for better interpretation, and provide calculations demonstrating how the figure was determined.

FMC Response: Figure 4-1 has been revised to change it from an isocontour to an isopach drawing to show color shading associated with depths of excavation. Note that the borrow availability assessment excludes from consideration the area in the vicinity of the shallow gravels. Additionally, there is no evidence to preclude any silt soils from being used as borrow material based on dispersion or desiccation potential. No changes to the text are warranted.

Table 4.3, Summary of Stormwater Sewer Piping Video Survey, page 4-3

18. After adding in sediment and other solids present between Area Inlets 1 and 3 (as discussed in Specific Comment 12 above), this table should be identified as a conservative estimate of solids to be removed from the storm sewer in areas RA-A, RAB, and RA-K. Relatively clear areas noted in Section 2.2.2 of the report (i.e., the first 40 feet in the segment from the east discharge pipe toward Area Inlet 1 and the first 55 feet in the segment from Manhole 1 to Area Inlet 3) do not appear to have been subtracted out of the volume calculations in this table.

FMC Response: As stated in response to Comment 12 above, the piping segment between Area Inlets 1 and 3 has been determined to no longer be present based on visual investigations in the vaults at both Area Inlet 1 and Area Inlet 3. Therefore, this segment was not included in Table 4.3. Also, column 6 (*Percent full of Sediment*) is an estimated average over the total length of the piping segment. A footnote has been added to Table 4.3 to indicate that the calculated "maximum" sediment volumes are a conservative estimate for waste management planning purposes.